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FURTHER STUDIES OF THE UNDERWATER
NOISE PRODUCED BY RAINFALL

National Center for Physical Acoustics

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FURTHER STUDIES OF THE UNDERWATER
NOISE PRODUCED BY RAINFALL

BY

PAUL A. ELMORE
HUGH C. PUMPHREY
and
LAWRENCE A. CRUM

National Center for Physical Acoustics
University, MS 38677

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19. (cont.) rainfall spectrum. Finally, the time between drop impact and bubble formation was found to increase monotonically as drop size or impact velocity increases.

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ABSTRACT

Further studies of the underwater noise produced by rainfall. Paul A. Elmore, Hugh C. Pumphrey, and Lawrence A. Crum; National Center for Physical Acoustics; University of Mississippi; University, MS 38677

A study of the sound produced by water drops striking a water surface has confirmed some earlier results [Pumphrey et al. *J. Acoust. Soc. Am.* 85, 1518 (1989)]. In particular, for a certain well-defined range of drop sizes and impact velocities, drops will predictably and repeatedly entrain bubbles; this phenomenon has been named regular entrainment. In the present study, various fixed drop diameters have been used to investigate how bubble frequency, dipole strength, and time between drop impact and bubble formation vary with impact velocity. It is found that as impact velocity is increased through the point where entrainment begins, both frequency and dipole strength decrease to a minimum value and then rise again as the highest velocity at which entrainment occurs is approached. Both terms show increased variability near the critical upper and lower velocities. The frequency tends to increase monotonically as drop size is reduced; drops that entrain bubbles at their terminal velocities tend to produce frequencies near 14 kHz, which is also the peak frequency of the natural rainfall spectrum. Finally, the time between drop impact and bubble formation was found to increase monotonically as drop size or impact velocity increases.

INTRODUCTION

This study further investigates the underwater noise of rainfall and the phenomenon known as regular entrainment. Previous studies (Pumphrey, Crum, and Bjørnø, 1989a; Pumphrey and Crum, 1989b) have shown that the impact of a single drop on a plane surface of water can make two sounds: first, an impact noise and then a bubble noise, which originates from the oscillations of a bubble entrained underneath the surface by a drop. Therefore, the spectrum of underwater rain noise, which is shown in Fig. 1, can only be caused by these two effects. However, the impact noise is not believed to be a major contributor to the total spectrum. Although not every drop entrains a bubble, the individual contribution by the bubbles are much larger than that due to the impact alone. The majority of these bubbles are thought to be oscillating at 14 kHz because the spectrum has a large peak at that frequency.

These studies have also shown that drops will entrain bubbles predictably and repeatedly within a well defined range of impact velocities and drop sizes, as shown in Fig. 2a. Entrainment that occurs in this manner is called "regular entrainment." Also shown in this figure are data from Scrimger, which give the sizes and number of raindrops measured in three different rainfalls (Scrimger et al., 1987). The comparisons indicate that the drops which regularly entrain drops at terminal velocity are found in abundance in natural rain. Thus, in order to understand the mechanism of rain noise, we must first learn about regular entrainment.

The regular entrainment process starts with the entraining drop striking the water and forming a conically shaped cavity. This cavity will eventually stop growing and collapse after a few milliseconds. As it does, the bottom part is pinched off from the rest of the cavity, forming a damped radially oscillating bubble underneath the surface. This bubble has a dipole radiation pattern because it is very close to a pressure release surface. Another process, which has been named "irregular entrainment" by Pumphrey and Crum, can create bubbles as well but by unpredictable cavity deformations underneath the water or entrainment by drops formed from jets erupting from the cavity (Franz, 1959; Longuet-Higgins, 1989; Pumphrey and Crum, 1989b; Oguz and Prosperetti, 1989).

The present experiment's purpose has been to reproduce these earlier findings and to examine more closely the role of regular entrainment in the underwater noise produced by rainfall. Thus, the experiment investigated the characteristics of bubbles over the entire entrainment region. The bubbles' radii, frequencies, and initial dipole strengths were measured along with the amount of time between drop impact and bubble formation. The measurements were made by keeping the drop size constant but varying the impact

velocity. The study was then conducted over a wide range of drop sizes. Using the results of the study, we can conclude whether or not rain noise is caused by regular entrainment.

METHODS

The experiments were conducted in a water tank measuring a cubic meter in volume filled with tap water to a depth between 0.85 and 0.9 meters. The transducer system used for measuring acoustic frequency and pressure was a miniature hydrophone (Brüel & Kjær 8103) and a charge amplifier (Brüel & Kjær 2635). The signal was then read on a digital oscilloscope (LeCroy 9400) which is capable of analyzing the signal in various ways (FFT's, averages, integration, etc.). The oscilloscope was interfaced by a GPIB to a computer (DEC MINC-73) for additional signal analysis. A diagram of the experimental set-up is shown in Fig. 3.

Drops of tap water were dropped into the water tank from a syringe suspended above the center of the tank. Various tubings or hypodermic needles were attached to it to create different sizes of drops. Drops larger than 1.71 mm in diameter were produced from allowing them to drip from the end of a needle, glass pipet, or piece of tubing. Smaller drops had to be produced by feeding the water from the syringe to a 30-gauge needle attached to the cone of a loudspeaker. The speaker-needle system was then vibrated with a square wave signal while allowing water to flow freely from the syringe to the needle's tip (this method gave the drops some but negligible amounts of horizontal velocity). The actual size of the drops, assuming that they are spherical, was determined by measuring the volumes of ten or fifteen captured samples with a microliter syringe, converting the each volume to a corresponding diameter, and then averaging the diameters. The standard deviation of the measured diameters was found to be quite small.

The impact velocity, v_i , of the drops was determined by measuring the height of the fall, z , and calculating v_i by using the equation

$$v_i = v_t \sqrt{1 - \exp\left(\frac{-2gz}{v_t^2}\right)}, \quad (1)$$

where v_t is the terminal velocity. The value of v_t for a given drop size was found by computing it from a polynomial fit (Dingle and Lee, 1972) of earlier experimental data (Gunn and Kinser, 1949). The polynomial fit and equation (1) were programmed into the MINC-73 computer to ease the computation. The error of impact velocity based on the error in measuring the height of fall was not found to be significant.

Using the impact velocities, the kinetic energy, T , of each drop at impact can be found from its classical form:

$$T = \frac{1}{2}mv_i^2, \quad (2)$$

where m is the drop's mass. Since the drop's radius, not mass, was directly measured, it was more convenient to express T in terms of the drop's radius, R , and v_i . The drop's mass is related to its radius by the relation

$$m = \rho V = \left(1.0 \times 10^3 \frac{\text{kg}}{\text{m}^3}\right) \left(\frac{4}{3}\pi R^3\right), \quad (3)$$

where ρ is the water density, V the drop's volume. Substituting this expression for mass into equation (2) gives the desired form,

$$T = \left(\frac{2\pi}{3} \times 10^3 \frac{\text{kg}}{\text{m}^3}\right) R^3 v_i^2. \quad (4)$$

The frequency of the bubble's oscillation was measured by either of two methods. One method was to measure the time between the second and seventh positive voltage peaks (to make sure transient behavior was excluded) directly from the oscilloscope screen, as shown in Fig. 4, and then multiply the reciprocal of the time by five. The LeCroy 9400 measures the temporal difference and its reciprocal between any two points along the trace. The other method was to interface the oscilloscope to the computer and use a program that displays numerical values of the oscillation's frequency and initial amplitude. The latter method was more precise than the first, but comparisons between the two showed no significant difference. The damped signals produced usually had quality factors of ten or higher.

From these readings the frequency was converted to a bubble radius, a , by the relation

$$a = \frac{\sqrt{3\kappa P_0/\rho}}{2\pi f}, \quad (5)$$

where P_0 is the static pressure of the bubble, ρ the water density, and f the bubble's frequency. Since the value of these variables were known for the environmental conditions during the experiment, the equation reduces to

$$a \approx \frac{3.28}{f} \quad (6)$$

Measurements of the initial dipole strength began with the measurements of the initial amplitude. These measurements were also done by either measuring initial voltage directly on the oscilloscope screen or by using the program. When reading it directly from the oscilloscope, the voltage difference was measured between the first negative voltage peak and the second positive peak (again, to exclude any transient behavior), as shown in Fig. 5. The initial voltage was then converted to initial dipole strength, D , by solving for D in the formula

$$p = \frac{D \cos \theta e^{i f(t - r/c)} e^{-\beta(t - r/c)}}{r} \quad (7)$$

where p is acoustic pressure, and θ is the angle between the bubble and the hydrophone with respect to the perpendicular of the plane of the water surface going through the hydrophone. f is the bubble frequency, t the time from bubble formation, c the velocity of sound underwater (≈ 1500 m/s), β the damping factor, and r the distance from the hydrophone to the bubble. This distance was set at five centimeters. Since $\theta = 0$, $\cos \theta = 1$. Also, $t - r/c \approx 0$, so $e^{-\beta(t - r/c)} \approx 1$, and $e^{i f(t - r/c)} = 1$ at a peak. Therefore,

$$p \approx \frac{D}{r} = 5 V_{pp} \quad (8)$$

for the equipment that was used. Since $r = 0.05$ m, the above equation reduces to

$$D \approx \frac{V_{pp}}{4} \quad (9)$$

The temporal measurement between the drop impact and bubble formation was facilitated by a function on the oscilloscope that averages the traces from fifty drop impacts and subsequent bubble noise and displays the average as a single trace. Using this resultant trace, the time measurement was made between the base of the bubble noise and a reference point in the transient behavior of the bubble's formation, as shown in Fig. 6.

The data analysis was done using the Cricket Graph software package available for Macintosh computers.

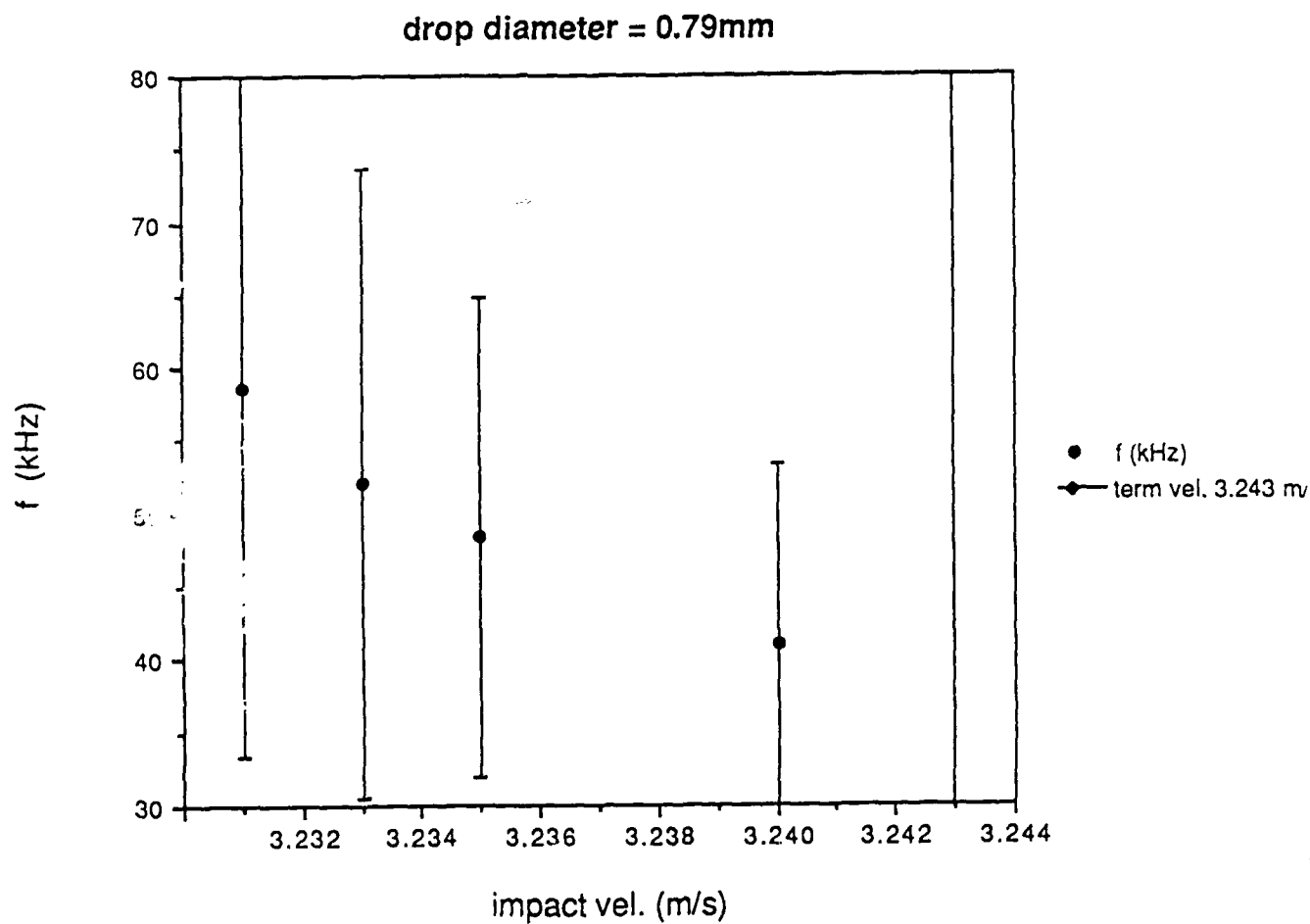
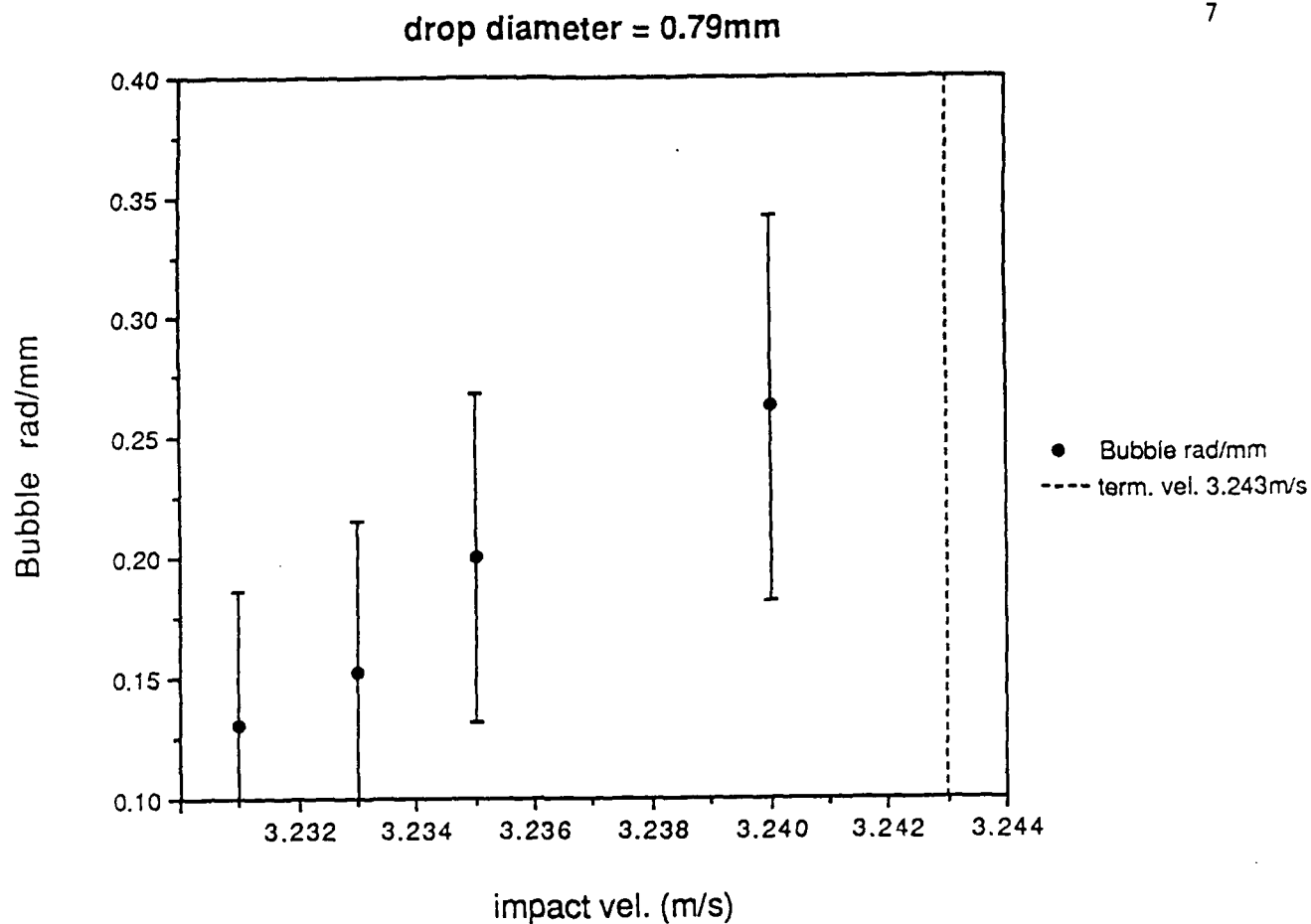
EXPLANATION OF DATA SET 1

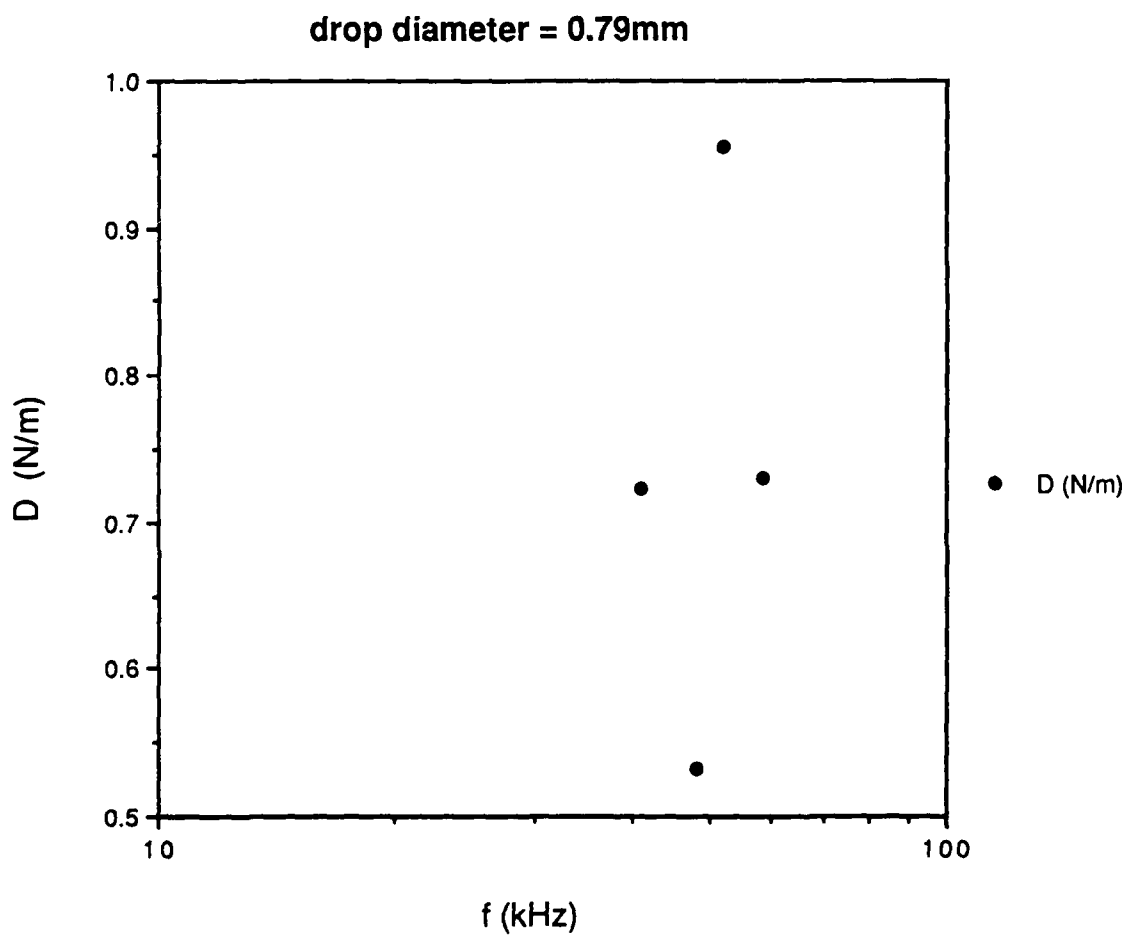
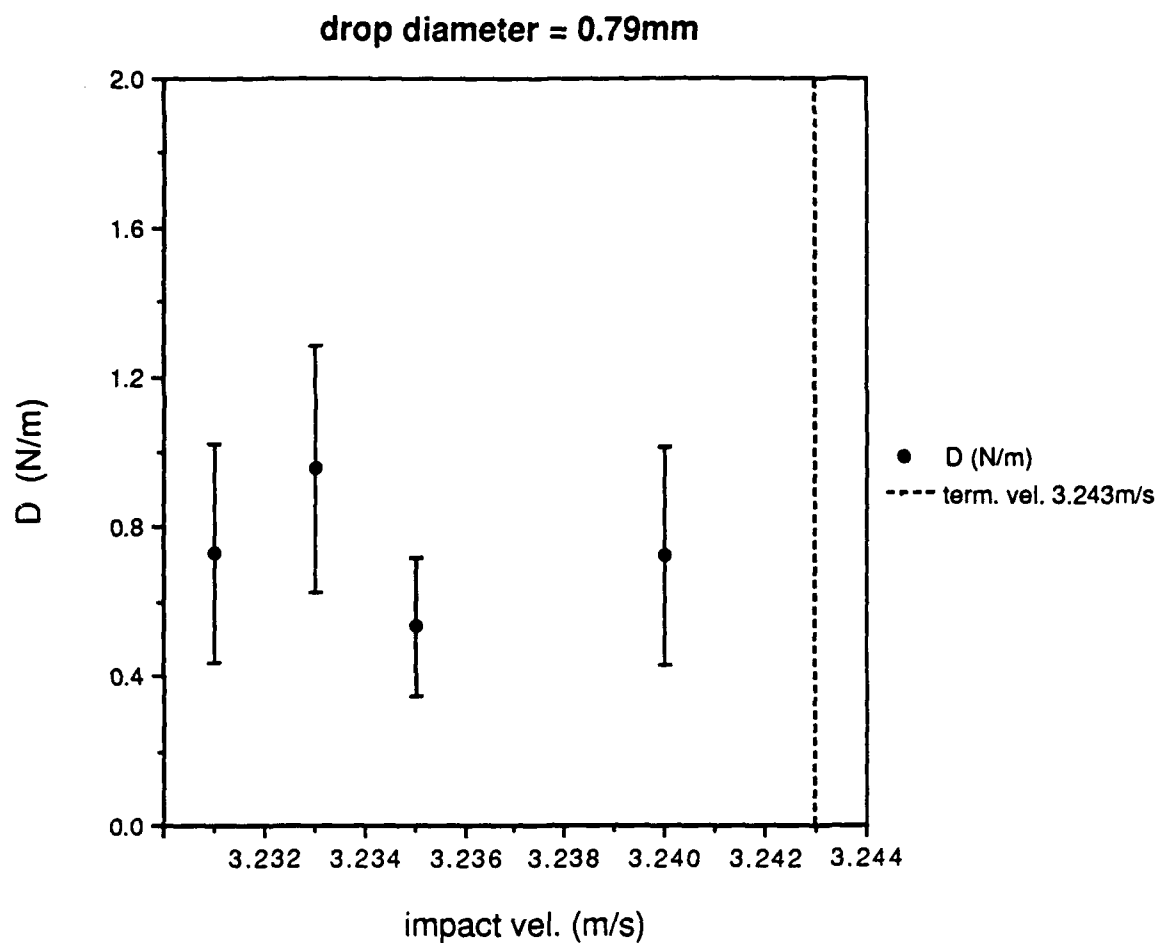
The first set of data shows the final velocity, bubble radius, frequency, and initial dipole strength for each drop size. The drop diameter, measured in millimeters, is listed above each table. The dates and times shown at the top of each sheet are not of any significance. The first column is the drop's impact velocity in meters per second. The columns following it are the measured values of the bubble's frequency in kilohertz, initial dipole strength in newtons per meter, and radius in millimeters. The standard deviations of each value follow it. Each row represents the average of thirty trials, except when noted.

There are four graphs that follow each data page. The first three plot the relationships between impact velocity and bubble size, frequency, and initial dipole strength. The fourth graph plots the initial dipole strength versus the frequency.

DATA SET 1

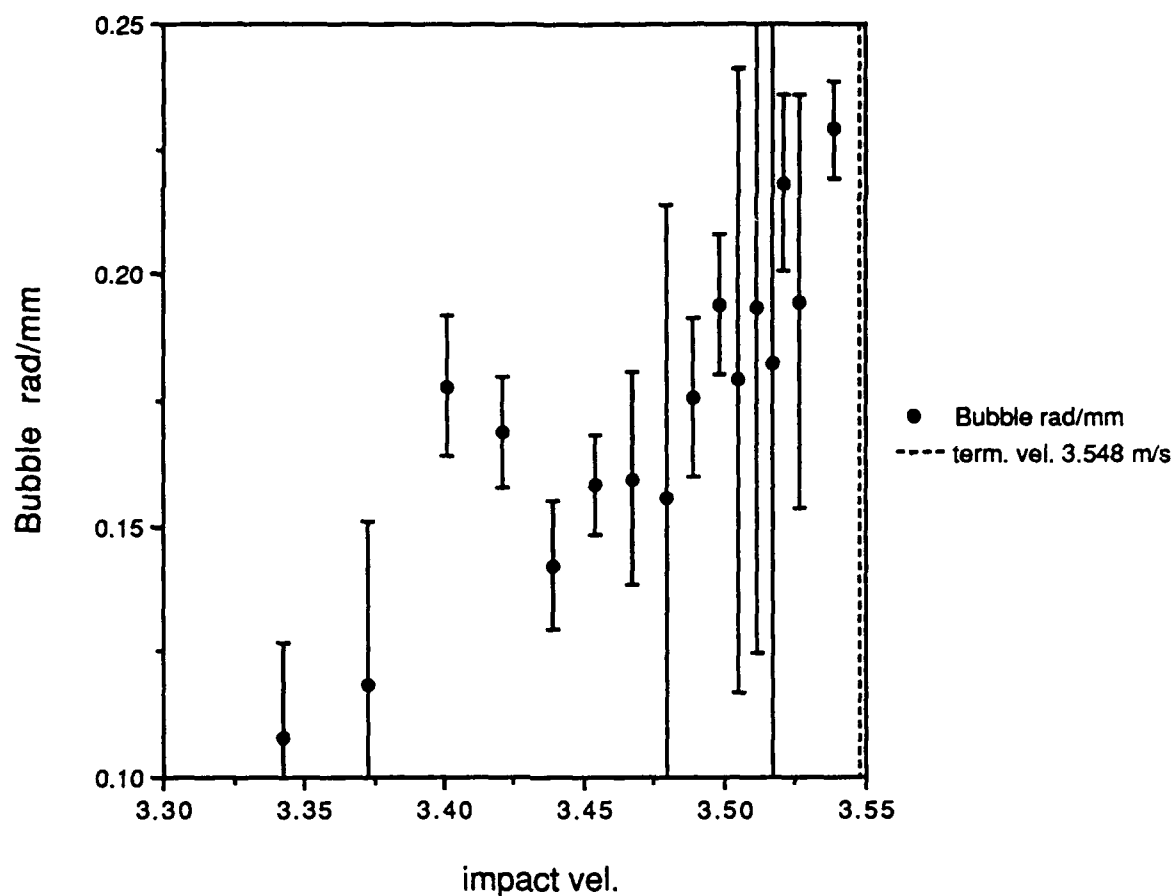
| | impact vel. | f (kHz) | sd of f | D (N/m) | sd of D | Bubble rad/mm | sd of rad |
|---|-------------|---------|---------|---------|---------|---------------|-----------|
| 1 | 3.235 | 48.350 | 16.422 | 0.532 | 0.185 | 0.200 | 0.068 |
| 2 | 3.233 | 52.088 | 21.562 | 0.955 | 0.330 | 0.152 | 0.063 |
| 3 | 3.231 | 58.626 | 25.267 | 0.730 | 0.290 | 0.130 | 0.056 |
| 4 | 3.240 | 40.875 | 12.521 | 0.723 | 0.290 | 0.262 | 0.080 |



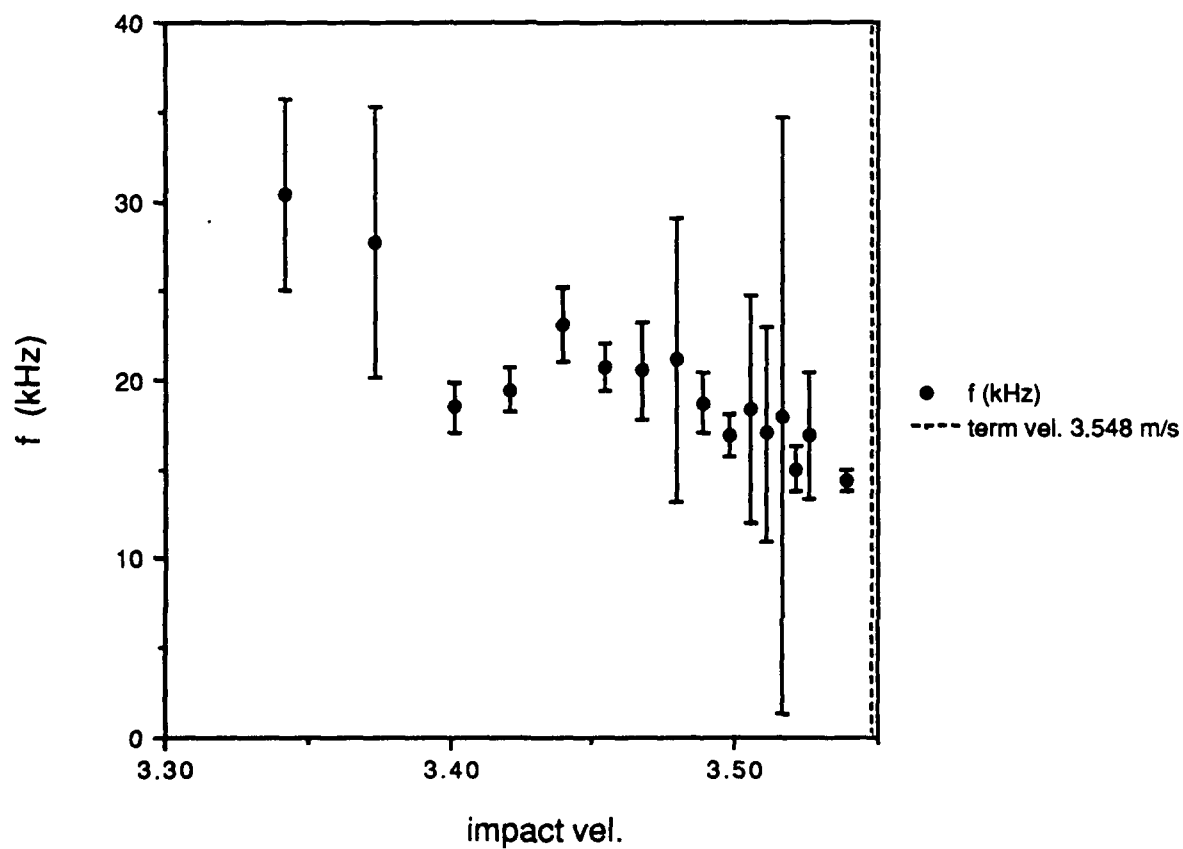


| | impact vel. | f (kHz) | sd of f | D (N/m) | sd of D | Bubble rad/mm | sd of rad |
|----|-------------|---------|---------|---------|---------|---------------|-----------|
| 1 | 3.539 | 14.331 | 0.612 | 0.422 | 0.070 | 0.229 | 0.010 |
| 2 | 3.526 | 16.852 | 3.581 | 0.318 | 0.065 | 0.195 | 0.041 |
| 3 | 3.521 | 15.029 | 1.197 | 0.385 | 0.075 | 0.218 | 0.017 |
| 4 | 3.517 | 17.973 | 16.704 | 0.362 | 0.080 | 0.182 | 0.170 |
| 5 | 3.511 | 16.975 | 6.032 | 0.350 | 0.095 | 0.193 | 0.069 |
| 6 | 3.505 | 18.329 | 6.341 | 0.438 | 0.092 | 0.179 | 0.062 |
| 7 | 3.498 | 16.899 | 1.213 | 0.407 | 0.058 | 0.194 | 0.014 |
| 8 | 3.489 | 18.698 | 1.690 | 0.492 | 0.107 | 0.175 | 0.016 |
| 9 | 3.479 | 21.115 | 7.920 | 0.652 | 0.163 | 0.155 | 0.058 |
| 10 | 3.467 | 20.579 | 2.743 | 0.340 | 0.060 | 0.159 | 0.021 |
| 11 | 3.454 | 20.749 | 1.315 | 0.463 | 0.075 | 0.158 | 0.010 |
| 12 | 3.439 | 23.081 | 2.084 | 0.472 | 0.075 | 0.142 | 0.013 |
| 13 | 3.421 | 19.439 | 1.285 | 0.365 | 0.045 | 0.169 | 0.011 |
| 14 | 3.401 | 18.447 | 1.460 | 0.405 | 0.065 | 0.178 | 0.014 |
| 15 | 3.373 | 27.705 | 7.600 | 0.873 | 0.223 | 0.118 | 0.032 |
| 16 | 3.342 | 30.355 | 5.319 | 1.005 | 0.170 | 0.108 | 0.019 |

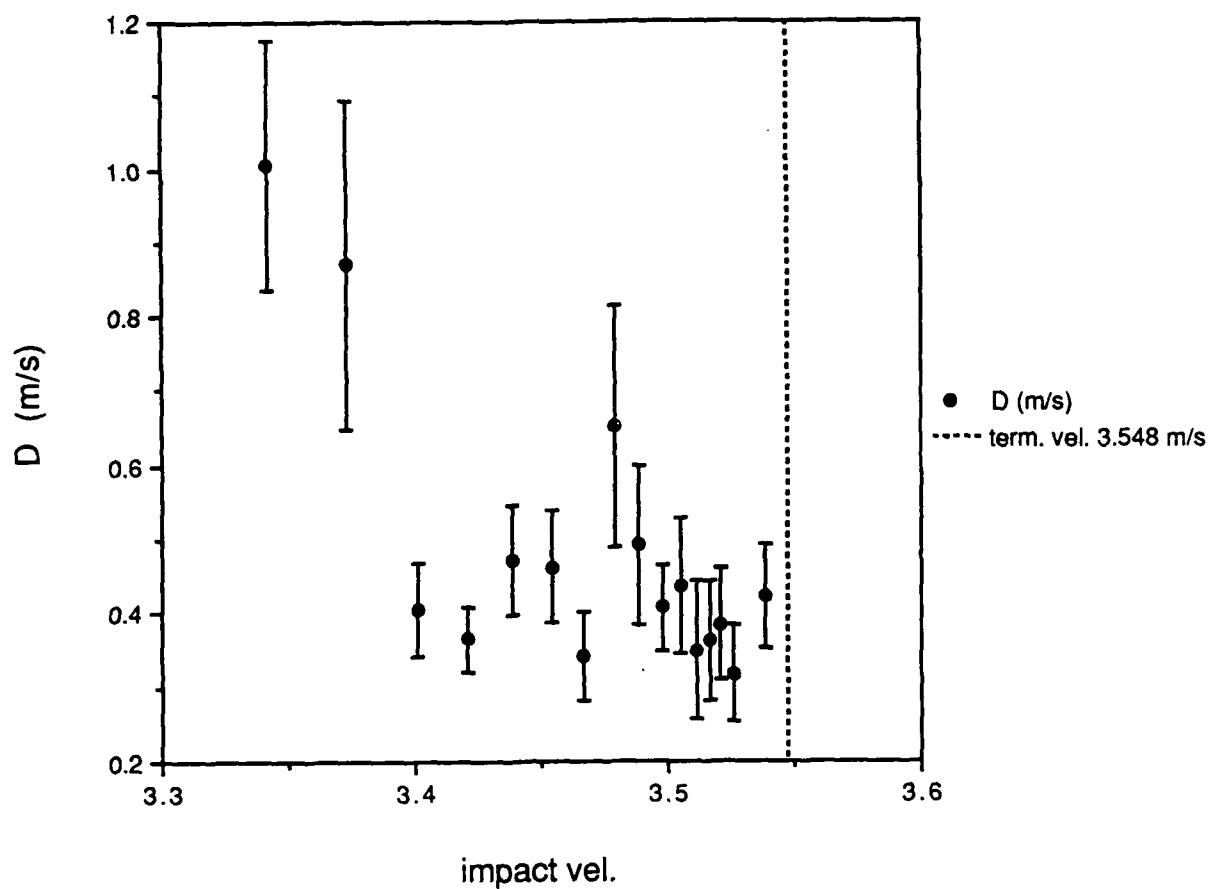
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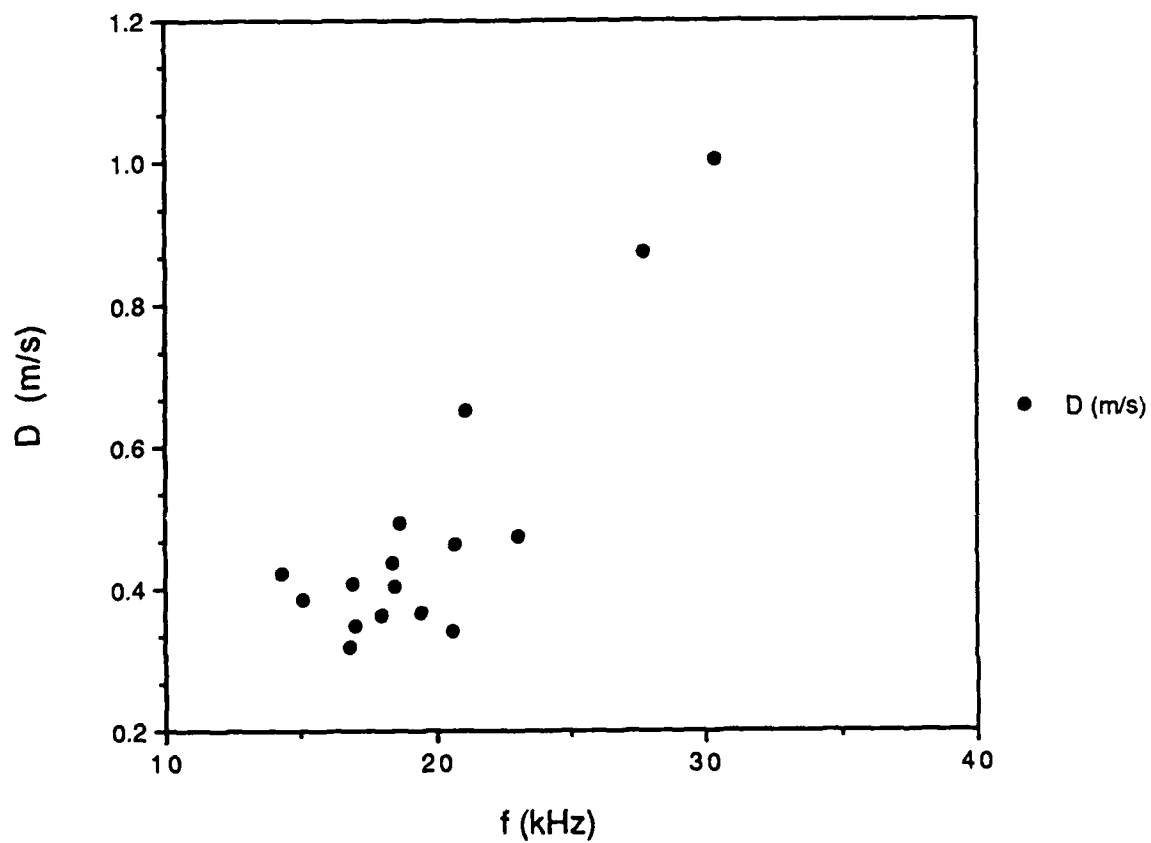
drop diameter = 0.87mm



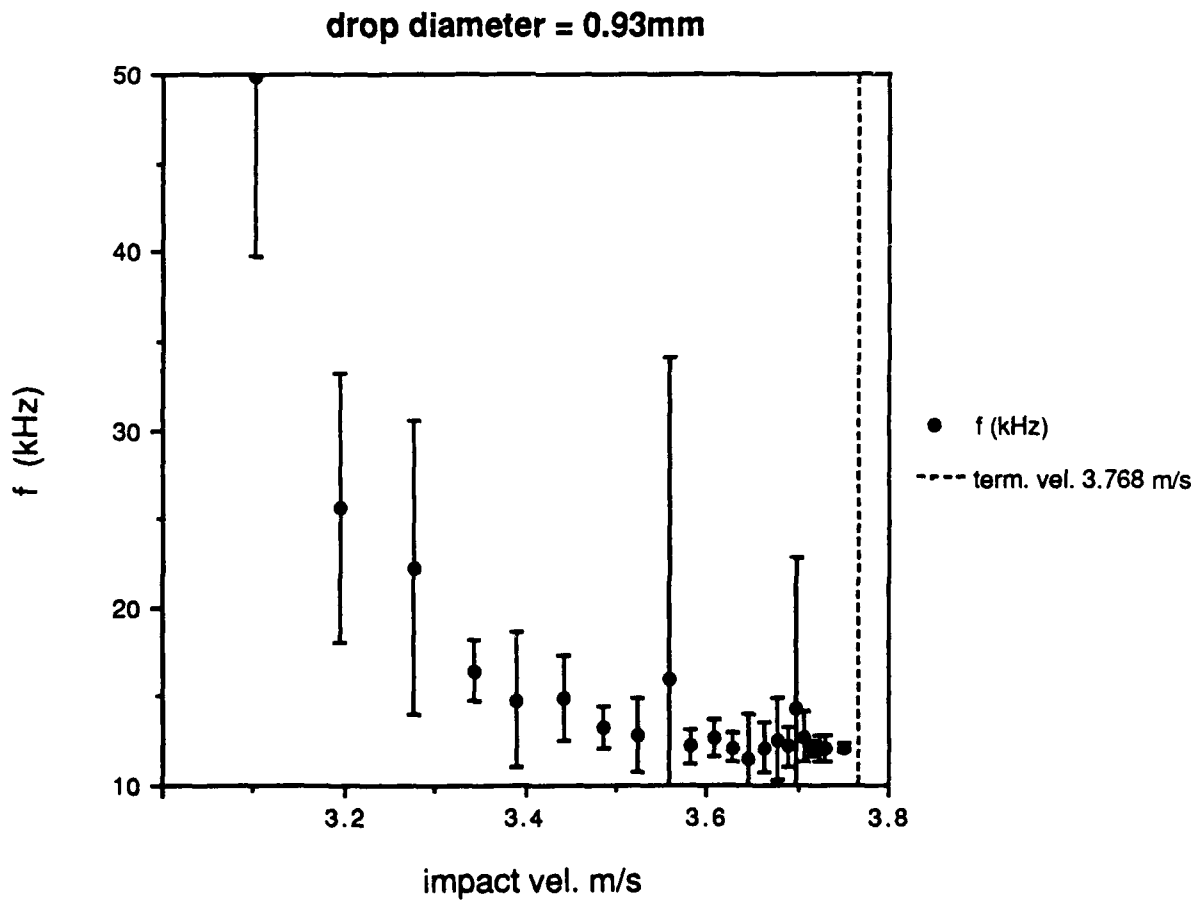
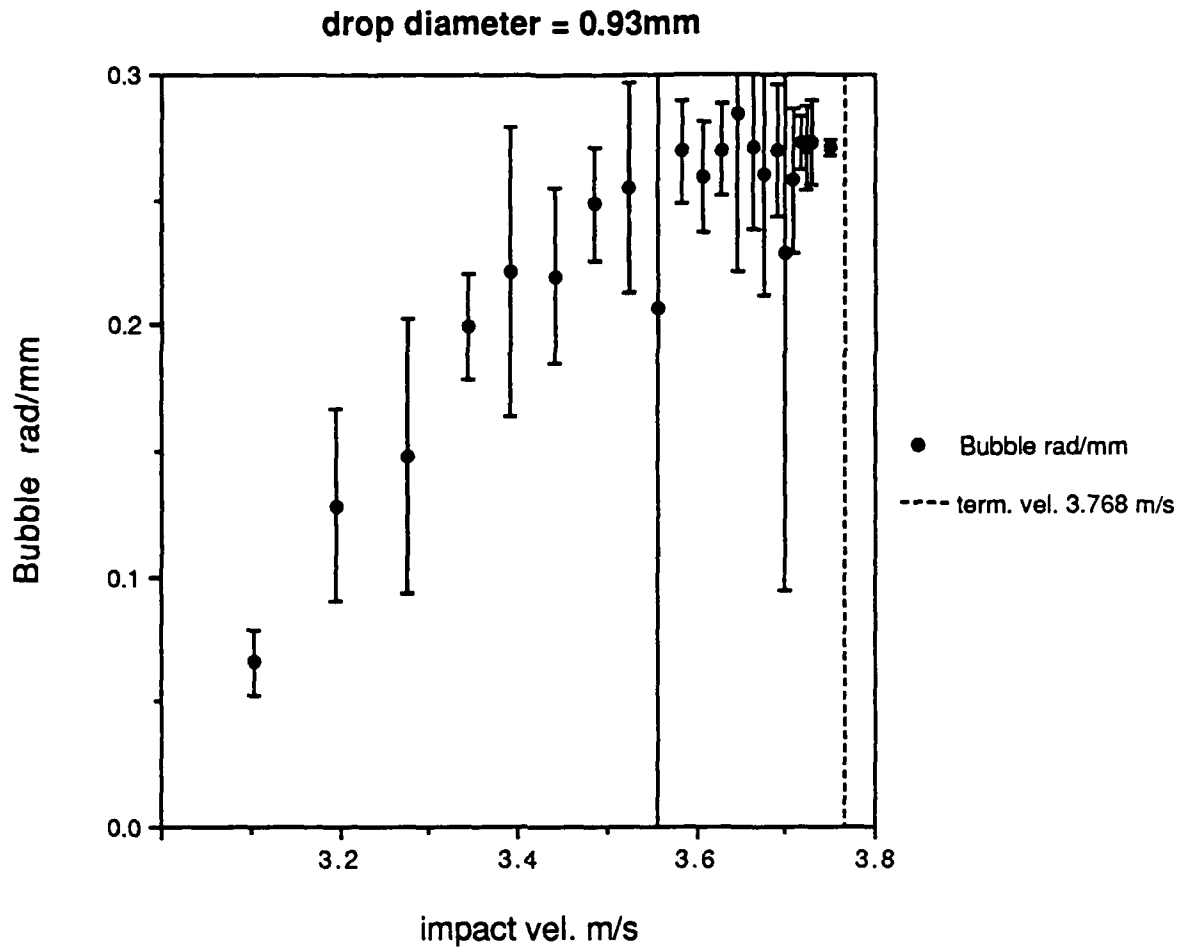
drop diameter = 0.87mm

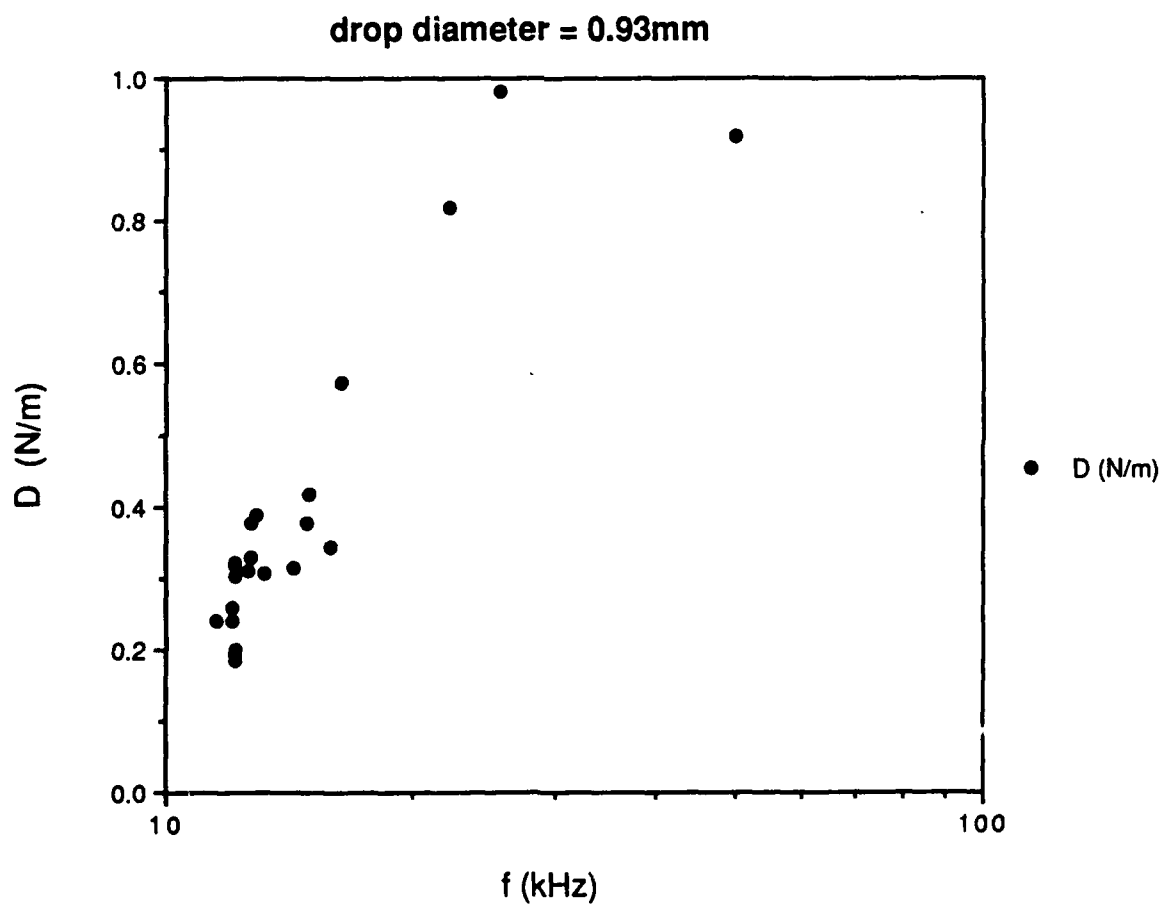
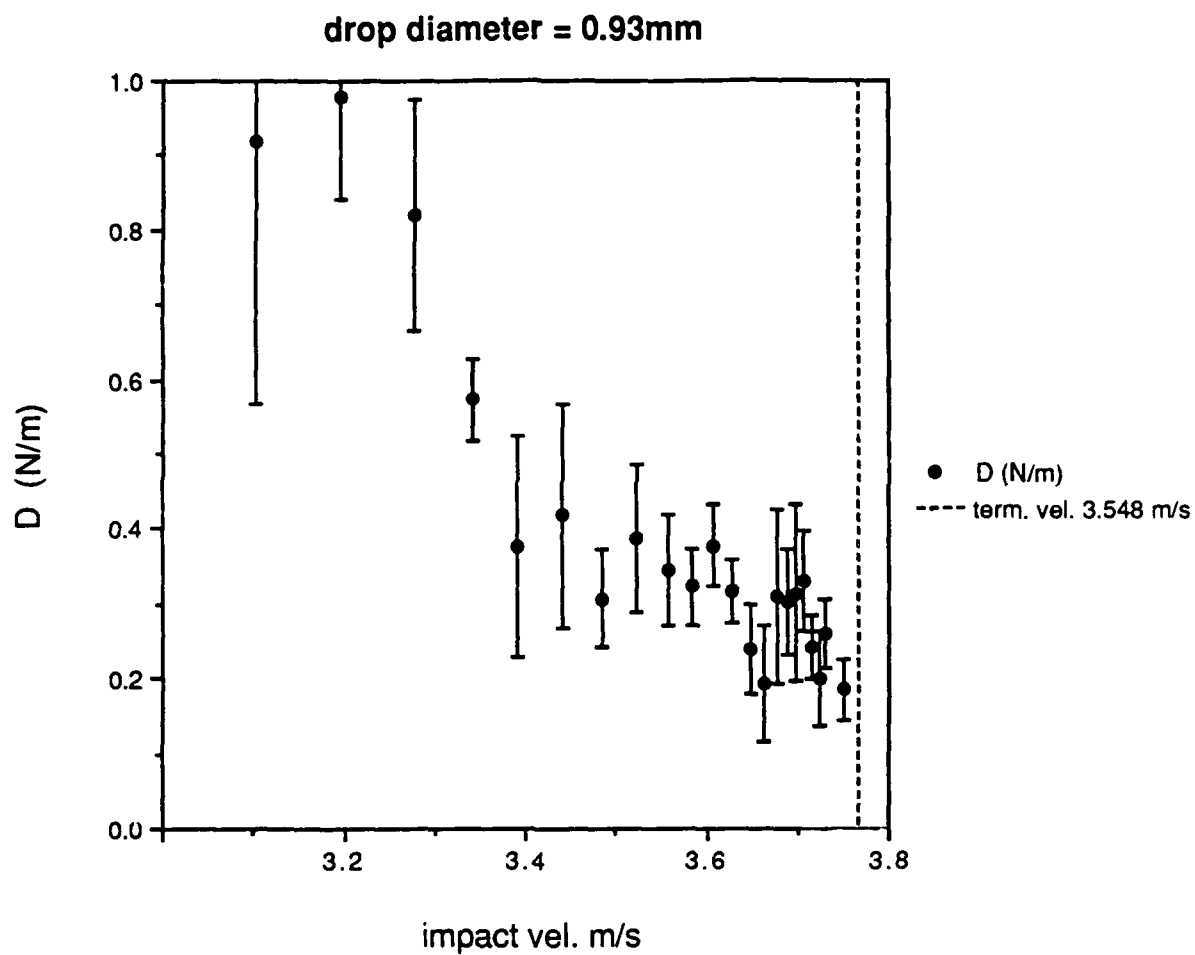


drop diameter = 0.87mm

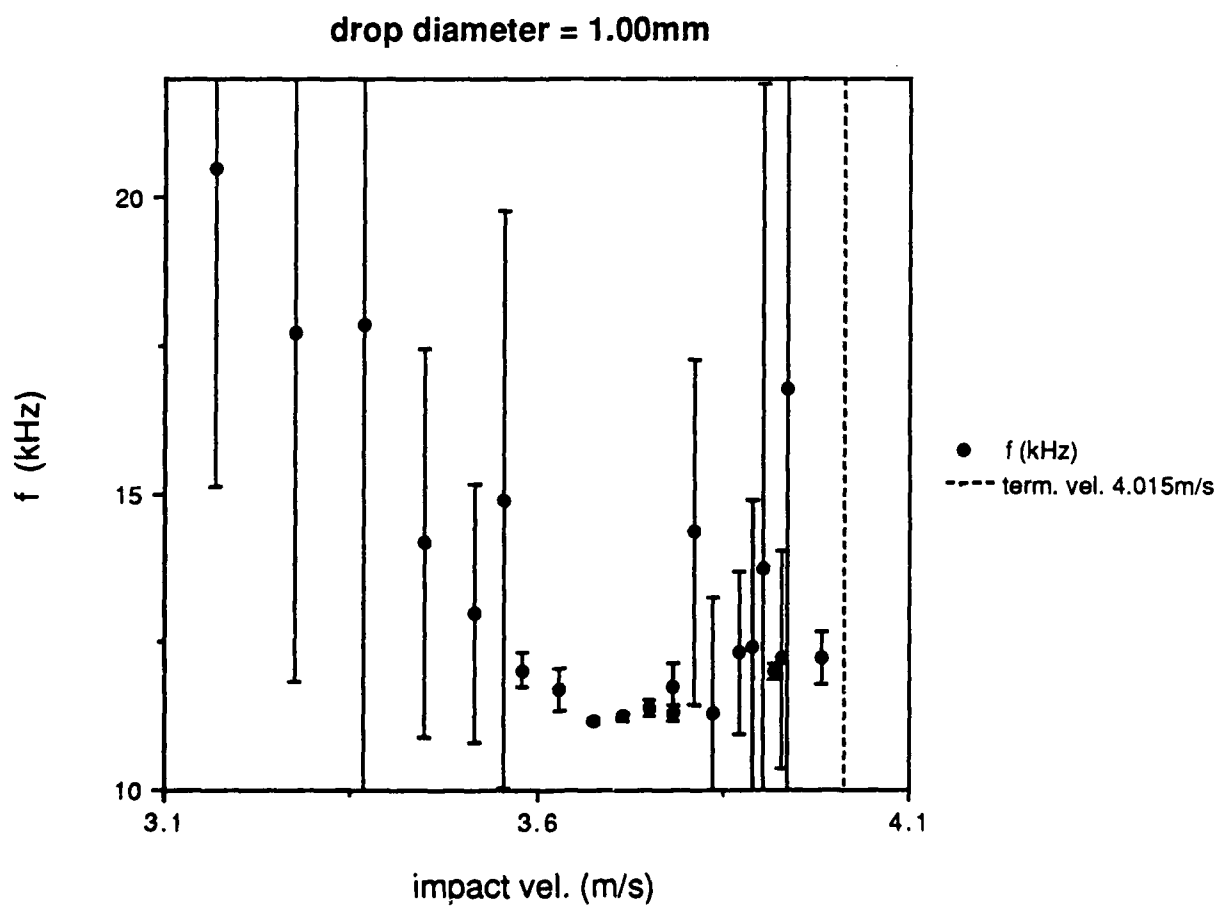
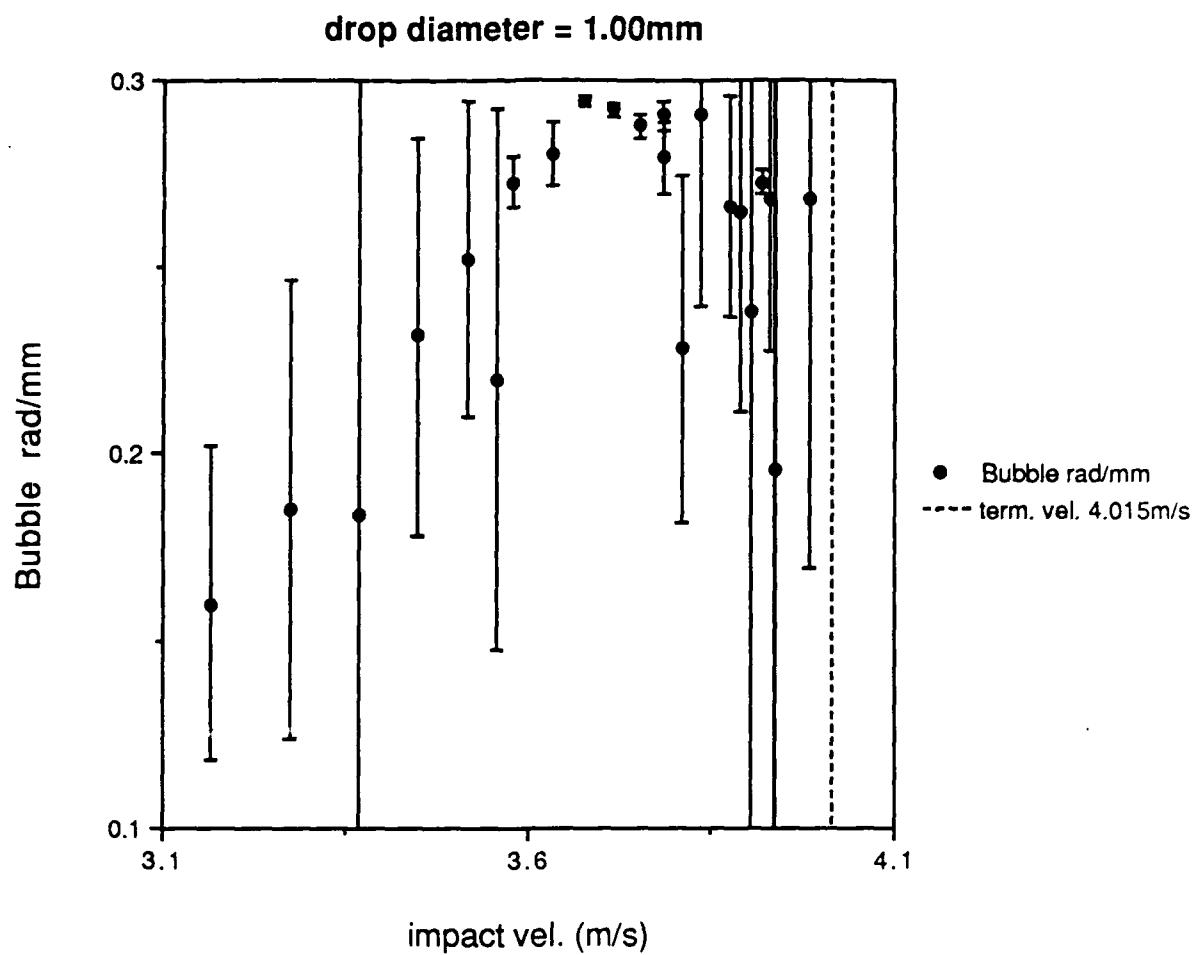


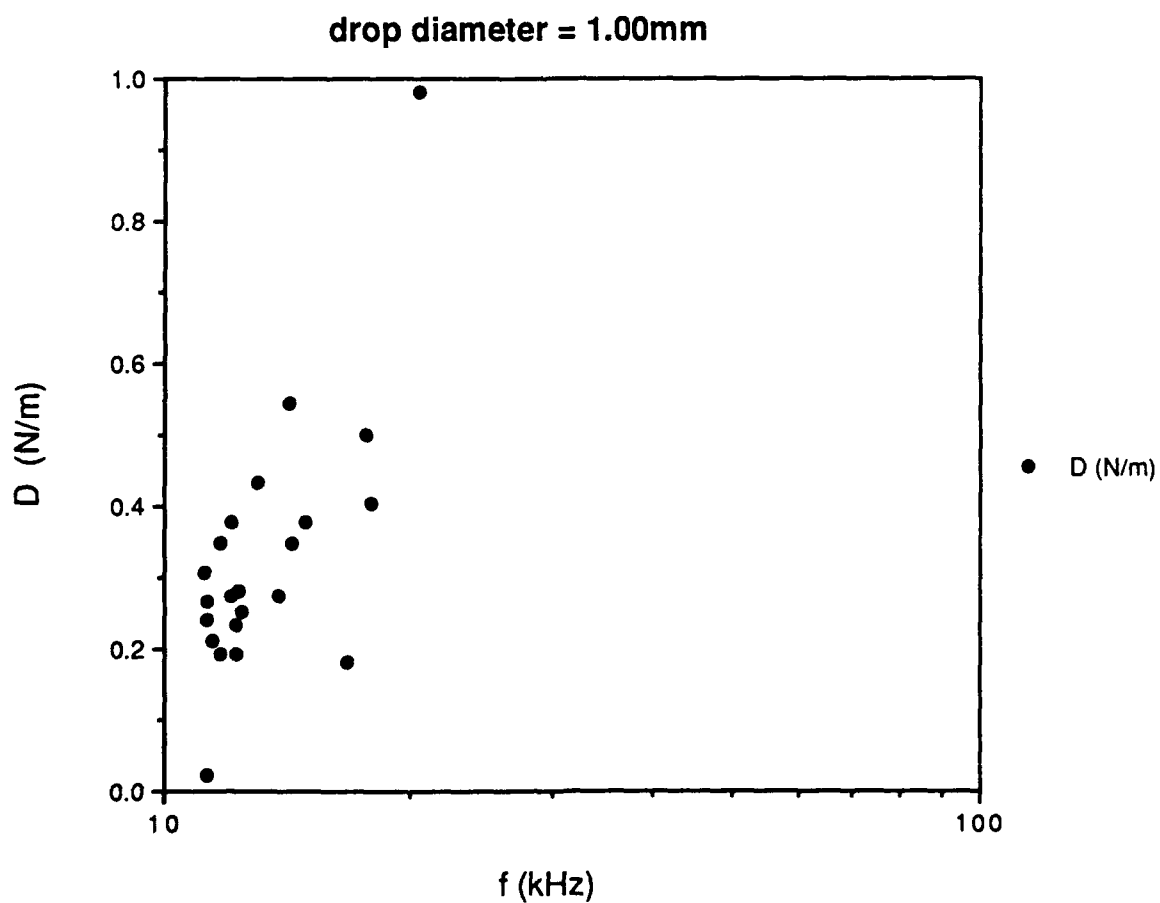
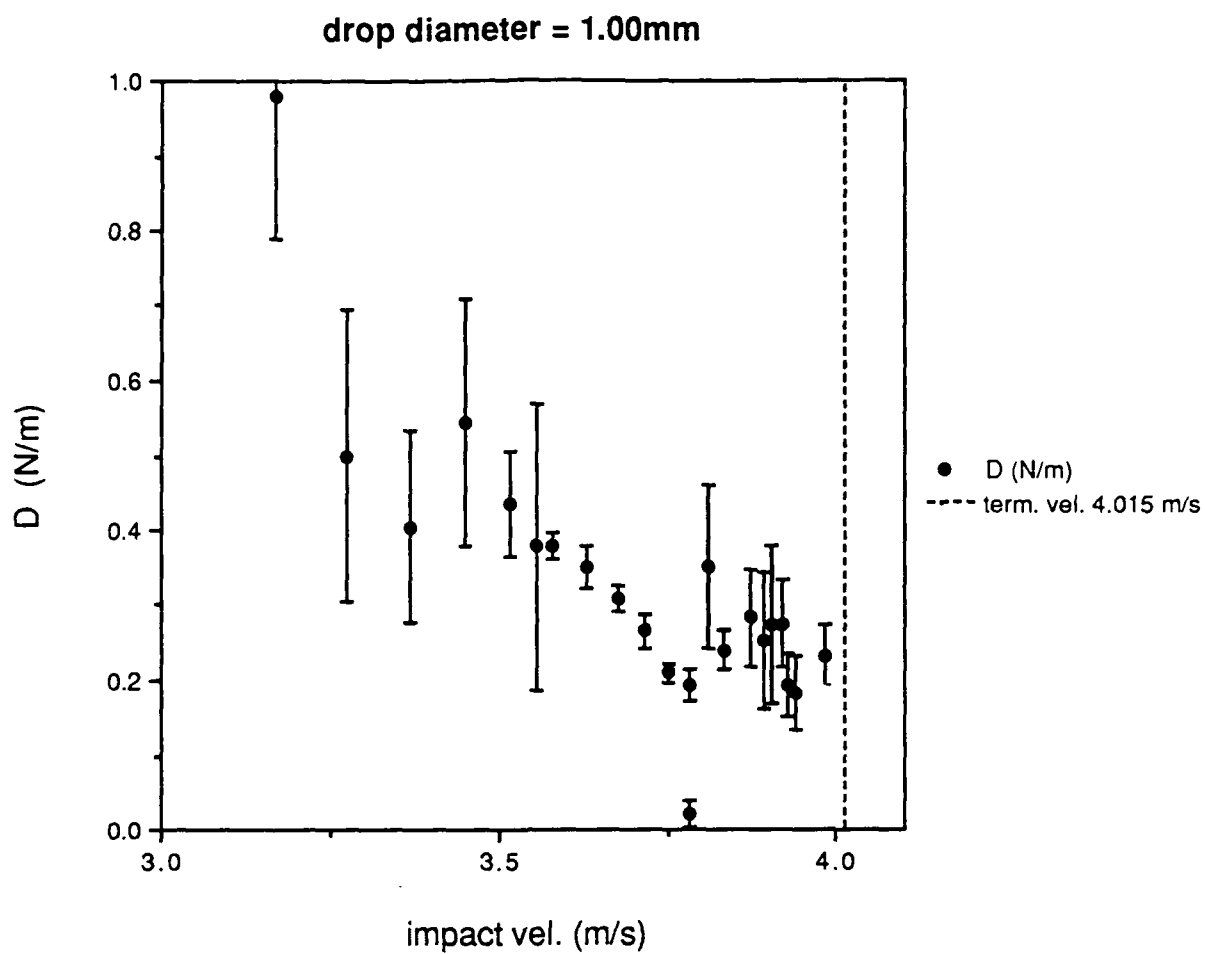
| | impact vel. | f (kHz) | sd of f | D (N/m) | sd of D | Bubble rad/mm | sd of rad |
|----|-------------|---------|---------|---------|---------|---------------|-----------|
| 1 | 3.103 | 49.786 | 10.003 | 0.917 | 0.350 | 0.066 | 0.013 |
| 2 | 3.196 | 25.592 | 7.621 | 0.980 | 0.138 | 0.128 | 0.038 |
| 3 | 3.276 | 22.220 | 8.228 | 0.820 | 0.155 | 0.148 | 0.055 |
| 4 | 3.343 | 16.426 | 1.734 | 0.573 | 0.055 | 0.200 | 0.021 |
| 5 | 3.441 | 14.933 | 2.395 | 0.417 | 0.150 | 0.220 | 0.035 |
| 6 | 3.390 | 14.808 | 3.837 | 0.378 | 0.147 | 0.222 | 0.057 |
| 7 | 3.485 | 13.216 | 1.205 | 0.307 | 0.065 | 0.248 | 0.023 |
| 8 | 3.523 | 12.866 | 2.104 | 0.388 | 0.100 | 0.255 | 0.042 |
| 9 | 3.558 | 15.878 | 18.225 | 0.345 | 0.072 | 0.207 | 0.237 |
| 10 | 3.583 | 12.190 | 0.948 | 0.323 | 0.052 | 0.269 | 0.021 |
| 11 | 3.608 | 12.662 | 1.079 | 0.378 | 0.055 | 0.259 | 0.022 |
| 12 | 3.629 | 12.145 | 0.832 | 0.318 | 0.043 | 0.270 | 0.019 |
| 13 | 3.647 | 11.535 | 2.548 | 0.240 | 0.060 | 0.284 | 0.063 |
| 14 | 3.663 | 12.143 | 1.425 | 0.193 | 0.077 | 0.270 | 0.032 |
| 15 | 3.677 | 12.584 | 2.352 | 0.310 | 0.117 | 0.261 | 0.049 |
| 16 | 3.689 | 12.167 | 1.168 | 0.302 | 0.070 | 0.270 | 0.026 |
| 17 | 3.699 | 14.336 | 8.425 | 0.315 | 0.117 | 0.229 | 0.134 |
| 18 | 3.708 | 12.731 | 1.433 | 0.330 | 0.068 | 0.258 | 0.029 |
| 19 | 3.716 | 12.021 | 0.456 | 0.242 | 0.043 | 0.273 | 0.010 |
| 20 | 3.723 | 12.126 | 0.741 | 0.200 | 0.062 | 0.270 | 0.017 |
| 21 | 3.729 | 12.024 | 0.744 | 0.260 | 0.045 | 0.273 | 0.017 |
| 22 | 3.751 | 12.156 | 0.154 | 0.185 | 0.040 | 0.270 | 0.003 |



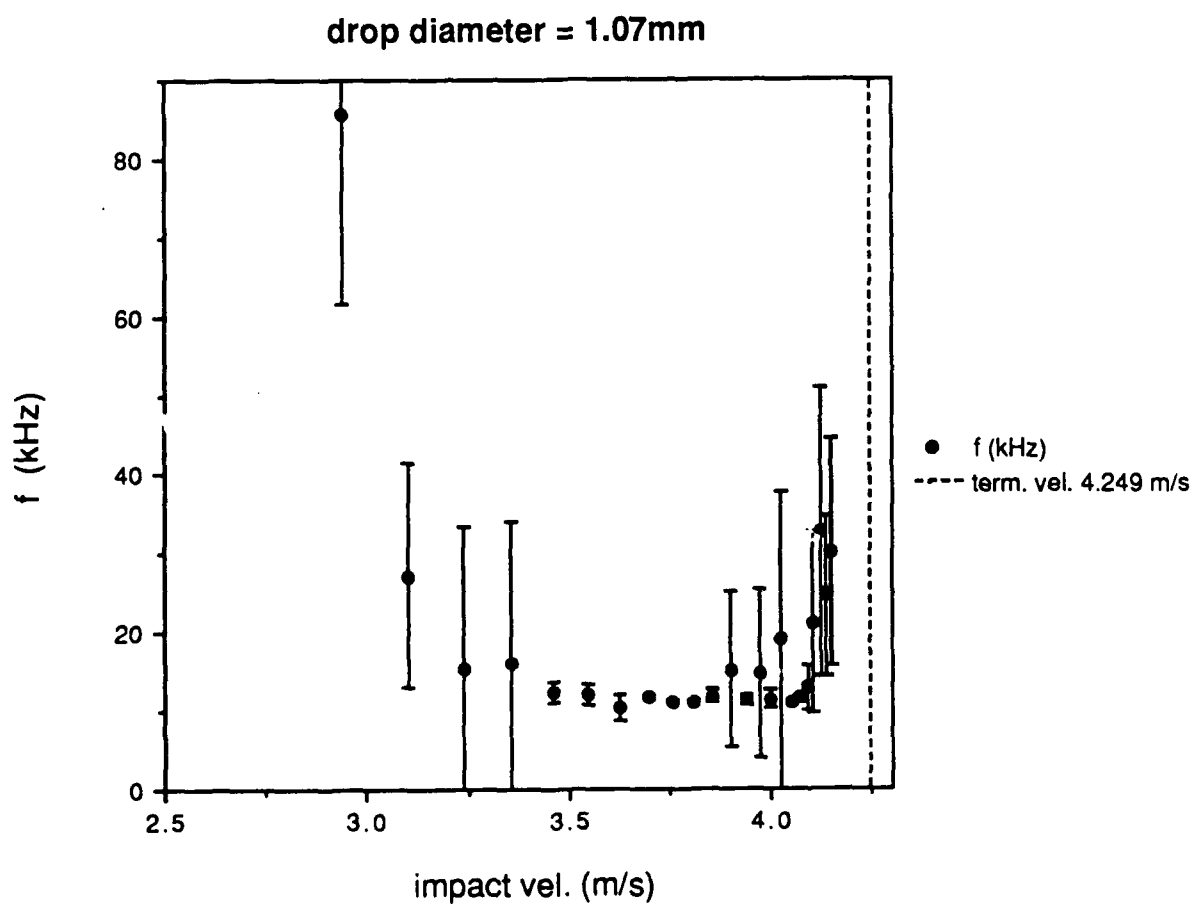
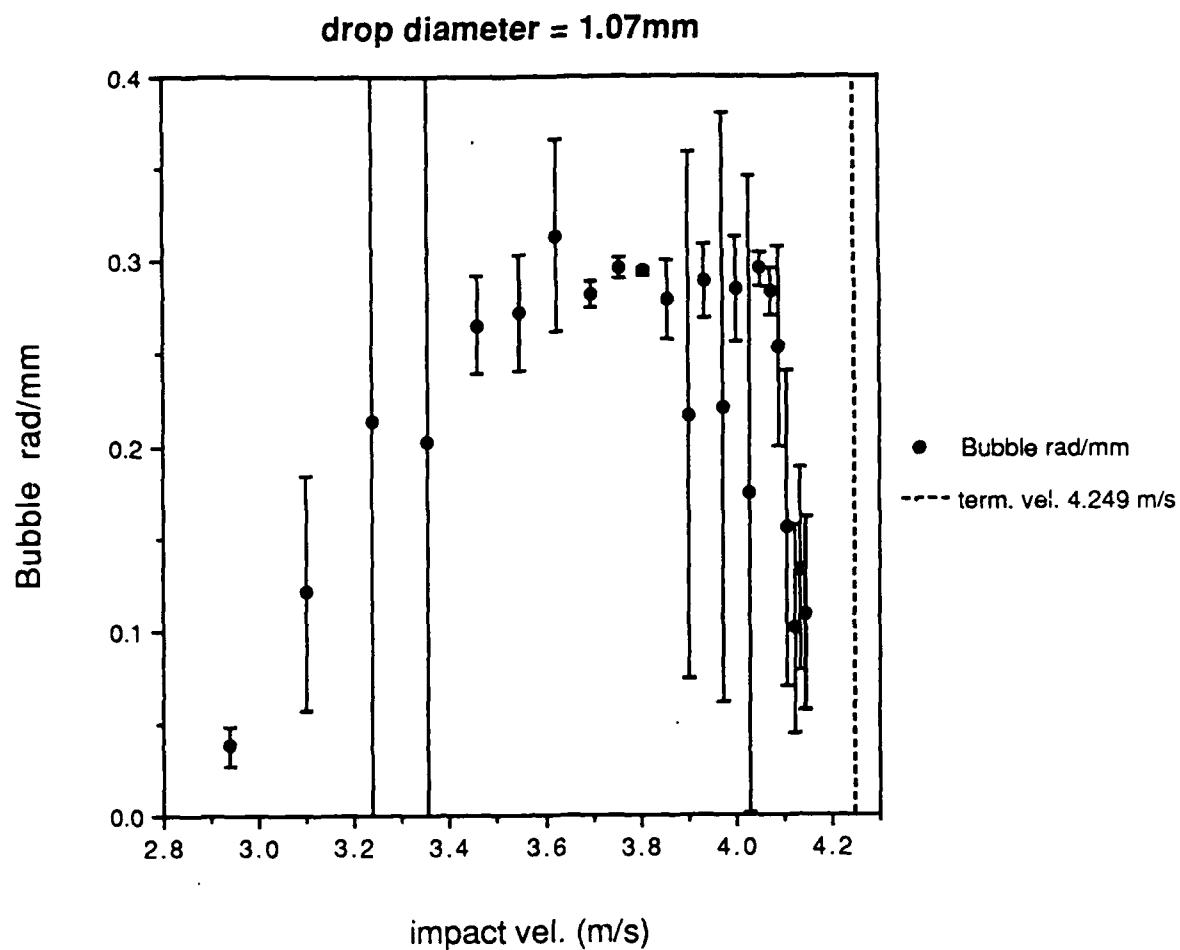


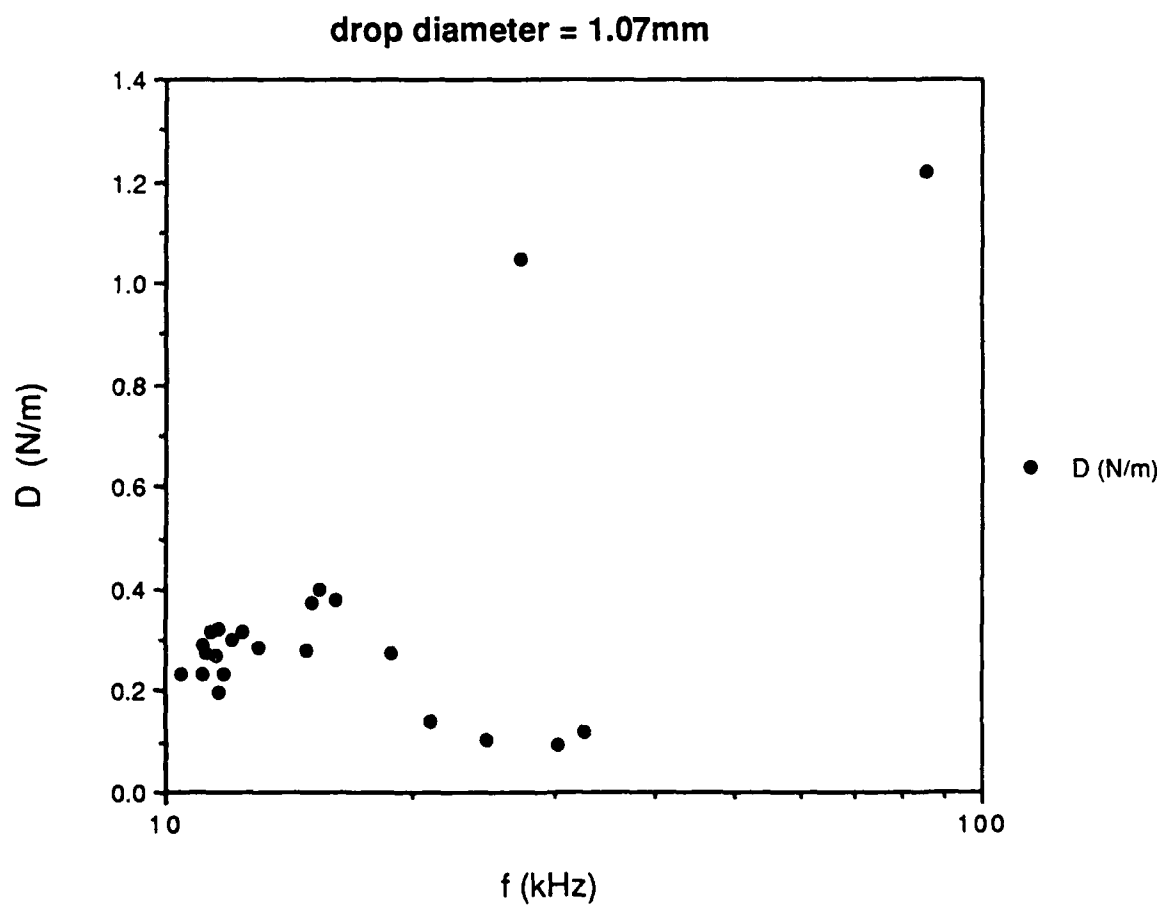
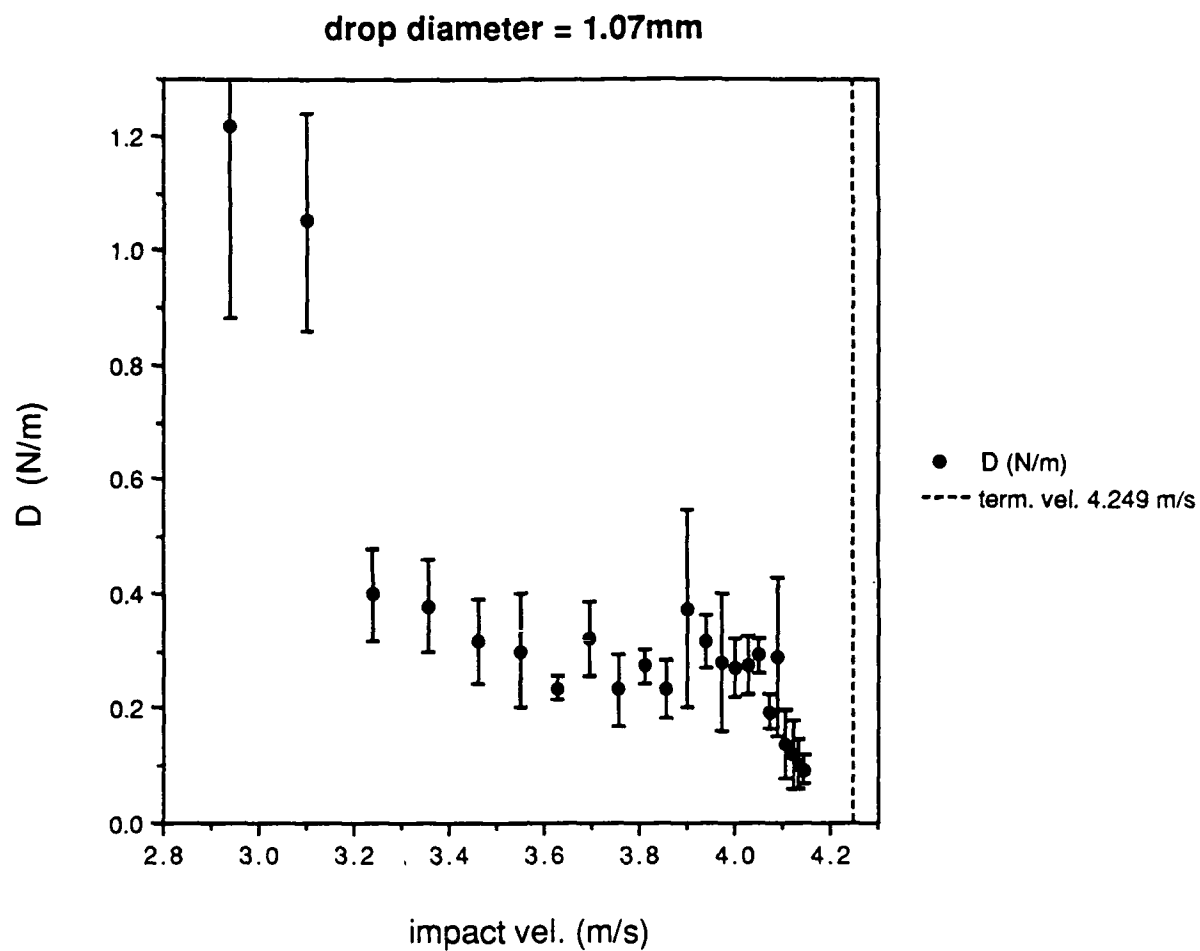
| | impact vel. | f (kHz) | sd of f | D (N/m) | sd of D | Bubble rad/mm | sd of radius |
|----|-------------|---------|---------|---------|---------|---------------|--------------|
| 1 | 3.167 | 20.500 | 5.368 | 0.980 | 0.190 | 0.160 | 0.042 |
| 2 | 3.275 | 17.707 | 5.865 | 0.500 | 0.195 | 0.185 | 0.061 |
| 3 | 3.368 | 17.866 | 12.250 | 0.405 | 0.128 | 0.184 | 0.126 |
| 4 | 3.449 | 14.174 | 3.267 | 0.545 | 0.165 | 0.231 | 0.053 |
| 5 | 3.518 | 13.000 | 2.184 | 0.435 | 0.070 | 0.252 | 0.042 |
| 6 | 3.579 | 12.022 | 0.282 | 0.378 | 0.018 | 0.273 | 0.006 |
| 7 | 3.631 | 11.703 | 0.366 | 0.350 | 0.028 | 0.280 | 0.009 |
| 8 | 3.677 | 11.148 | 0.050 | 0.307 | 0.018 | 0.294 | 0.001 |
| 9 | 3.717 | 11.233 | 0.063 | 0.265 | 0.022 | 0.292 | 0.002 |
| 10 | 3.753 | 11.401 | 0.138 | 0.210 | 0.013 | 0.288 | 0.003 |
| 11 | 3.784 | 11.291 | 0.153 | 0.021 | 0.018 | 0.290 | 0.004 |
| 12 | 3.784 | 11.733 | 0.400 | 0.193 | 0.020 | 0.280 | 0.010 |
| 13 | 3.811 | 14.365 | 2.923 | 0.350 | 0.109 | 0.228 | 0.046 |
| 14 | 3.835 | 11.287 | 1.988 | 0.240 | 0.028 | 0.291 | 0.051 |
| 15 | 3.556 | 14.906 | 4.876 | 0.378 | 0.190 | 0.220 | 0.072 |
| 16 | 3.874 | 12.321 | 1.370 | 0.282 | 0.065 | 0.266 | 0.030 |
| 17 | 3.891 | 12.403 | 2.505 | 0.253 | 0.092 | 0.264 | 0.053 |
| 18 | 3.905 | 13.763 | 8.163 | 0.275 | 0.105 | 0.238 | 0.141 |
| 19 | 3.918 | 12.023 | 0.138 | 0.275 | 0.058 | 0.273 | 0.003 |
| 20 | 3.929 | 12.215 | 1.863 | 0.193 | 0.043 | 0.269 | 0.041 |
| 21 | 3.938 | 16.768 | 16.502 | 0.182 | 0.048 | 0.196 | 0.193 |
| 22 | 3.983 | 12.217 | 0.449 | 0.233 | 0.040 | 0.268 | 0.099 |



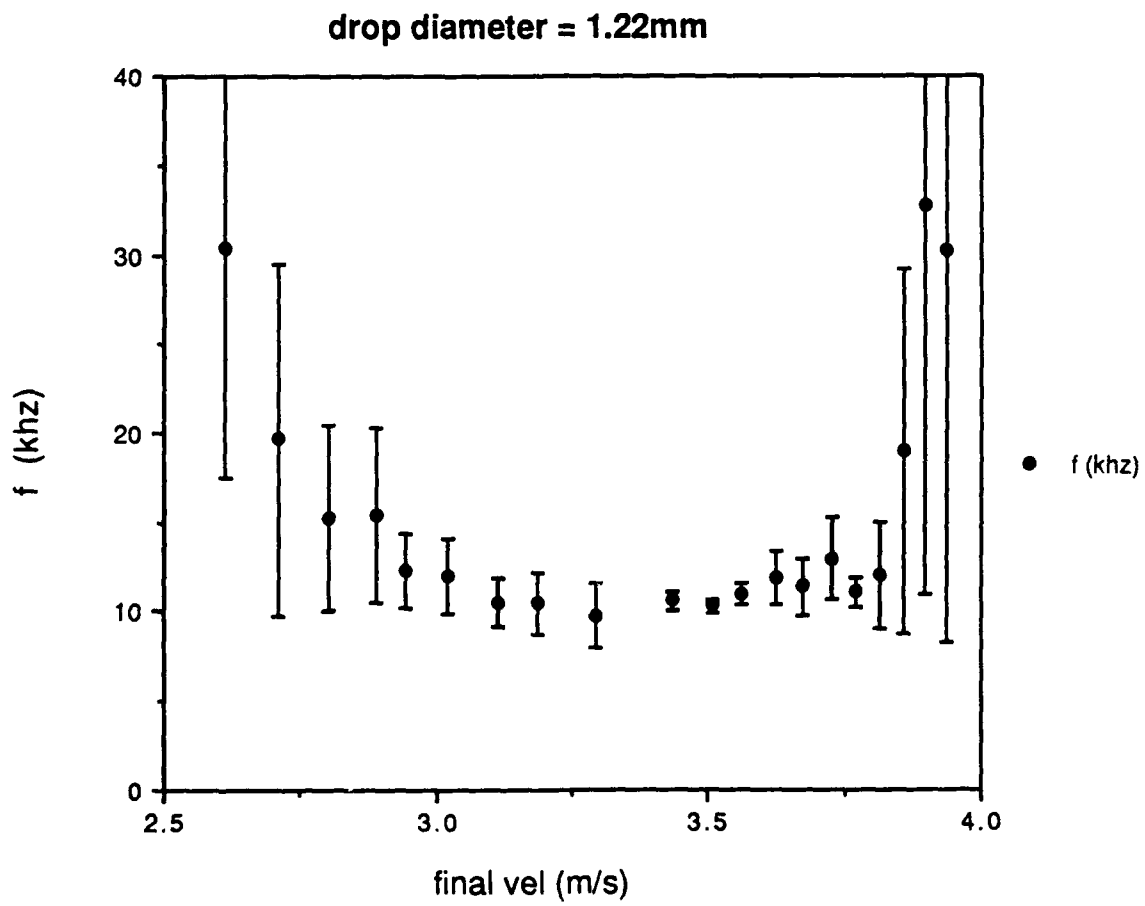
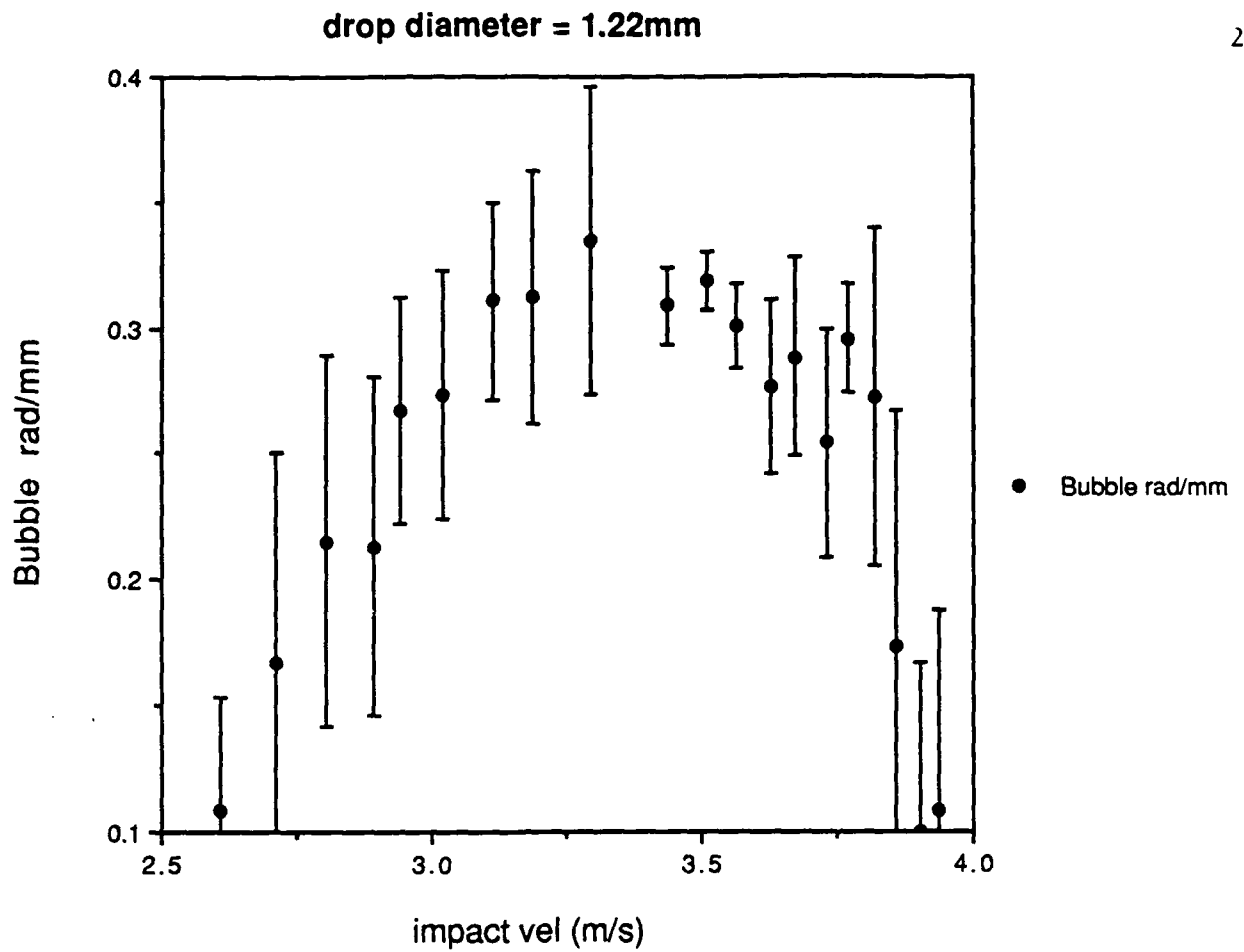


| | impact vel. | f (kHz) | sd of f | D (N/m) | sd of D | Bubble rad/mm | sd of rad | 18 |
|----|-------------|---------|---------|---------|---------|---------------|-----------|----|
| 1 | 2.941 | 85.753 | 24.074 | 1.218 | 0.335 | 0.038 | 0.011 | |
| 2 | 3.101 | 27.208 | 14.211 | 1.050 | 0.193 | 0.121 | 0.063 | |
| 3 | 3.238 | 15.391 | 17.903 | 0.398 | 0.083 | 0.213 | 0.248 | |
| 4 | 3.356 | 16.186 | 18.079 | 0.378 | 0.080 | 0.203 | 0.226 | |
| 5 | 3.459 | 12.376 | 1.224 | 0.318 | 0.075 | 0.265 | 0.026 | |
| 6 | 3.549 | 12.064 | 1.409 | 0.300 | 0.098 | 0.272 | 0.032 | |
| 7 | 3.627 | 10.455 | 1.742 | 0.235 | 0.020 | 0.314 | 0.052 | |
| 8 | 3.696 | 11.616 | 0.298 | 0.320 | 0.065 | 0.282 | 0.007 | |
| 9 | 3.757 | 11.080 | 0.202 | 0.233 | 0.062 | 0.296 | 0.005 | |
| 10 | 3.810 | 11.152 | 0.101 | 0.275 | 0.030 | 0.294 | 0.003 | |
| 11 | 3.858 | 11.764 | 0.888 | 0.235 | 0.050 | 0.279 | 0.021 | |
| 12 | 3.900 | 15.138 | 9.947 | 0.372 | 0.172 | 0.217 | 0.142 | |
| 13 | 3.937 | 11.346 | 0.805 | 0.318 | 0.048 | 0.289 | 0.021 | |
| 14 | 3.971 | 14.851 | 10.727 | 0.280 | 0.117 | 0.221 | 0.160 | |
| 15 | 4.000 | 11.506 | 1.139 | 0.270 | 0.050 | 0.285 | 0.028 | |
| 16 | 4.027 | 18.925 | 18.821 | 0.275 | 0.050 | 0.173 | 0.172 | |
| 17 | 4.050 | 11.097 | 0.359 | 0.292 | 0.030 | 0.296 | 0.010 | |
| 18 | 4.090 | 12.949 | 2.745 | 0.287 | 0.138 | 0.253 | 0.054 | |
| 19 | 4.071 | 11.599 | 0.524 | 0.195 | 0.030 | 0.283 | 0.013 | |
| 20 | 4.106 | 21.123 | 11.572 | 0.138 | 0.060 | 0.155 | 0.085 | |
| 21 | 4.121 | 32.643 | 18.186 | 0.117 | 0.060 | 0.100 | 0.056 | |
| 22 | 4.136 | 24.655 | 10.258 | 0.102 | 0.045 | 0.133 | 0.055 | |
| 23 | 4.147 | 30.209 | 14.412 | 0.092 | 0.025 | 0.109 | 0.052 | |

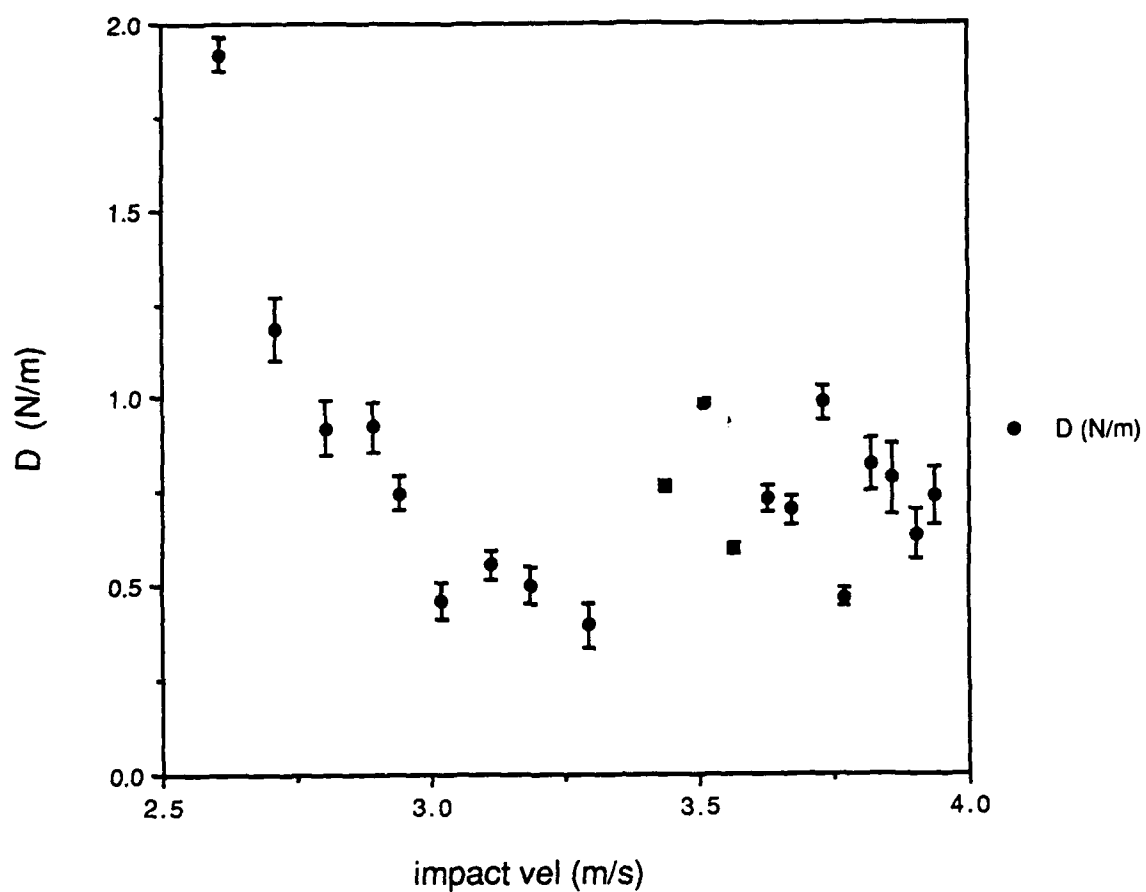




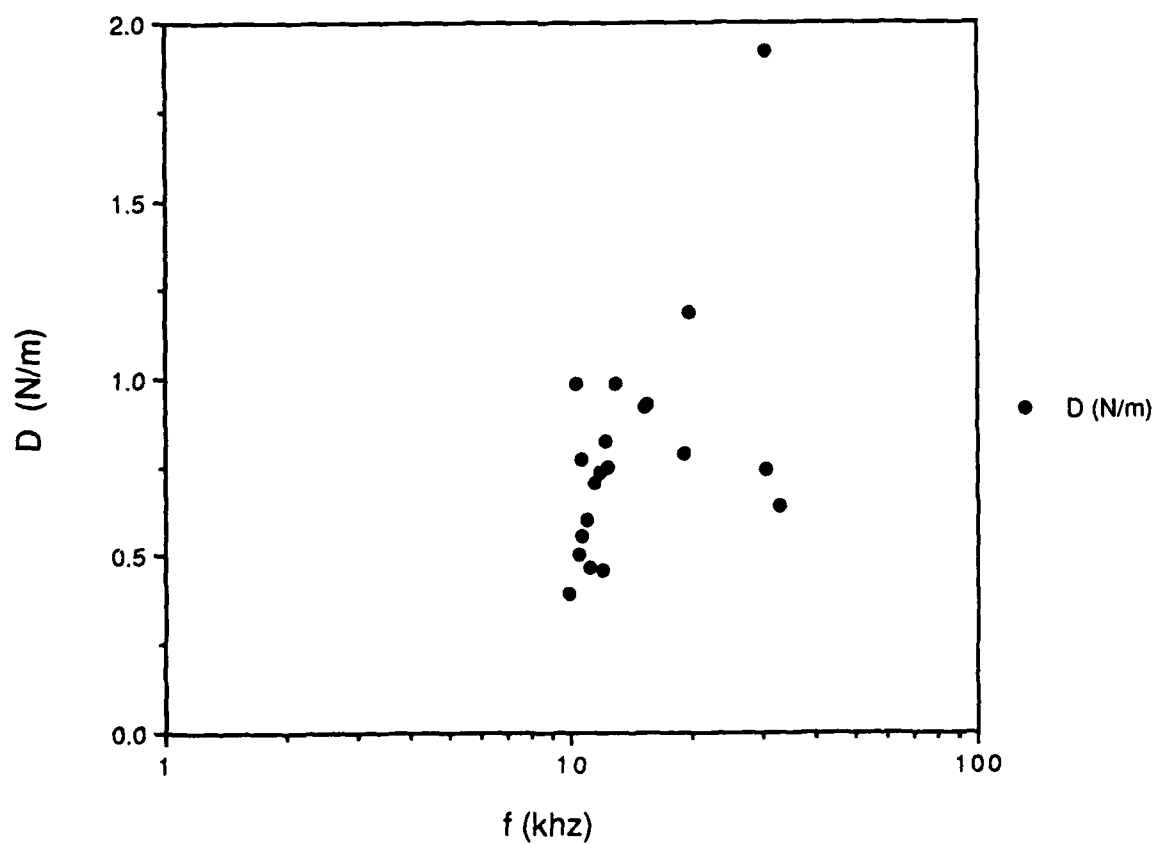
| | impact vel | f (khz) | sd of f | D (N/m) | sd of D | Bubble rad/mm | sd of rad |
|----|------------|---------|---------|---------|---------|---------------|-----------|
| 1 | 2.610 | 30.372 | 12.849 | 1.917 | 0.149 | 0.108 | 0.046 |
| 2 | 2.711 | 19.664 | 9.813 | 1.186 | 0.230 | 0.167 | 0.083 |
| 3 | 2.804 | 15.230 | 5.225 | 0.922 | 0.193 | 0.215 | 0.074 |
| 4 | 2.891 | 15.389 | 4.861 | 0.925 | 0.229 | 0.213 | 0.067 |
| 5 | 2.943 | 12.266 | 2.049 | 0.747 | 0.158 | 0.267 | 0.045 |
| 6 | 3.022 | 11.996 | 2.139 | 0.461 | 0.178 | 0.273 | 0.049 |
| 7 | 3.114 | 10.558 | 1.343 | 0.554 | 0.124 | 0.311 | 0.040 |
| 8 | 3.188 | 10.505 | 1.695 | 0.502 | 0.097 | 0.312 | 0.050 |
| 9 | 3.508 | 10.312 | 0.370 | 0.985 | 0.166 | 0.318 | 0.011 |
| 10 | 3.625 | 11.857 | 1.483 | 0.731 | 0.158 | 0.277 | 0.035 |
| 11 | 3.729 | 12.894 | 2.298 | 0.988 | 0.218 | 0.254 | 0.045 |
| 12 | 3.294 | 9.814 | 1.794 | 0.394 | 0.063 | 0.334 | 0.061 |
| 13 | 3.436 | 10.630 | 0.515 | 0.769 | 0.115 | 0.309 | 0.015 |
| 14 | 3.562 | 10.923 | 0.610 | 0.599 | 0.076 | 0.300 | 0.017 |
| 15 | 3.673 | 11.363 | 1.547 | 0.702 | 0.086 | 0.289 | 0.039 |
| 16 | 3.772 | 11.094 | 0.809 | 0.470 | 0.119 | 0.296 | 0.022 |
| 17 | 3.817 | 12.056 | 2.968 | 0.823 | 0.189 | 0.272 | 0.067 |
| 18 | 3.860 | 18.911 | 10.219 | 0.785 | 0.211 | 0.173 | 0.094 |
| 19 | 3.900 | 32.727 | 21.765 | 0.635 | 0.247 | 0.100 | 0.067 |
| 20 | 3.935 | 30.154 | 21.827 | 0.740 | 0.290 | 0.109 | 0.079 |



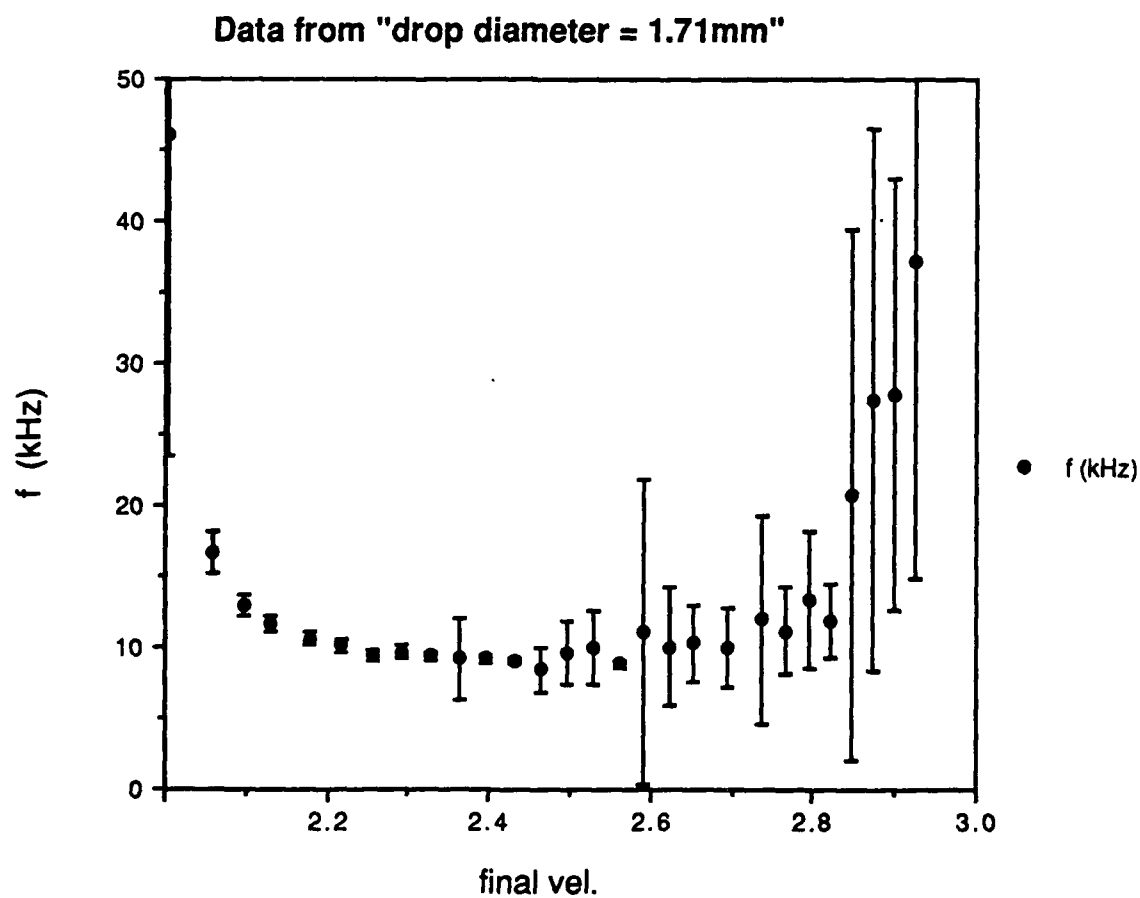
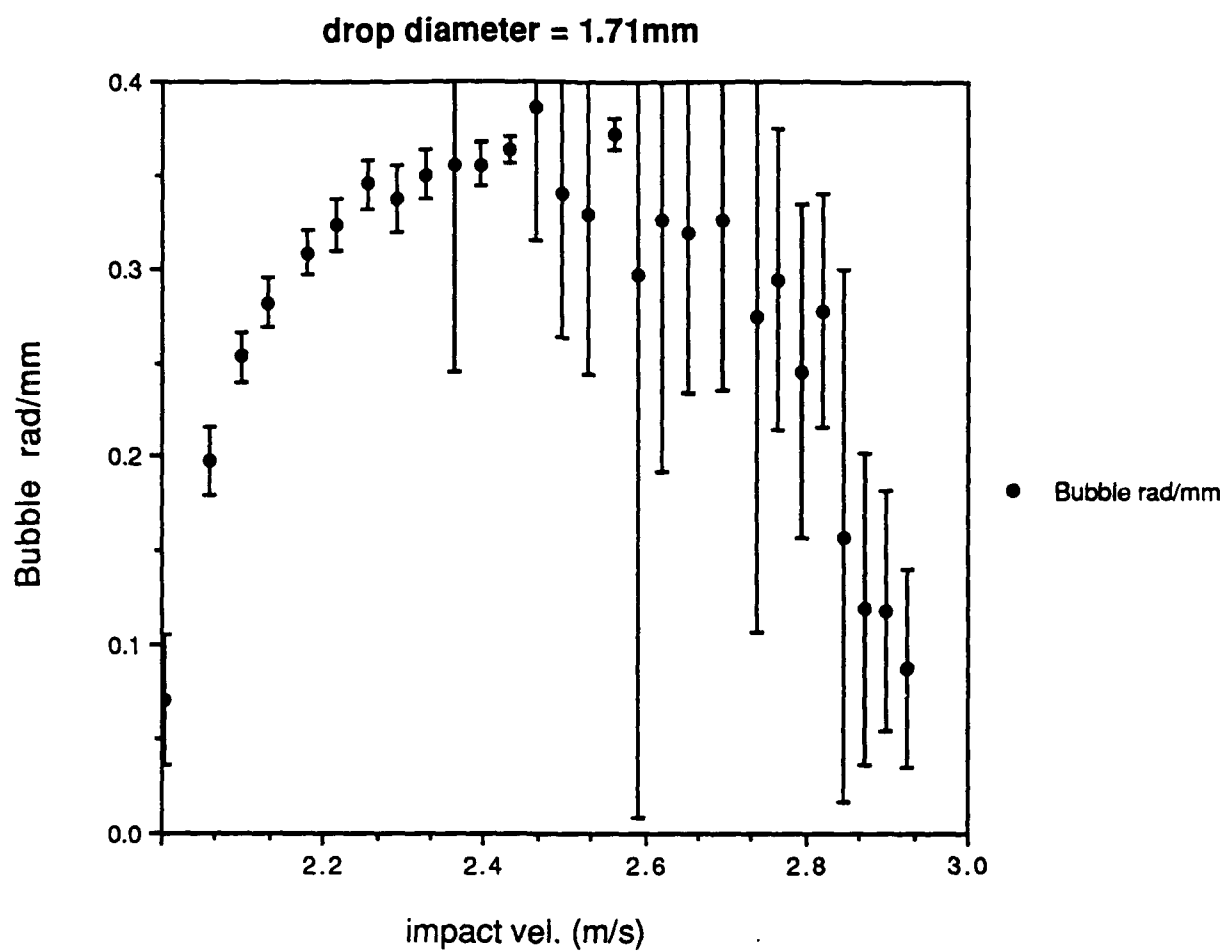
drop diameter = 1.22mm

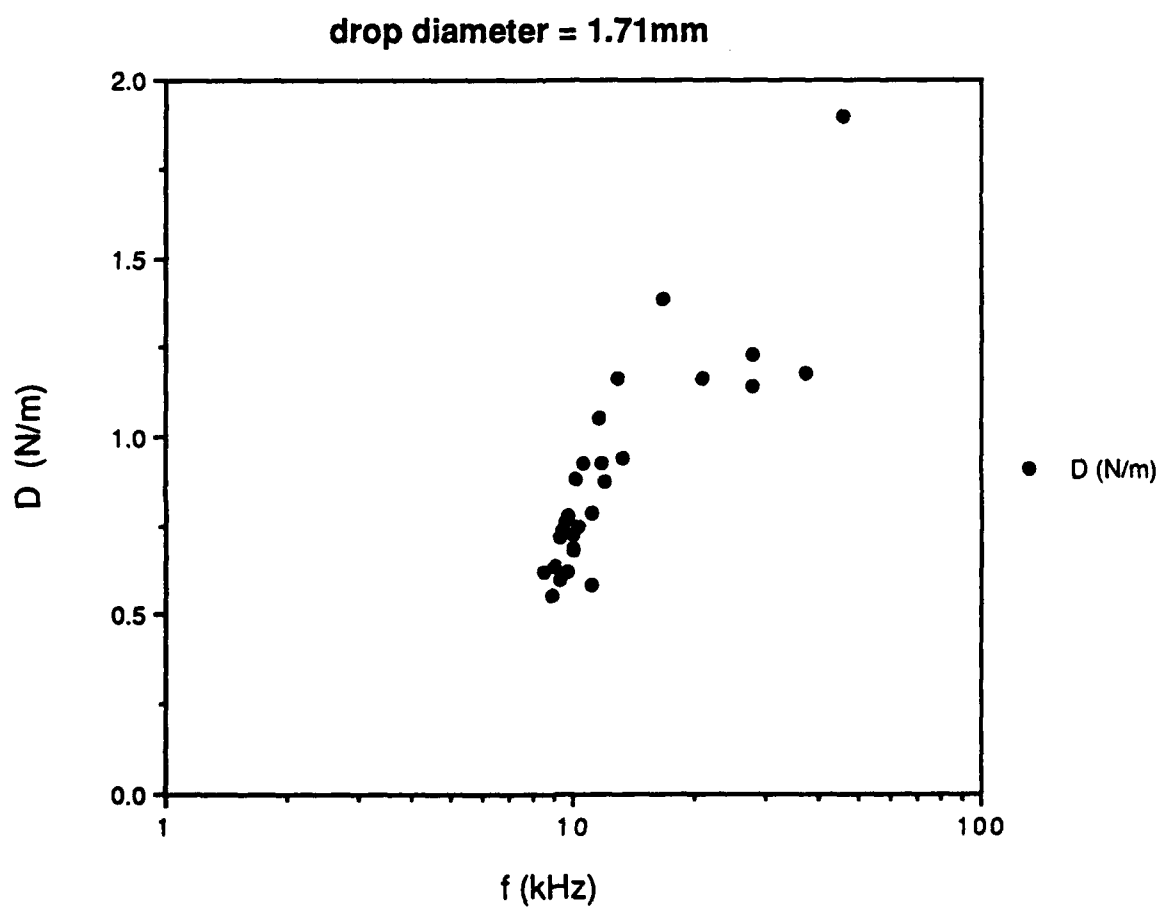
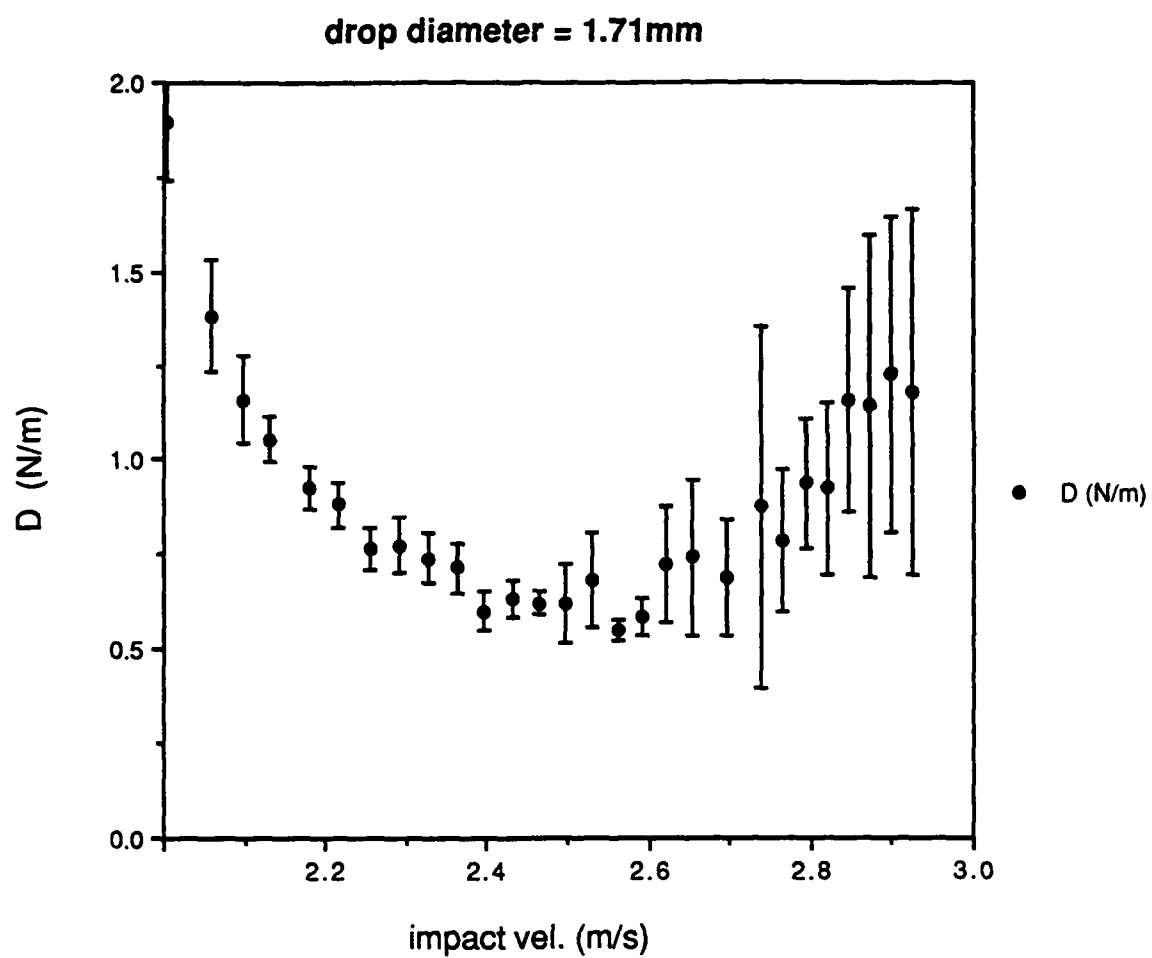


drop diameter = 1.22mm



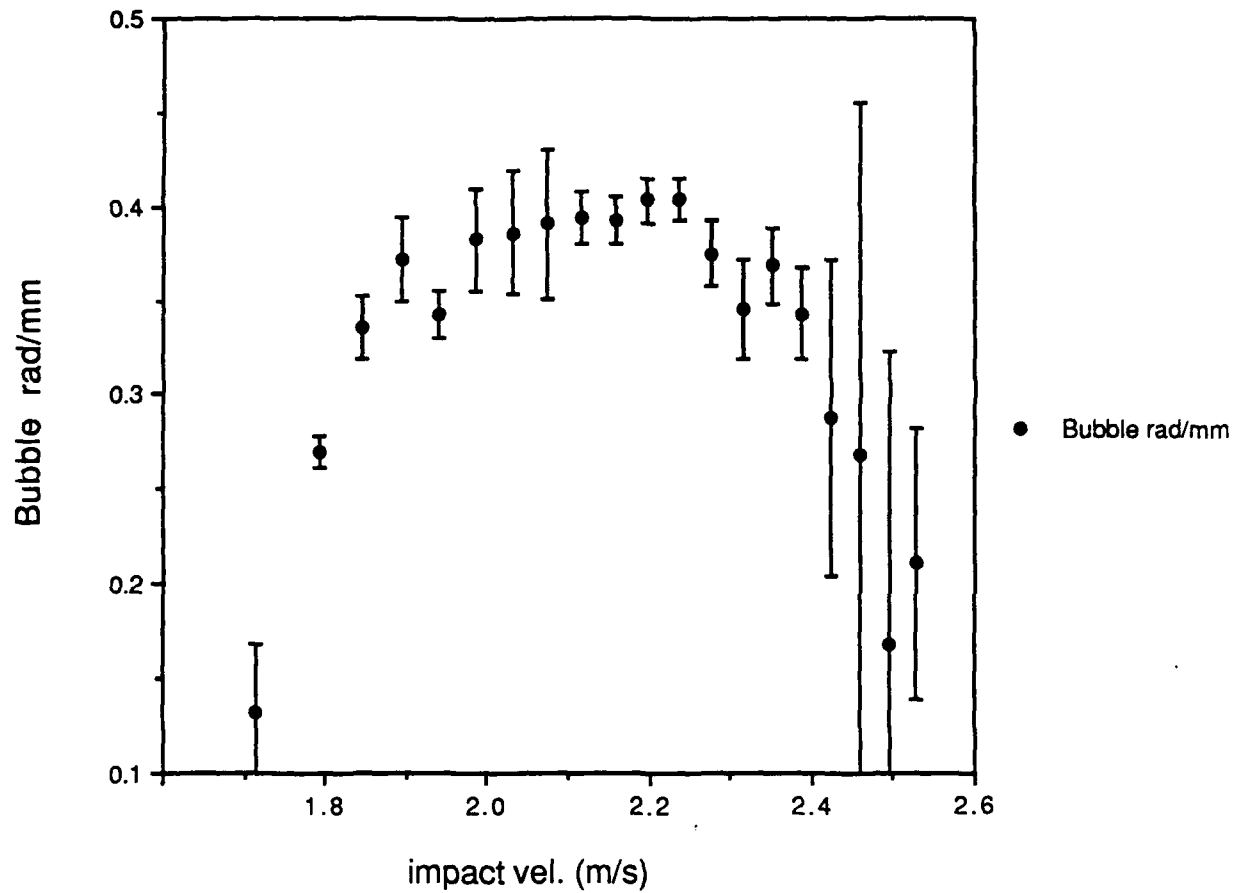
| | final vel. | f (kHz) | sd of f | D (N/m) | sd of D | Bubble rad/mm | sd of rad |
|----|------------|---------|---------|---------|---------|---------------|-----------|
| 1 | 2.004 | 46.174 | 22.574 | 1.897 | 0.155 | 0.071 | 0.035 |
| 2 | 2.058 | 16.600 | 1.505 | 1.383 | 0.147 | 0.198 | 0.018 |
| 3 | 2.099 | 12.964 | 0.705 | 1.160 | 0.117 | 0.253 | 0.014 |
| 4 | 2.130 | 11.639 | 0.538 | 1.055 | 0.058 | 0.282 | 0.013 |
| 5 | 2.179 | 10.637 | 0.418 | 0.927 | 0.058 | 0.308 | 0.012 |
| 6 | 2.217 | 10.140 | 0.423 | 0.883 | 0.060 | 0.323 | 0.013 |
| 7 | 2.255 | 9.492 | 0.365 | 0.765 | 0.058 | 0.346 | 0.013 |
| 8 | 2.292 | 9.718 | 0.526 | 0.775 | 0.072 | 0.338 | 0.018 |
| 9 | 2.328 | 9.362 | 0.340 | 0.740 | 0.065 | 0.350 | 0.013 |
| 10 | 2.363 | 9.233 | 2.850 | 0.715 | 0.065 | 0.355 | 0.110 |
| 11 | 2.397 | 9.211 | 0.317 | 0.600 | 0.052 | 0.356 | 0.012 |
| 12 | 2.431 | 9.029 | 0.169 | 0.635 | 0.048 | 0.363 | 0.007 |
| 13 | 2.465 | 8.482 | 1.582 | 0.623 | 0.033 | 0.387 | 0.072 |
| 14 | 2.497 | 9.657 | 2.164 | 0.620 | 0.102 | 0.340 | 0.076 |
| 15 | 2.529 | 9.954 | 2.579 | 0.682 | 0.122 | 0.330 | 0.085 |
| 16 | 2.561 | 8.807 | 0.199 | 0.552 | 0.028 | 0.372 | 0.008 |
| 17 | 2.591 | 11.070 | 10.737 | 0.585 | 0.050 | 0.296 | 0.287 |
| 18 | 2.622 | 10.069 | 4.126 | 0.723 | 0.152 | 0.326 | 0.133 |
| 19 | 2.652 | 10.294 | 2.728 | 0.745 | 0.205 | 0.319 | 0.084 |
| 20 | 2.695 | 10.048 | 2.780 | 0.690 | 0.150 | 0.326 | 0.090 |
| 21 | 2.738 | 11.946 | 7.300 | 0.875 | 0.480 | 0.275 | 0.168 |
| 22 | 2.766 | 11.141 | 3.031 | 0.787 | 0.190 | 0.294 | 0.080 |
| 23 | 2.794 | 13.340 | 4.817 | 0.938 | 0.172 | 0.246 | 0.089 |
| 24 | 2.821 | 11.810 | 2.631 | 0.925 | 0.225 | 0.278 | 0.062 |
| 25 | 2.847 | 20.767 | 18.640 | 1.160 | 0.295 | 0.158 | 0.142 |
| 26 | 2.874 | 27.478 | 19.067 | 1.143 | 0.453 | 0.119 | 0.083 |
| 27 | 2.900 | 27.783 | 15.139 | 1.228 | 0.417 | 0.118 | 0.064 |
| 28 | 2.925 | 37.226 | 22.462 | 1.180 | 0.485 | 0.088 | 0.053 |



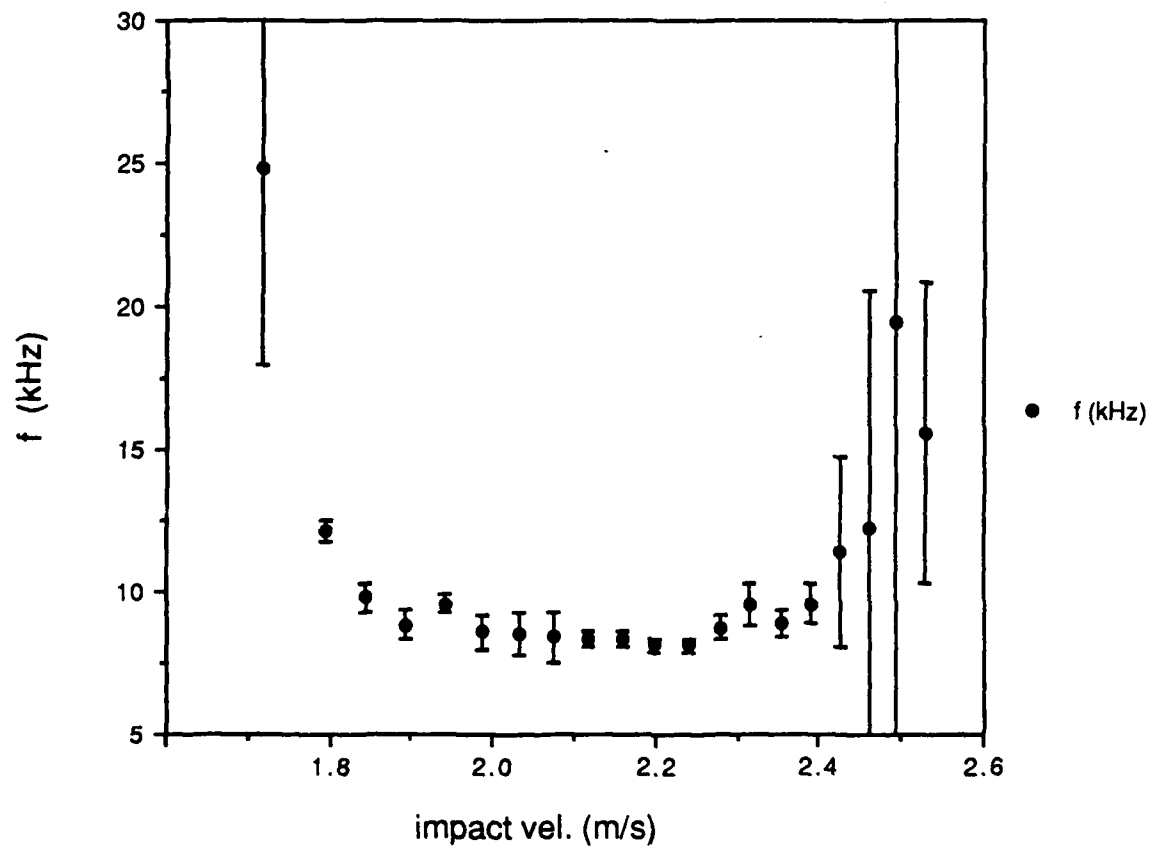


| | impact vel. | f (kHz) | sd of f | D (N/m) | sd of D | Bubble rad/mm | sd of rad |
|----|-------------|---------|---------|---------|---------|---------------|-----------|
| 1 | 1.716 | 24.796 | 6.820 | 0.510 | 0.155 | 0.132 | 0.036 |
| 2 | 1.794 | 12.134 | 0.390 | 0.613 | 0.022 | 0.270 | 0.009 |
| 3 | 1.845 | 9.786 | 0.487 | 0.603 | 0.033 | 0.335 | 0.017 |
| 4 | 1.893 | 8.827 | 0.530 | 0.647 | 0.022 | 0.372 | 0.022 |
| 5 | 1.940 | 9.573 | 0.346 | 0.647 | 0.028 | 0.343 | 0.012 |
| 6 | 1.986 | 8.580 | 0.615 | 0.657 | 0.025 | 0.382 | 0.027 |
| 7 | 2.031 | 8.496 | 0.723 | 0.640 | 0.033 | 0.386 | 0.033 |
| 8 | 2.074 | 8.389 | 0.850 | 0.585 | 0.055 | 0.391 | 0.040 |
| 9 | 2.117 | 8.325 | 0.307 | 0.600 | 0.052 | 0.394 | 0.015 |
| 10 | 2.158 | 8.346 | 0.262 | 0.713 | 0.040 | 0.393 | 0.012 |
| 11 | 2.199 | 8.128 | 0.238 | 0.735 | 0.035 | 0.404 | 0.012 |
| 12 | 2.238 | 8.115 | 0.219 | 0.708 | 0.022 | 0.404 | 0.011 |
| 13 | 2.277 | 8.745 | 0.413 | 0.743 | 0.028 | 0.375 | 0.018 |
| 14 | 2.315 | 9.510 | 0.731 | 0.760 | 0.058 | 0.345 | 0.027 |
| 15 | 2.352 | 8.905 | 0.493 | 0.762 | 0.037 | 0.368 | 0.020 |
| 16 | 2.389 | 9.558 | 0.696 | 0.818 | 0.030 | 0.343 | 0.025 |
| 17 | 2.424 | 11.381 | 3.320 | 0.843 | 0.065 | 0.288 | 0.084 |
| 18 | 2.459 | 12.179 | 8.389 | 0.828 | 0.110 | 0.269 | 0.186 |
| 19 | 2.494 | 19.439 | 17.760 | 0.825 | 0.230 | 0.169 | 0.154 |
| 20 | 2.528 | 15.525 | 5.281 | 0.973 | 0.215 | 0.211 | 0.072 |

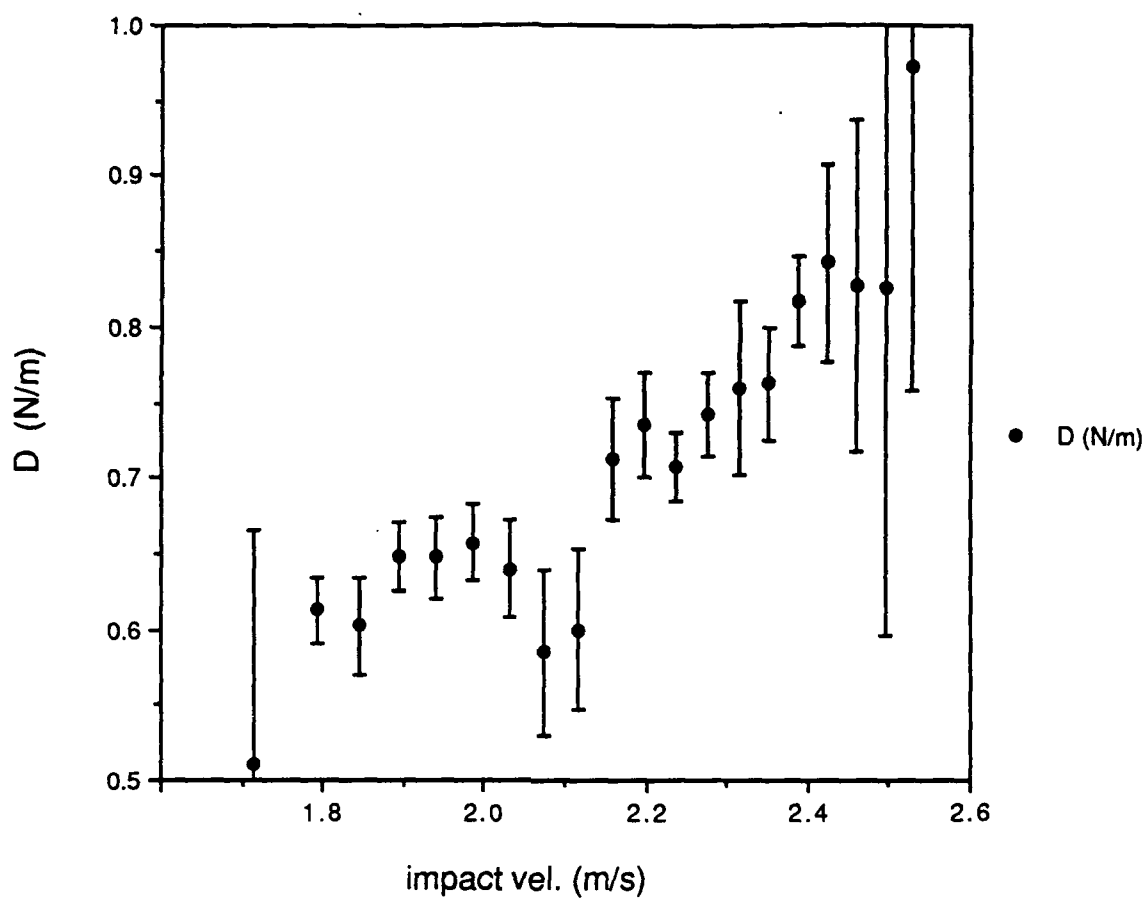
drop diameter = 2.17mm



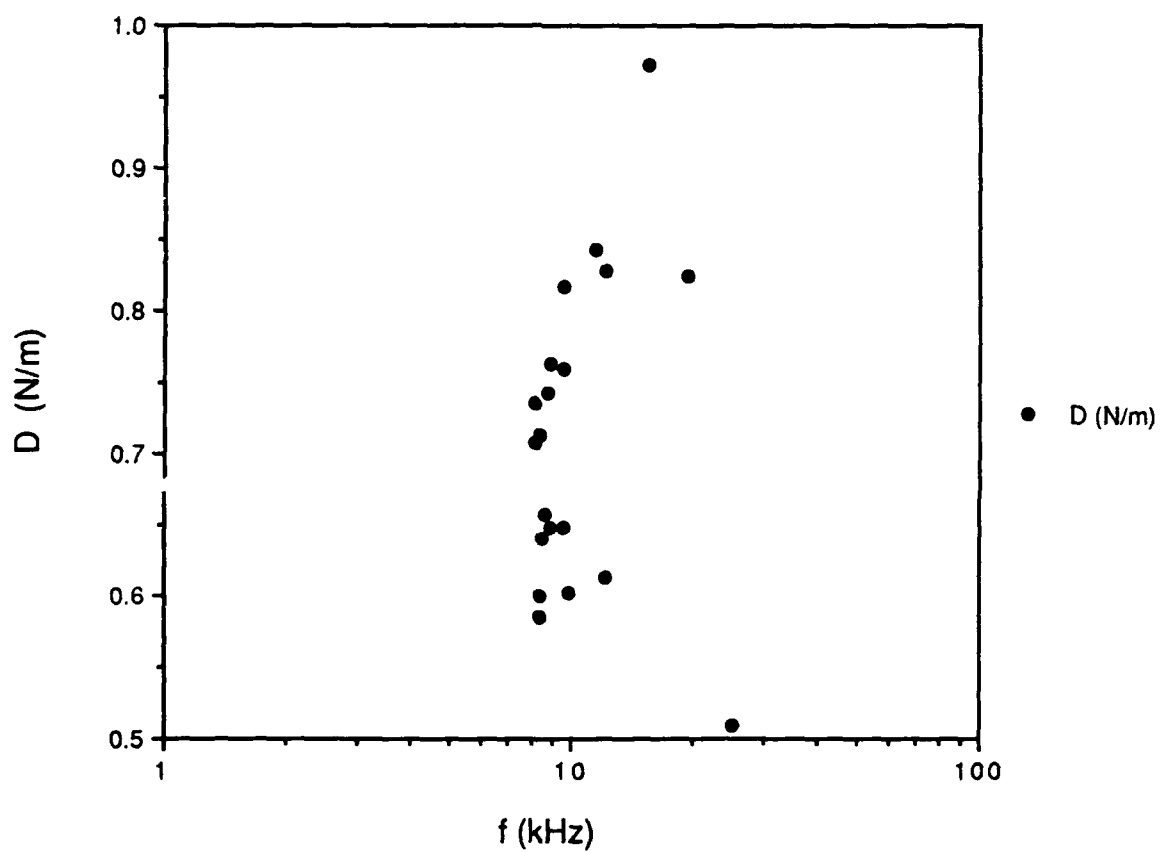
drop diameter = 2.17mm



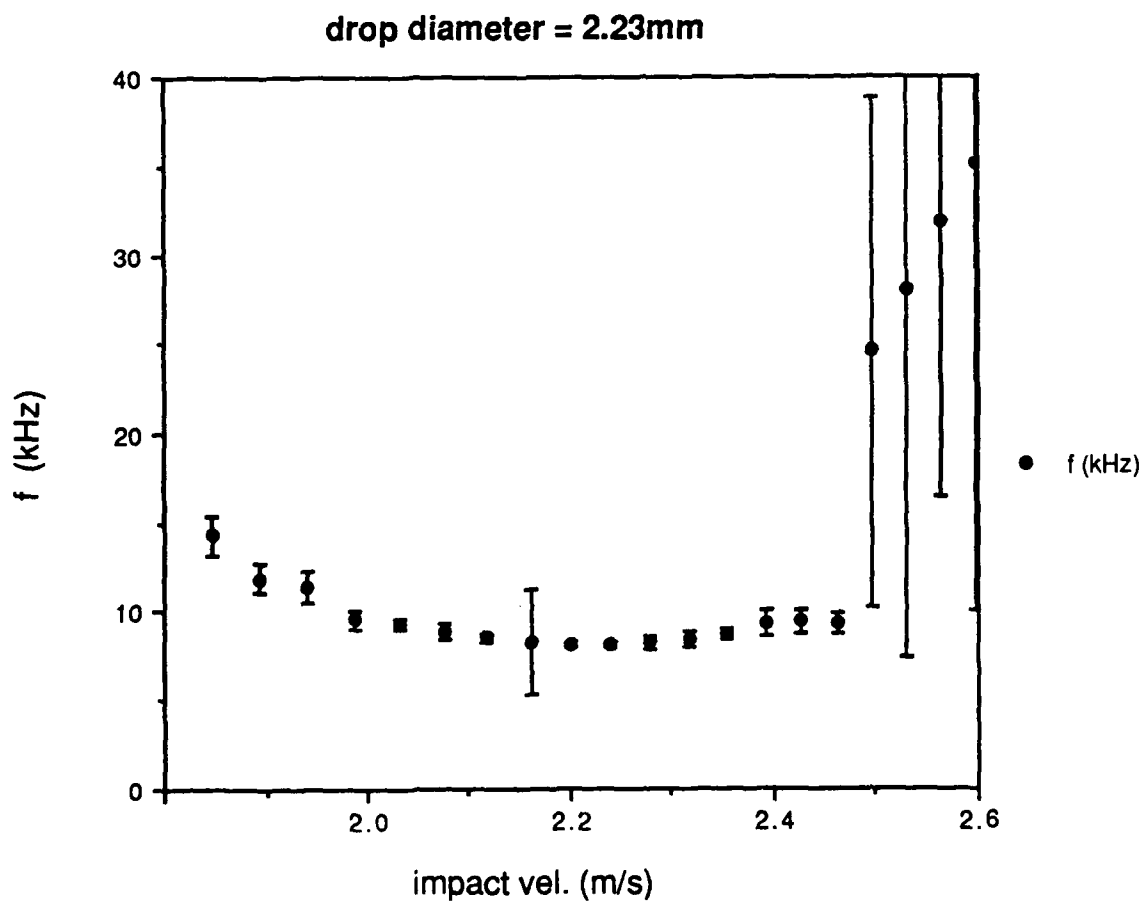
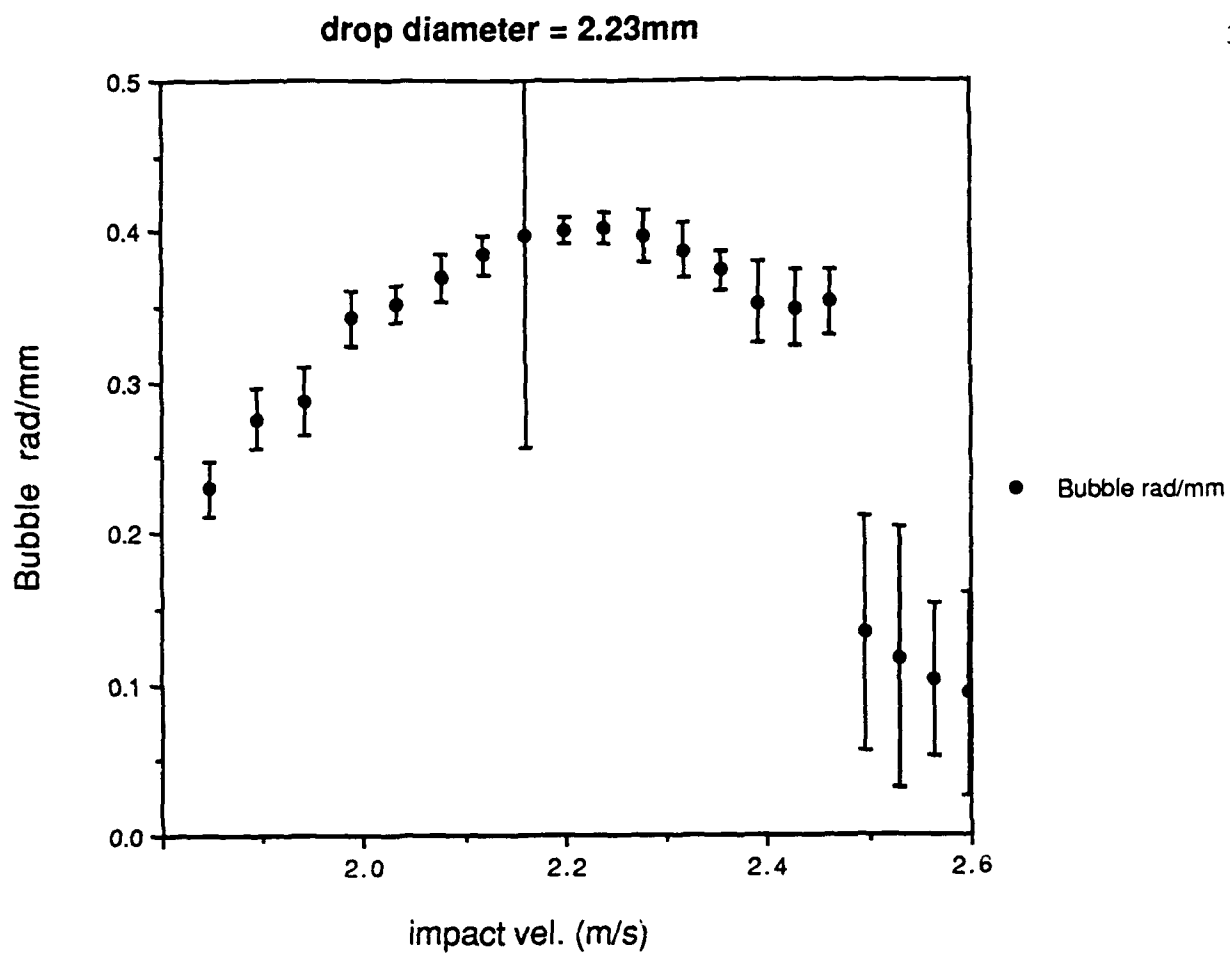
drop diameter = 2.17mm

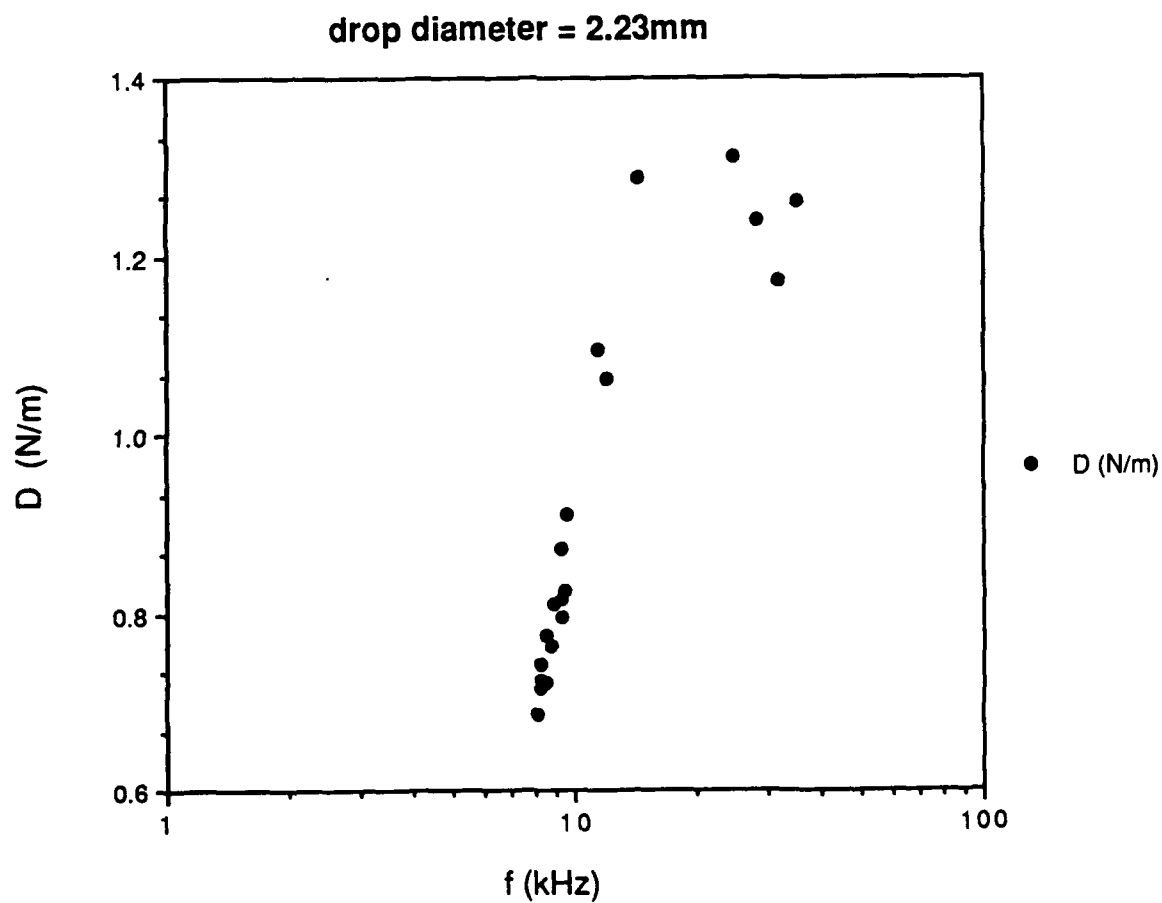
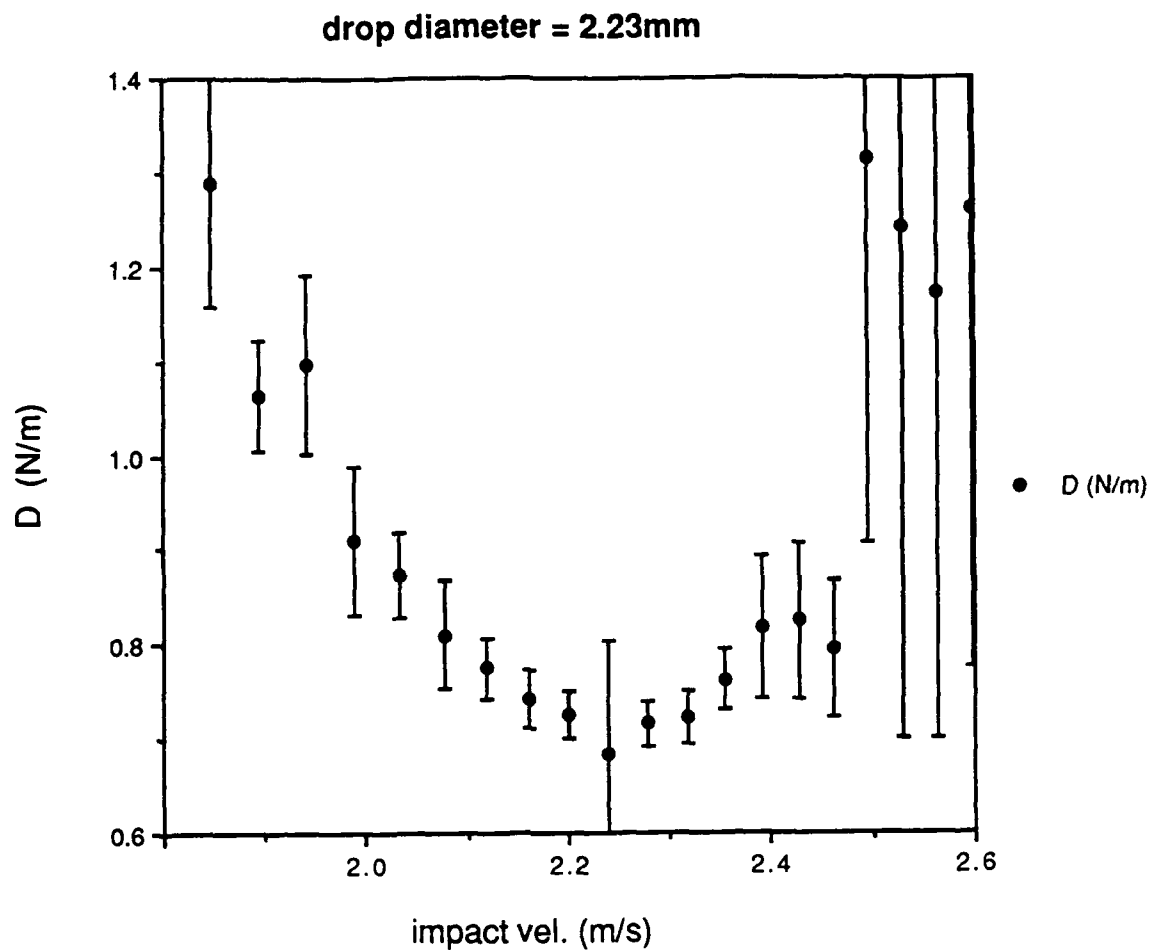


drop diameter = 2.17mm



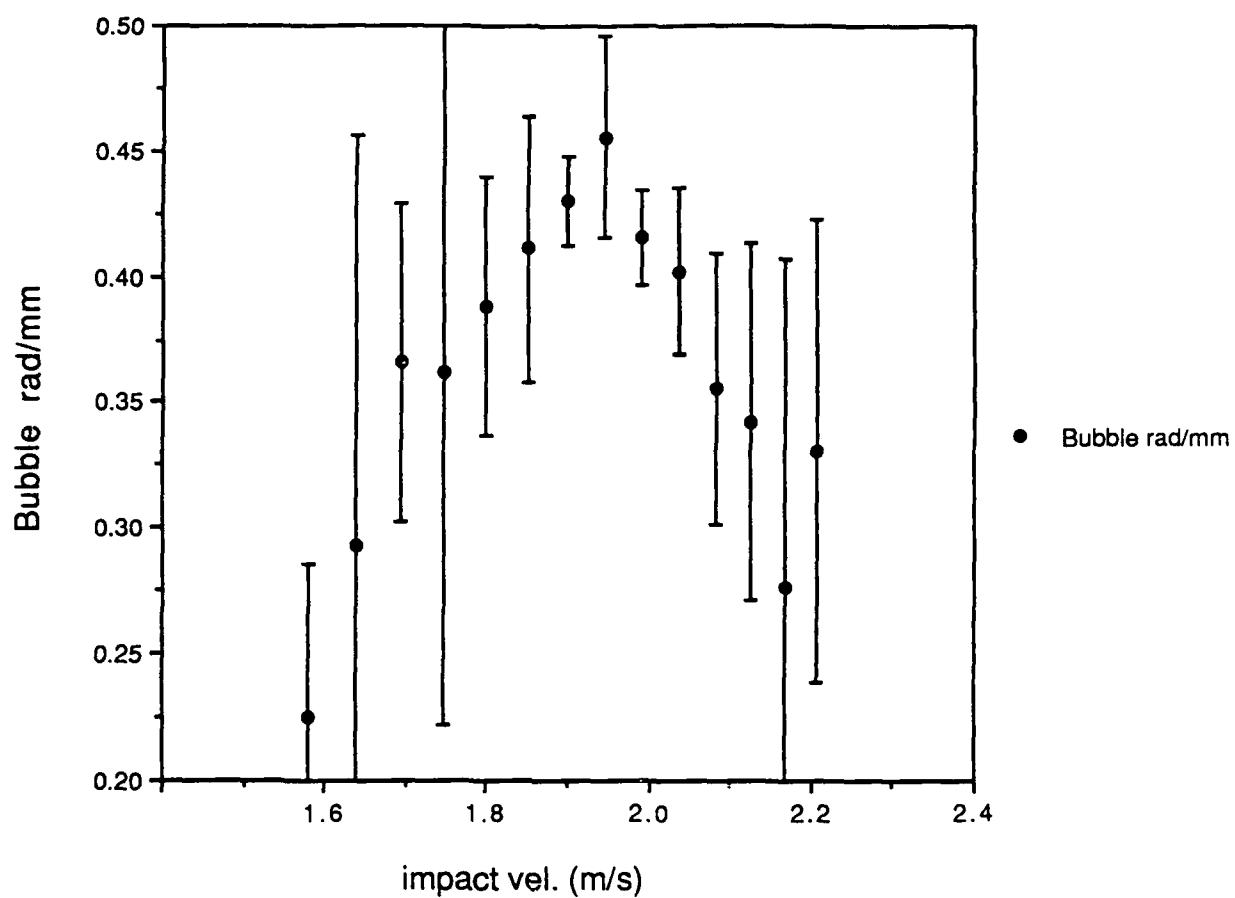
| | impact vel. | f (kHz) | sd of f | D (N/m) | sd of D | Bubble rad/mm | sd of rad |
|----|-------------|---------|---------|---------|---------|---------------|-----------|
| 1 | 1.846 | 14.300 | 1.117 | 1.288 | 0.130 | 0.229 | 0.018 |
| 2 | 1.894 | 11.881 | 0.836 | 1.062 | 0.058 | 0.276 | 0.019 |
| 3 | 1.941 | 11.406 | 0.920 | 1.095 | 0.095 | 0.288 | 0.023 |
| 4 | 1.987 | 9.563 | 0.506 | 0.910 | 0.077 | 0.343 | 0.018 |
| 5 | 2.032 | 9.306 | 0.314 | 0.873 | 0.045 | 0.352 | 0.012 |
| 6 | 2.076 | 8.891 | 0.383 | 0.810 | 0.058 | 0.369 | 0.016 |
| 7 | 2.118 | 8.533 | 0.278 | 0.775 | 0.033 | 0.384 | 0.013 |
| 8 | 2.160 | 8.269 | 2.940 | 0.743 | 0.030 | 0.397 | 0.141 |
| 9 | 2.200 | 8.185 | 0.179 | 0.725 | 0.025 | 0.401 | 0.009 |
| 10 | 2.240 | 8.149 | 0.207 | 0.685 | 0.117 | 0.403 | 0.010 |
| 11 | 2.279 | 8.269 | 0.363 | 0.716 | 0.025 | 0.397 | 0.017 |
| 12 | 2.317 | 8.465 | 0.402 | 0.723 | 0.028 | 0.387 | 0.018 |
| 13 | 2.354 | 8.773 | 0.304 | 0.762 | 0.033 | 0.374 | 0.013 |
| 14 | 2.391 | 9.305 | 0.708 | 0.818 | 0.075 | 0.352 | 0.027 |
| 15 | 2.427 | 9.413 | 0.682 | 0.825 | 0.083 | 0.348 | 0.025 |
| 16 | 2.462 | 9.293 | 0.573 | 0.795 | 0.072 | 0.353 | 0.022 |
| 17 | 2.496 | 24.548 | 14.274 | 1.312 | 0.405 | 0.134 | 0.078 |
| 18 | 2.530 | 27.932 | 20.458 | 1.240 | 0.540 | 0.117 | 0.086 |
| 19 | 2.564 | 31.849 | 15.423 | 1.173 | 0.472 | 0.103 | 0.050 |
| 20 | 2.597 | 35.173 | 25.170 | 1.260 | 0.485 | 0.093 | 0.067 |



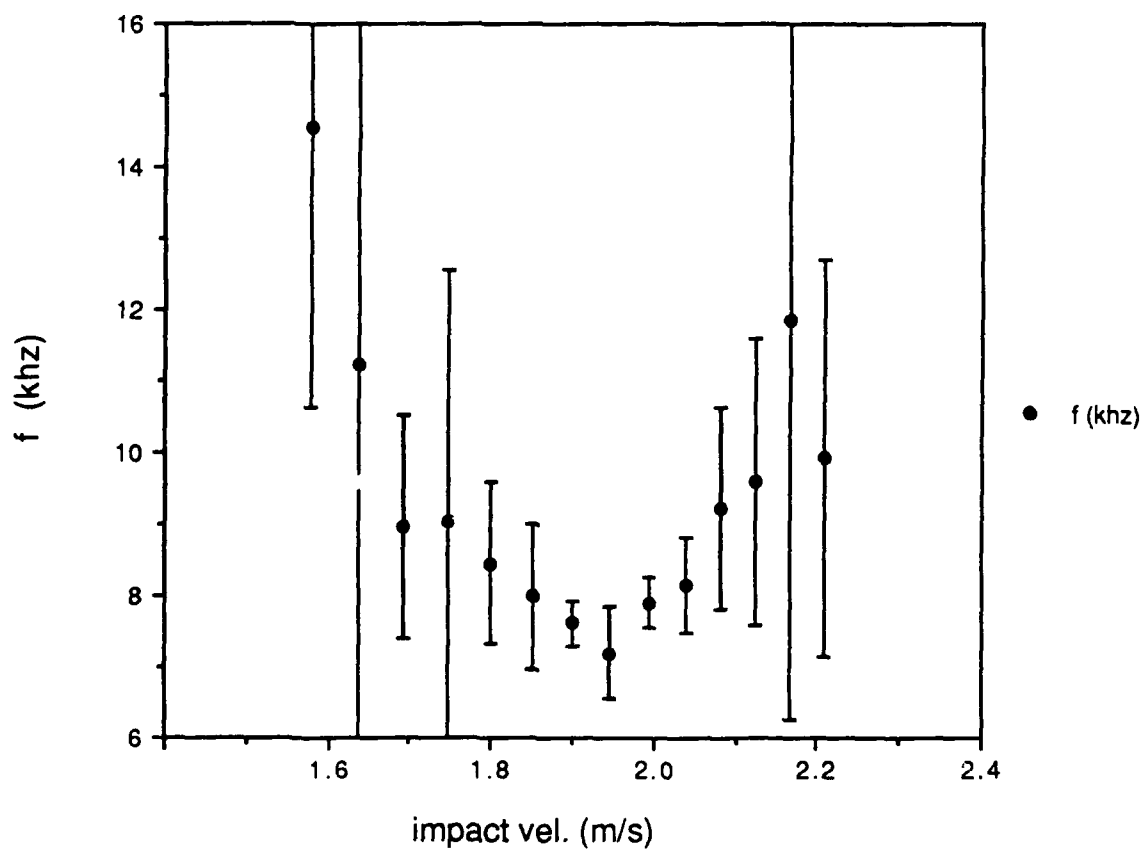


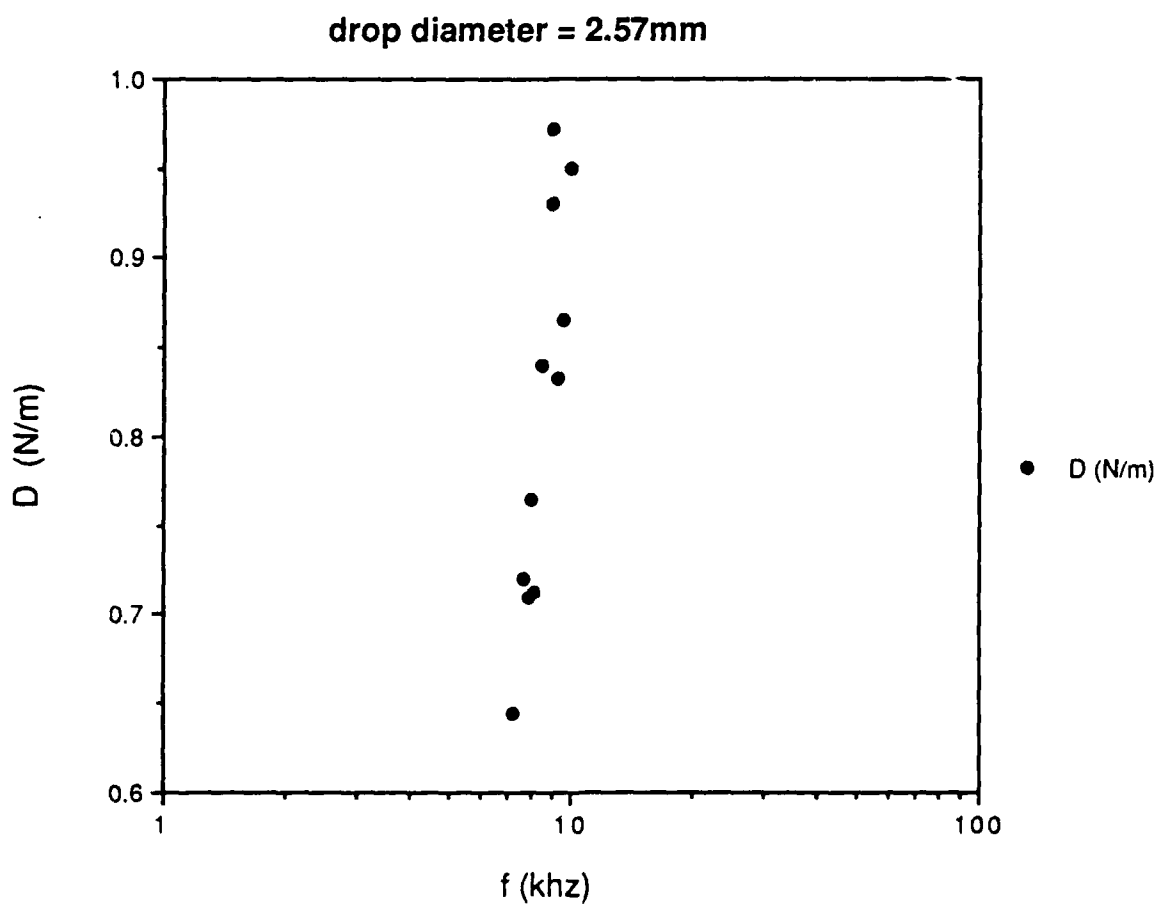
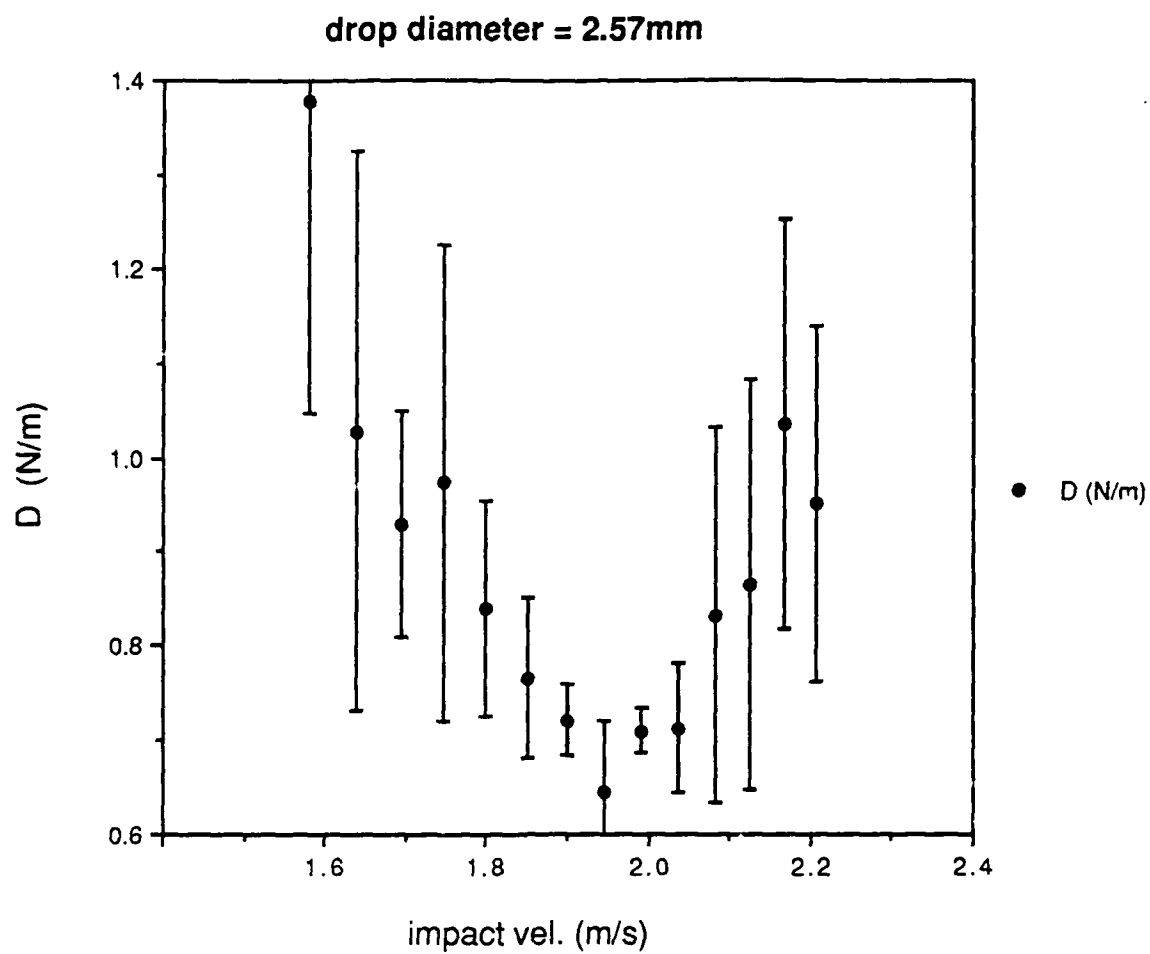
| | impact vel. | f (khz) | sd of f | D (N/m) | sd of D | Bubble rad/mm | sd of rad |
|----|-------------|---------|---------|---------|---------|---------------|-----------|
| 1 | 2.208 | 9.927 | 2.770 | 0.950 | 0.188 | 0.330 | 0.092 |
| 2 | 2.167 | 11.850 | 5.573 | 1.035 | 0.217 | 0.277 | 0.130 |
| 3 | 2.125 | 9.586 | 1.993 | 0.865 | 0.217 | 0.342 | 0.071 |
| 4 | 2.082 | 9.233 | 1.400 | 0.833 | 0.200 | 0.355 | 0.054 |
| 5 | 2.038 | 8.155 | 0.671 | 0.713 | 0.068 | 0.402 | 0.033 |
| 6 | 1.993 | 7.901 | 0.354 | 0.710 | 0.022 | 0.415 | 0.019 |
| 7 | 1.947 | 7.202 | 0.640 | 0.645 | 0.075 | 0.455 | 0.040 |
| 8 | 1.899 | 7.625 | 0.314 | 0.720 | 0.037 | 0.430 | 0.018 |
| 9 | 1.850 | 7.987 | 1.030 | 0.765 | 0.085 | 0.411 | 0.053 |
| 10 | 1.800 | 8.460 | 1.116 | 0.840 | 0.115 | 0.388 | 0.051 |
| 11 | 1.747 | 9.050 | 3.498 | 0.973 | 0.253 | 0.362 | 0.140 |
| 12 | 1.693 | 8.965 | 1.546 | 0.930 | 0.120 | 0.366 | 0.063 |
| 13 | 1.637 | 11.207 | 6.241 | 1.028 | 0.297 | 0.293 | 0.163 |
| 14 | 1.579 | 14.563 | 3.944 | 1.377 | 0.333 | 0.225 | 0.061 |

drop diameter = 2.57mm



drop diameter = 2.57mm

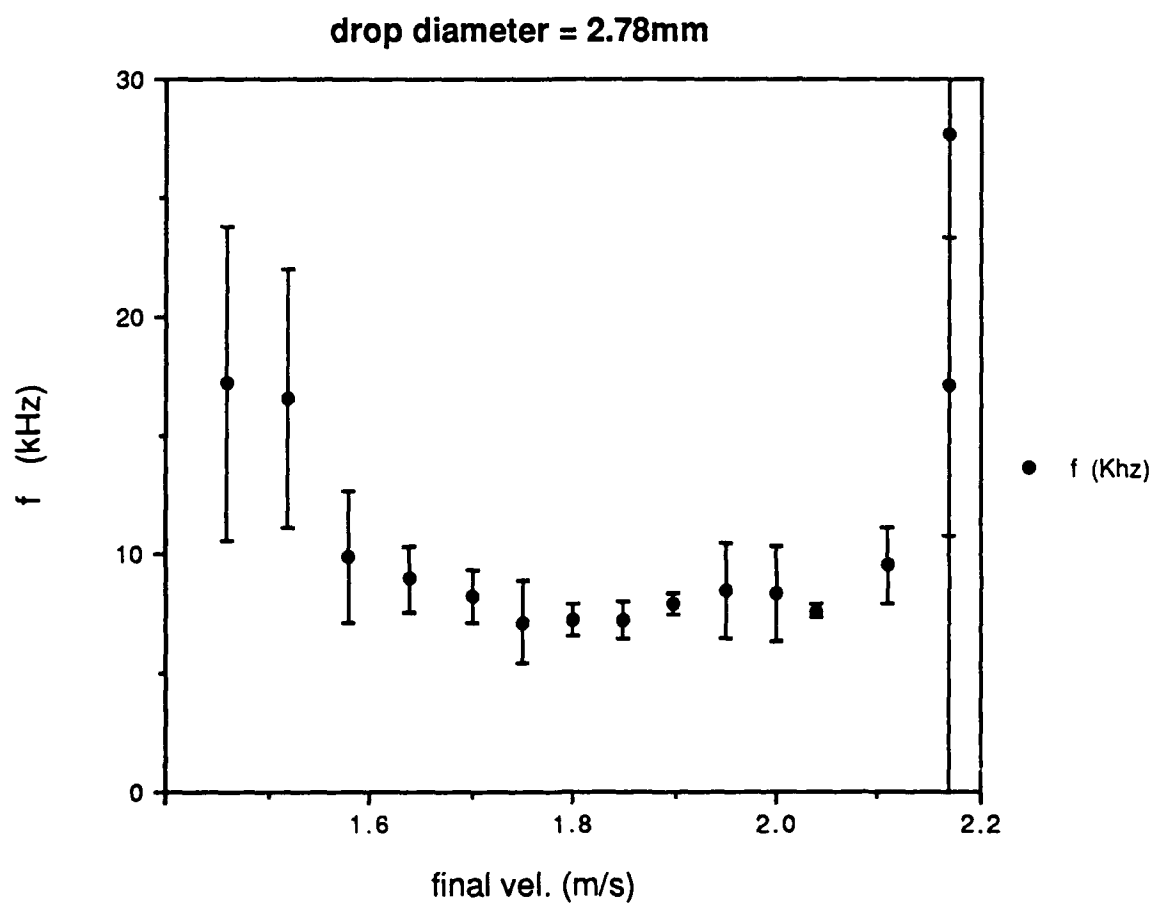
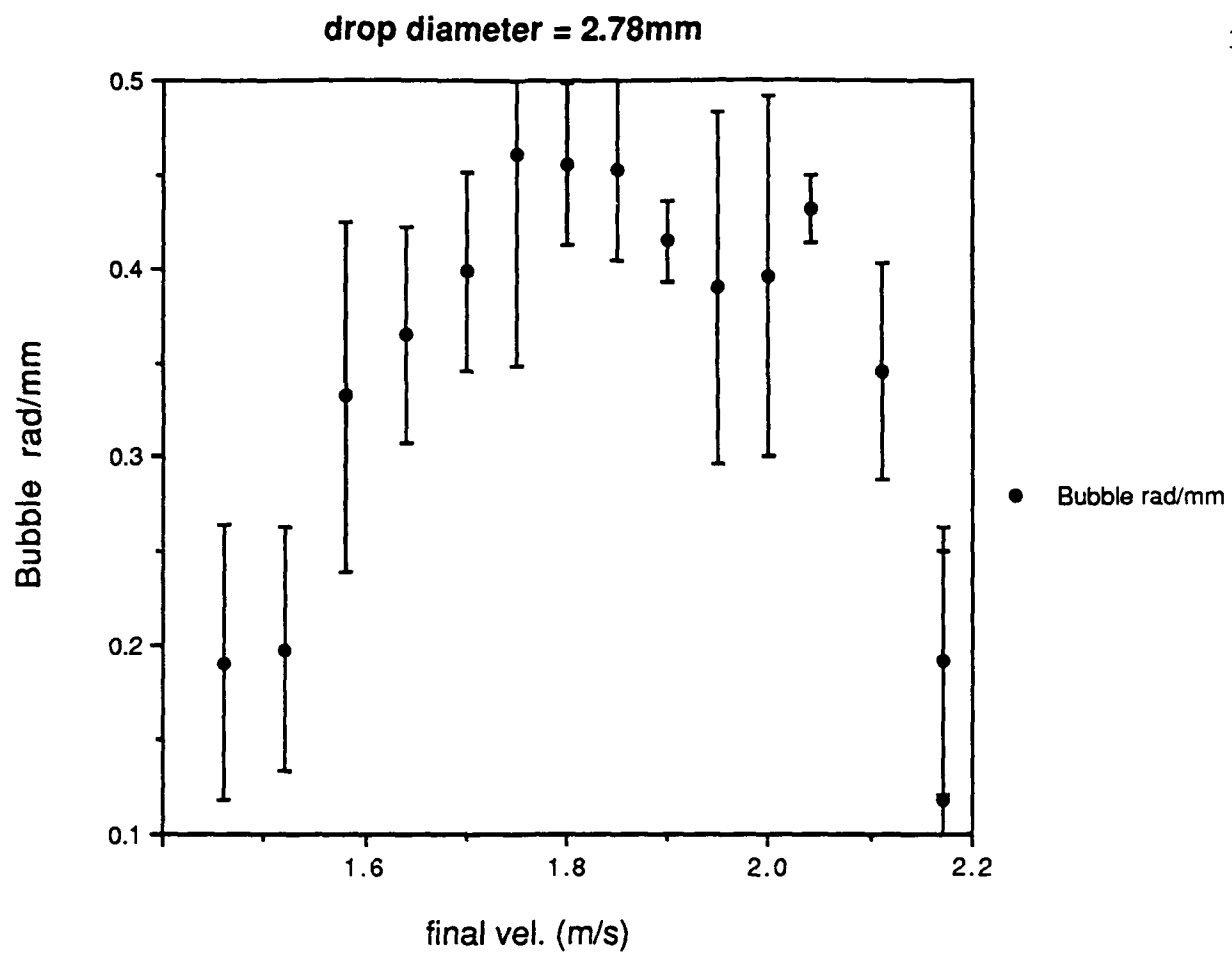


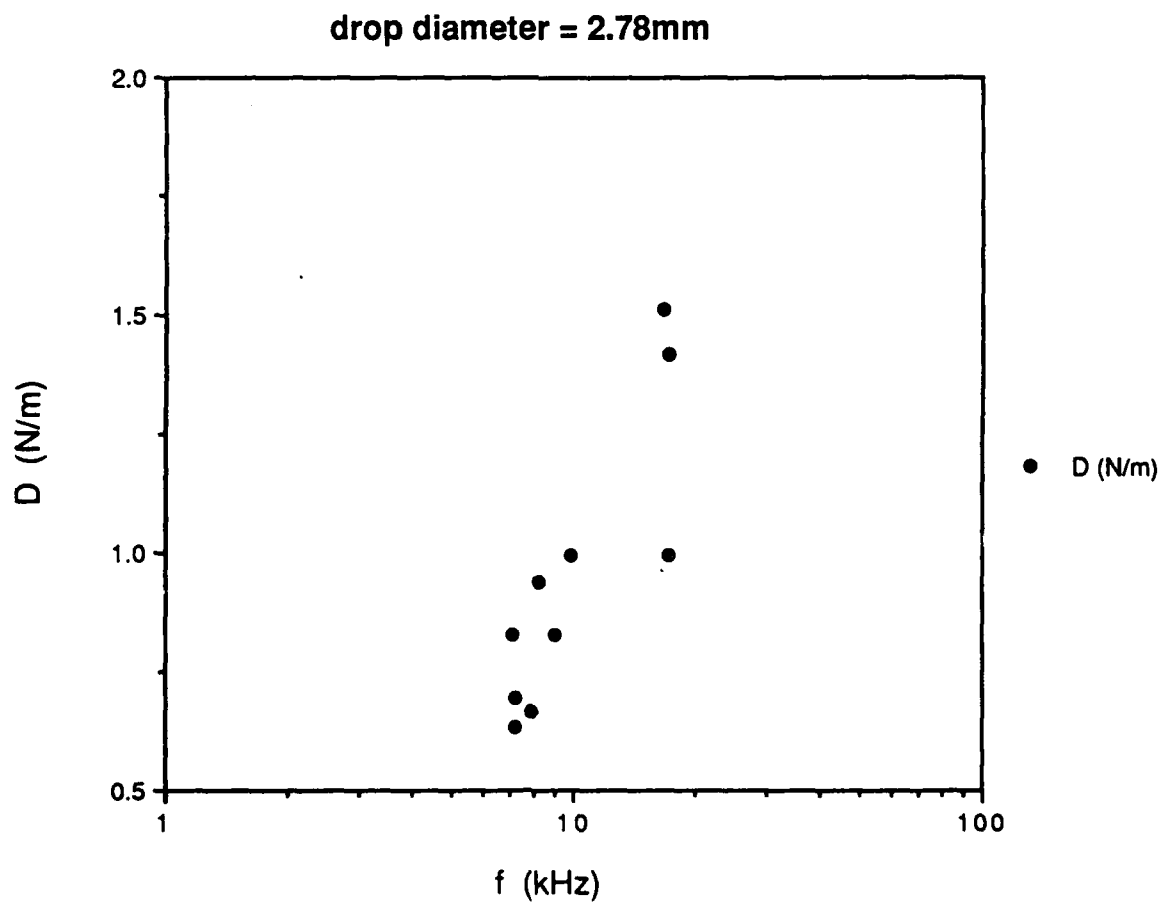
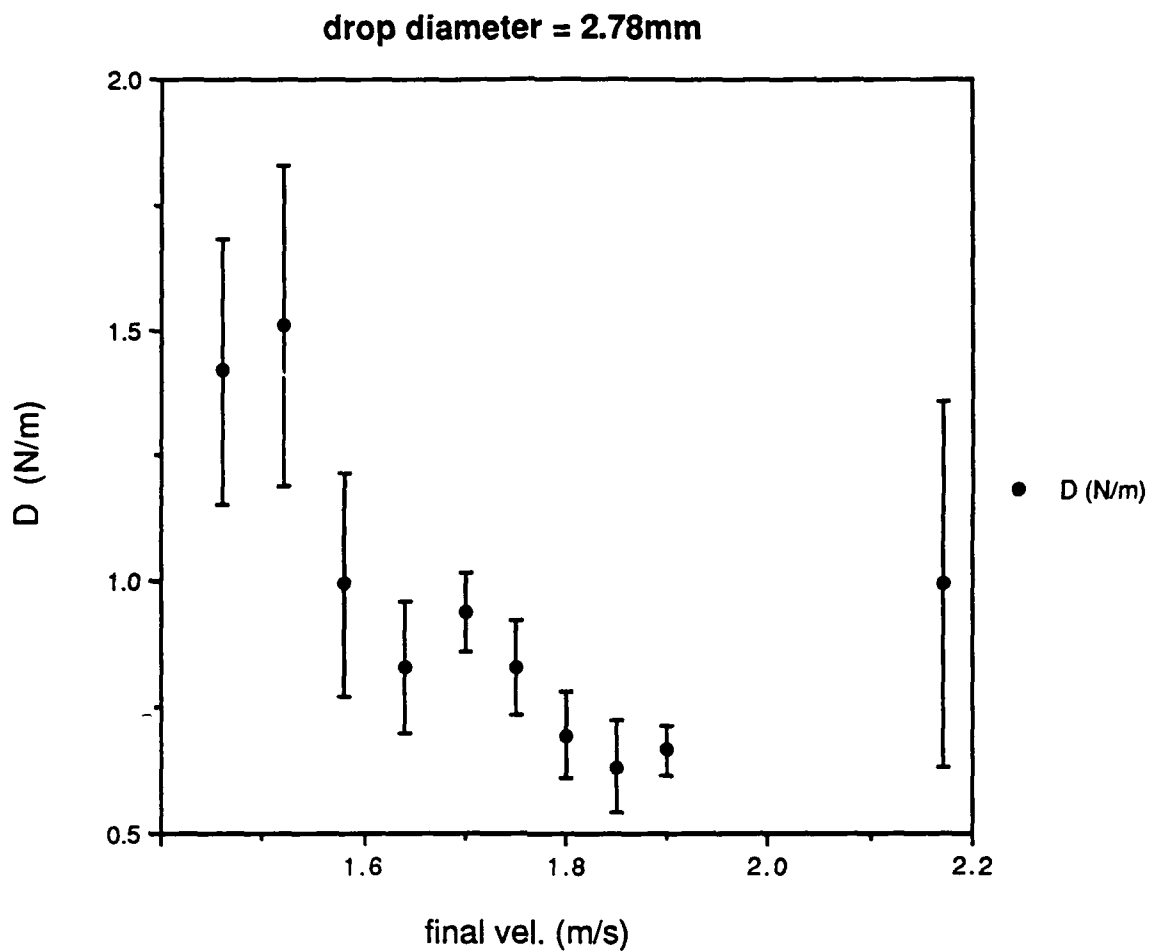


| | final vel. | f (kHz) | sd of f | D (N/m) | sd of D | Bubble rad/mm | sd of rad |
|----|------------|---------|---------|---------|---------|---------------|-----------|
| 1 | 2.110 | 9.506 | 1.573 | 0.000 | 0.000 | 0.345 | 0.057 |
| 2 | 2.170 | 27.714 | 31.057 | 0.000 | 0.000 | 0.118 | 0.133 |
| 3 | 2.040 | 7.595 | 0.313 | 0.000 | 0.000 | 0.432 | 0.018 |
| 4 | 2.000 | 8.280 | 2.001 | 0.000 | 0.000 | 0.396 | 0.096 |
| 5 | 1.950 | 8.423 | 2.022 | 0.000 | 0.000 | 0.389 | 0.093 |
| 6 | 1.900 | 7.909 | 0.409 | 0.665 | 0.048 | 0.415 | 0.021 |
| 7 | 2.170 | 17.070 | 6.272 | 0.995 | 0.362 | 0.192 | 0.071 |
| 8 | 1.850 | 7.246 | 0.772 | 0.632 | 0.092 | 0.453 | 0.048 |
| 9 | 1.800 | 7.201 | 0.674 | 0.695 | 0.085 | 0.455 | 0.043 |
| 10 | 1.750 | 7.126 | 1.736 | 0.830 | 0.092 | 0.460 | 0.112 |
| 11 | 1.700 | 8.236 | 1.085 | 0.940 | 0.080 | 0.398 | 0.052 |
| 12 | 1.640 | 8.980 | 1.400 | 0.828 | 0.130 | 0.365 | 0.057 |
| 13 | 1.580 | 9.871 | 2.767 | 0.995 | 0.223 | 0.332 | 0.093 |
| 14 | 1.520 | 16.567 | 5.438 | 1.510 | 0.320 | 0.198 | 0.065 |
| 15 | 1.460 | 17.174 | 6.586 | 1.417 | 0.263 | 0.191 | 0.073 |

NOTE TO THE USE OF $d=2.78\text{mm}$

The dipole strength values, D, that equal zero are artificial; they were inserted solely to make the graphing work. For impact velocity = 2.170 m/s, $N = 75$.

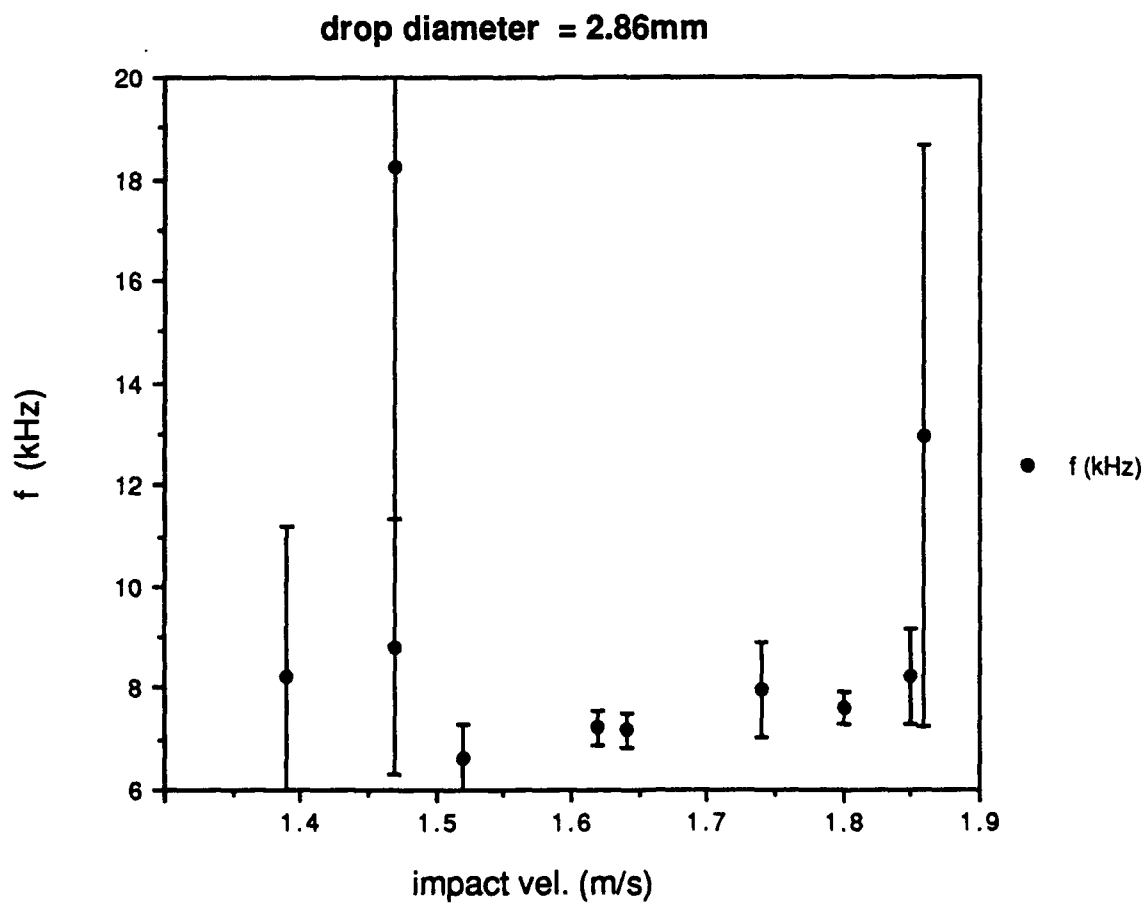
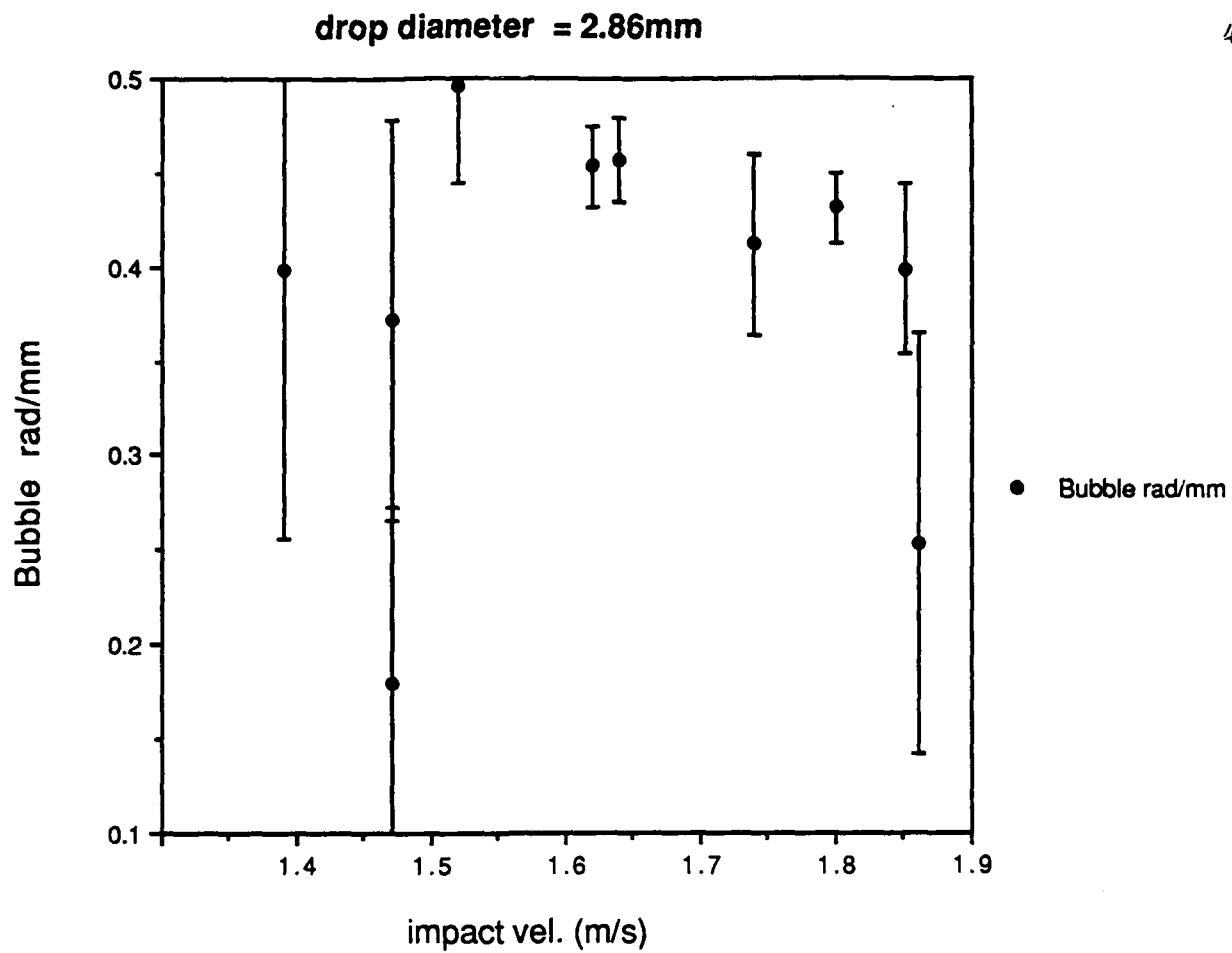




| | final vel. | f (kHz) | sd of f | Bubble rad/mm | sd of rad |
|----|------------|---------|---------|---------------|-----------|
| 1 | 1.620 | 7.233 | 0.338 | 0.453 | 0.021 |
| 2 | 1.740 | 7.968 | 0.939 | 0.412 | 0.049 |
| 3 | 1.470 | 8.817 | 2.520 | 0.372 | 0.106 |
| 4 | 1.860 | 12.950 | 5.727 | 0.253 | 0.112 |
| 5 | 1.470 | 18.217 | 9.365 | 0.180 | 0.093 |
| 6 | 1.390 | 8.248 | 2.943 | 0.398 | 0.142 |
| 7 | 1.520 | 6.611 | 0.685 | 0.496 | 0.051 |
| 8 | 1.640 | 7.174 | 0.352 | 0.457 | 0.022 |
| 9 | 1.800 | 7.610 | 0.322 | 0.431 | 0.018 |
| 10 | 1.850 | 8.228 | 0.940 | 0.399 | 0.046 |

NOTE TO THE USE OF $D=2.86\text{mm}$

Not all of the data points represent the average of $N = 30$ measured frequencies. For the two impact velocities = 1.47 m/s, $N = 20$ and 84. For impact velocity = 1.85 m/s, $N = 20$.

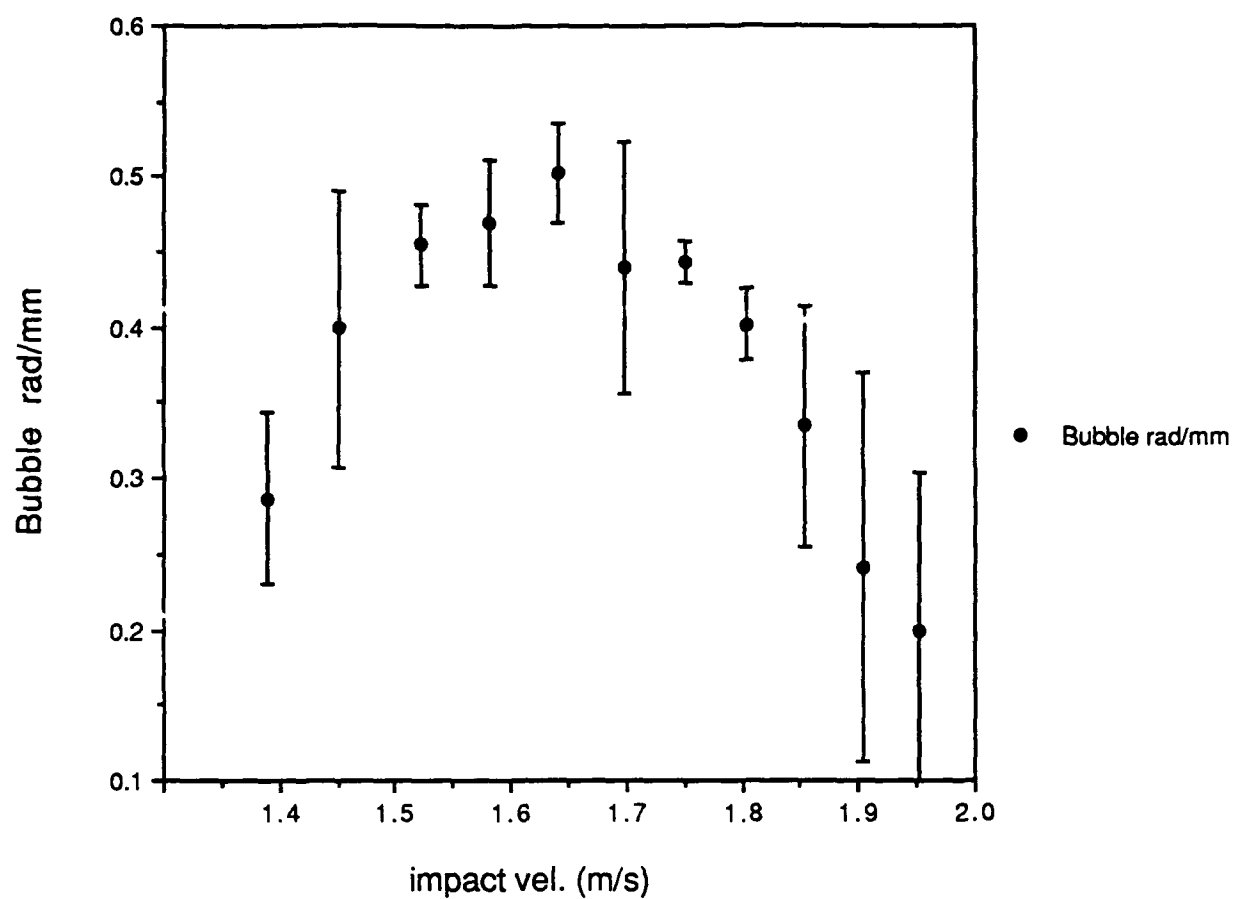


drop diameter = 3.07mm

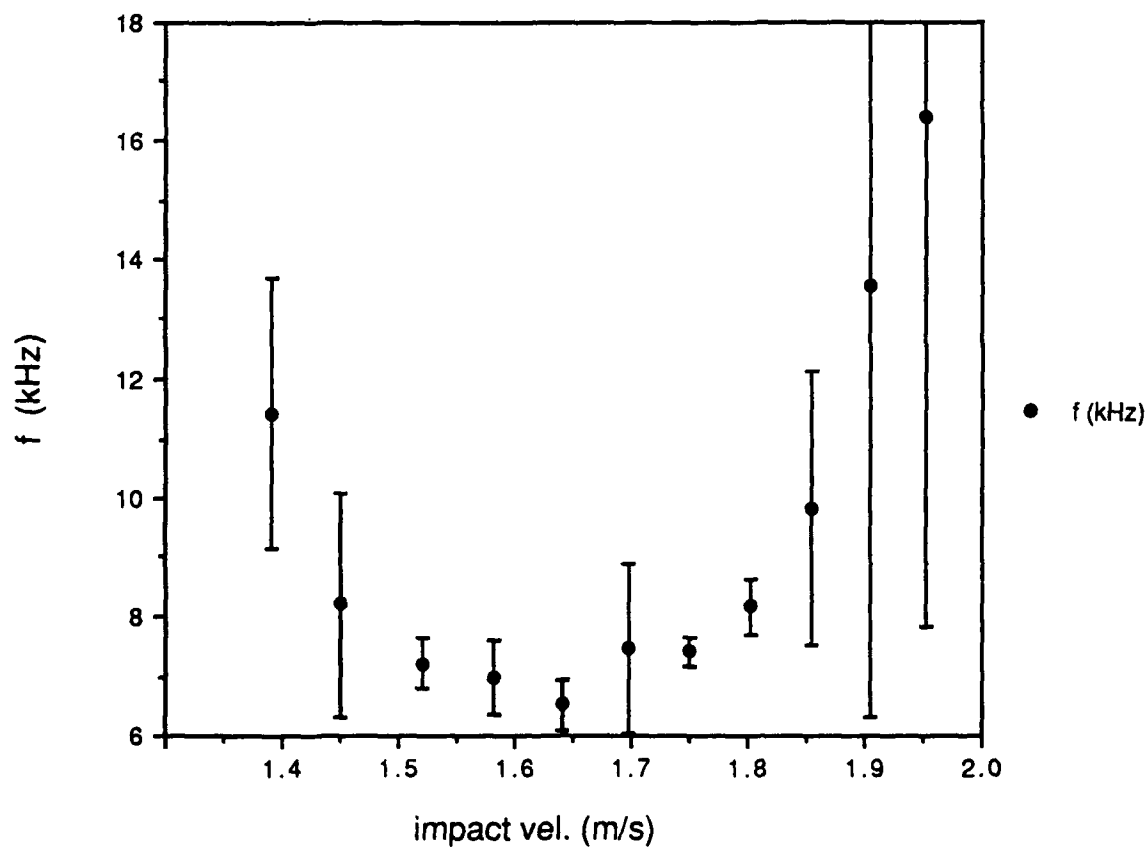
Thu, Jul 20, 1989 1:02 PM

| | impact vel. | f (kHz) | sd of f | D (N/m) | sd of D | Bubble rad/mm | sd of rad |
|----|-------------|---------|---------|---------|---------|---------------|-----------|
| 1 | 1.390 | 11.422 | 2.271 | 1.060 | 0.215 | 0.287 | 0.057 |
| 2 | 1.451 | 8.212 | 1.883 | 0.855 | 0.190 | 0.399 | 0.092 |
| 3 | 1.521 | 7.214 | 0.422 | 0.785 | 0.045 | 0.455 | 0.027 |
| 4 | 1.582 | 6.993 | 0.620 | 0.710 | 0.065 | 0.469 | 0.042 |
| 5 | 1.640 | 6.527 | 0.420 | 0.565 | 0.055 | 0.503 | 0.032 |
| 6 | 1.697 | 7.467 | 1.425 | 0.630 | 0.025 | 0.439 | 0.084 |
| 7 | 1.751 | 7.408 | 0.233 | 0.625 | 0.030 | 0.443 | 0.014 |
| 8 | 1.803 | 8.157 | 0.484 | 0.625 | 0.050 | 0.402 | 0.024 |
| 9 | 1.854 | 9.810 | 2.311 | 0.905 | 0.225 | 0.334 | 0.079 |
| 10 | 1.904 | 13.567 | 7.235 | 0.745 | 0.205 | 0.242 | 0.129 |
| 11 | 1.952 | 16.416 | 5.594 | 1.140 | 0.275 | 0.200 | 0.155 |

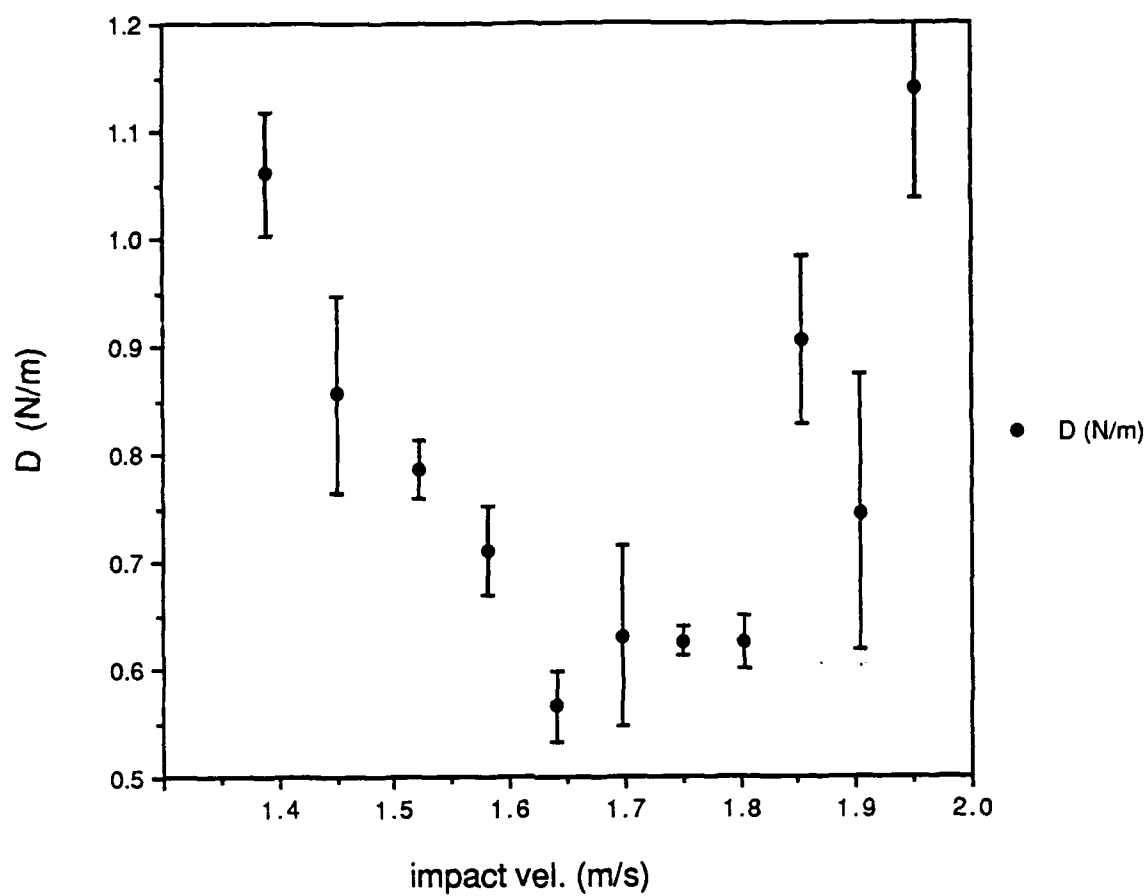
drop diameter = 3.07mm



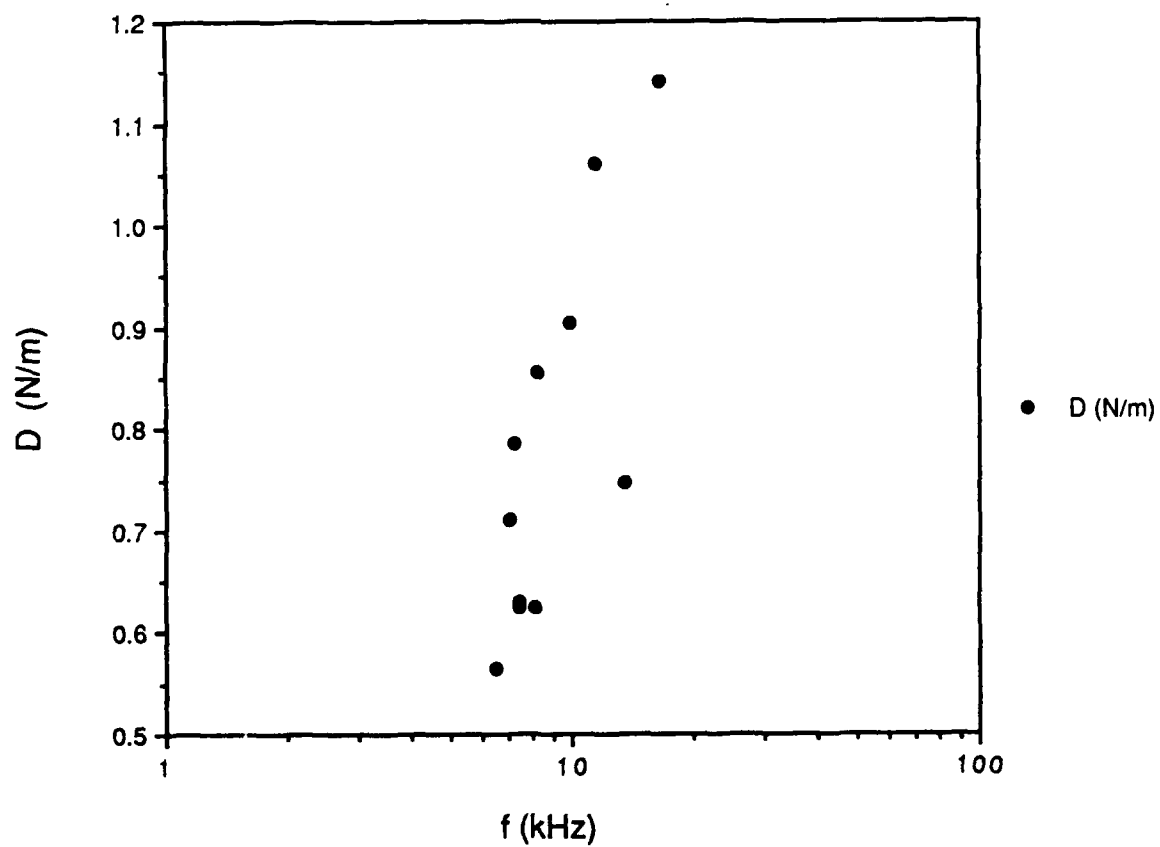
drop diameter = 3.07mm



drop diameter = 3.07mm



drop diameter = 3.07mm

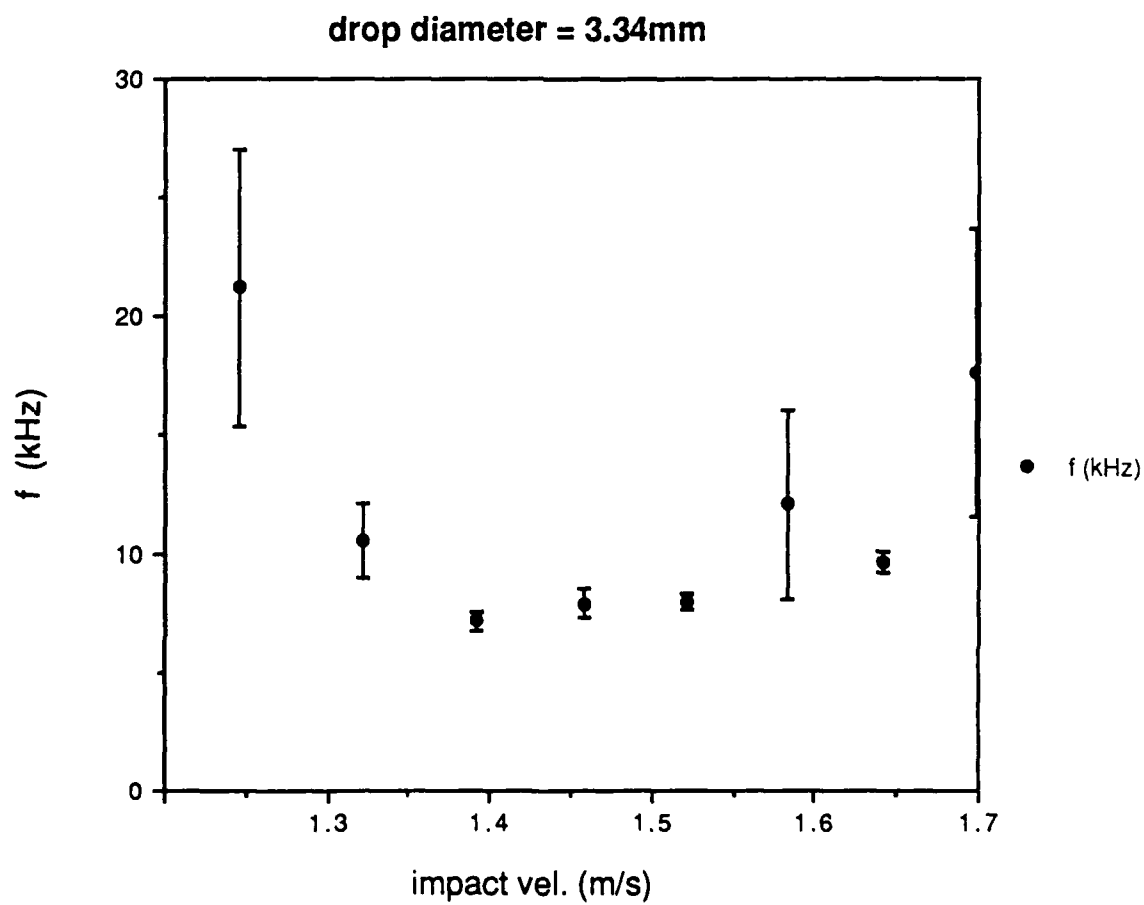
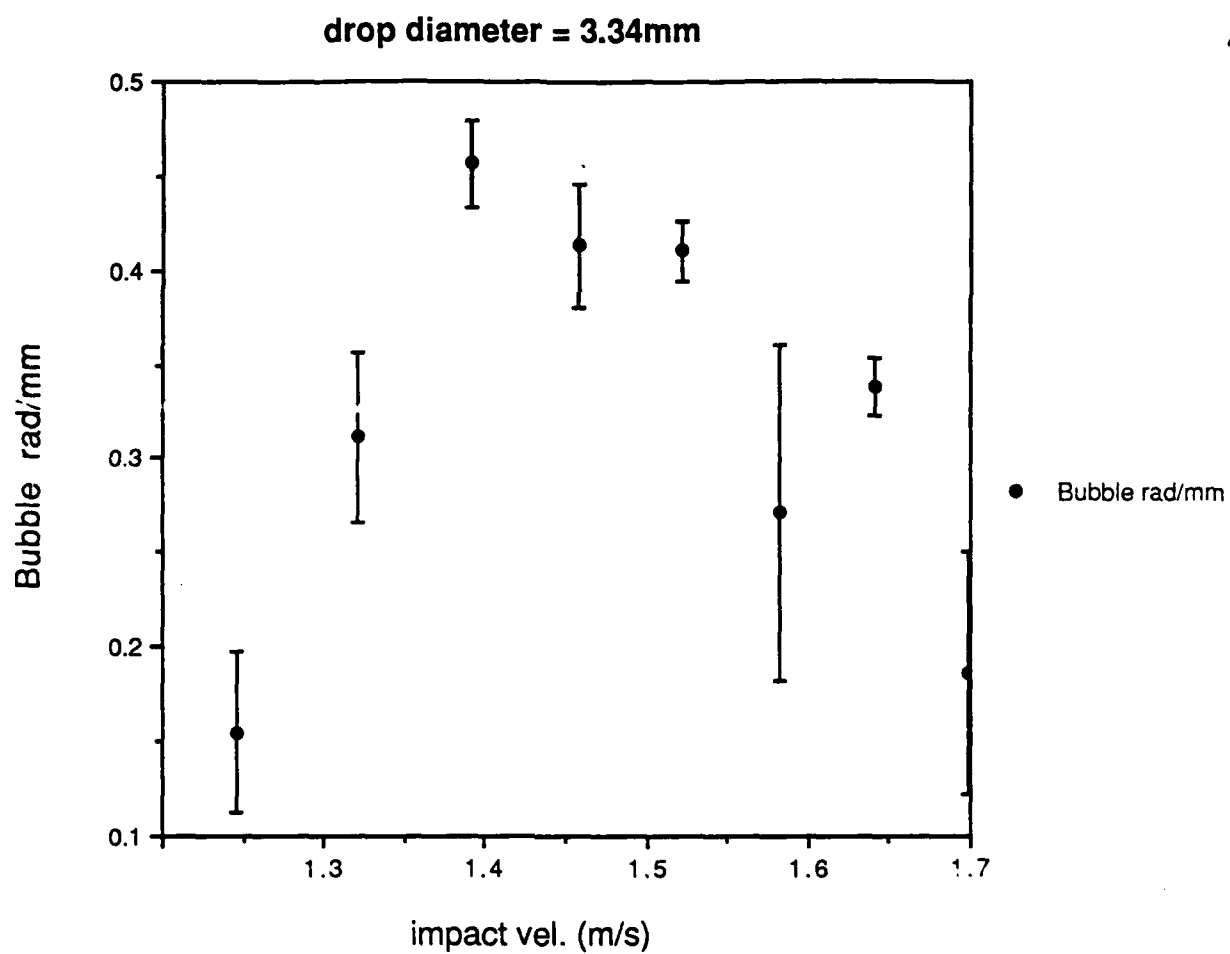


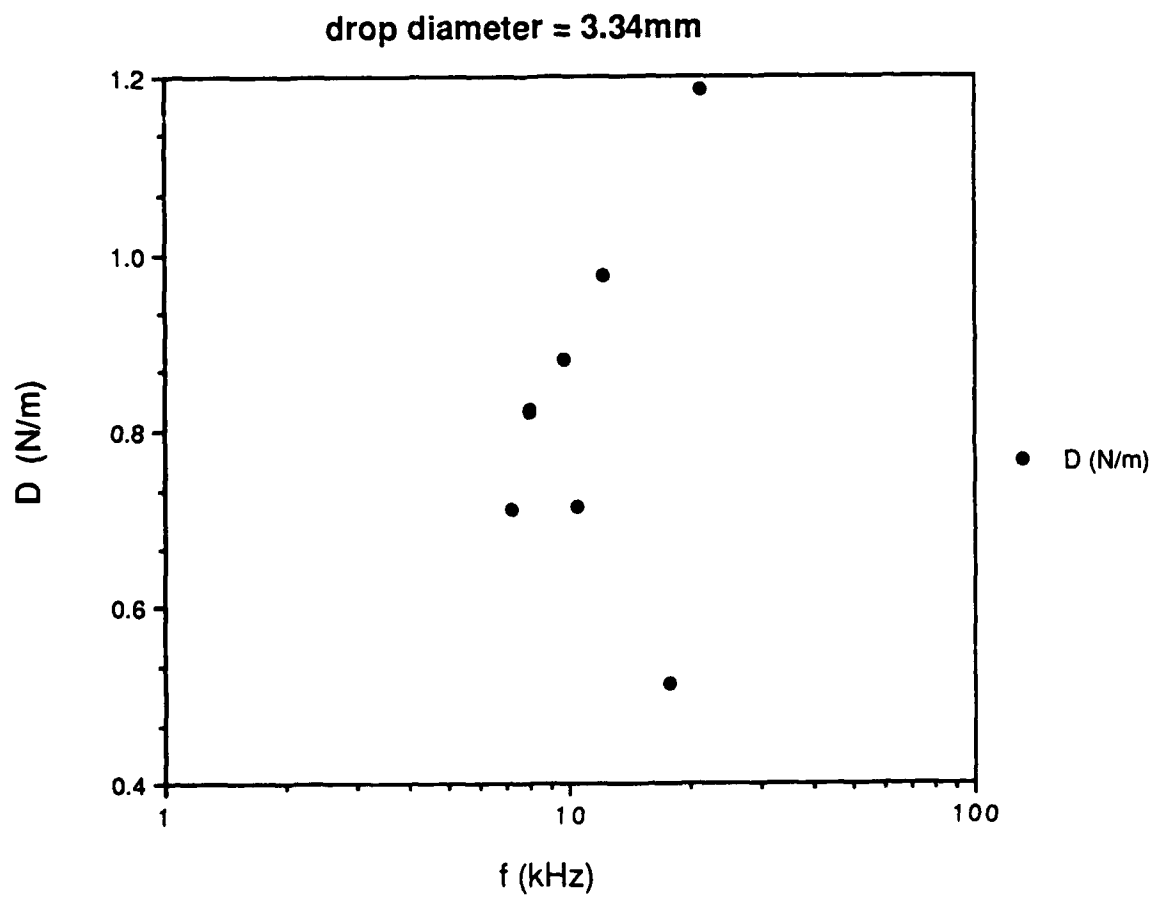
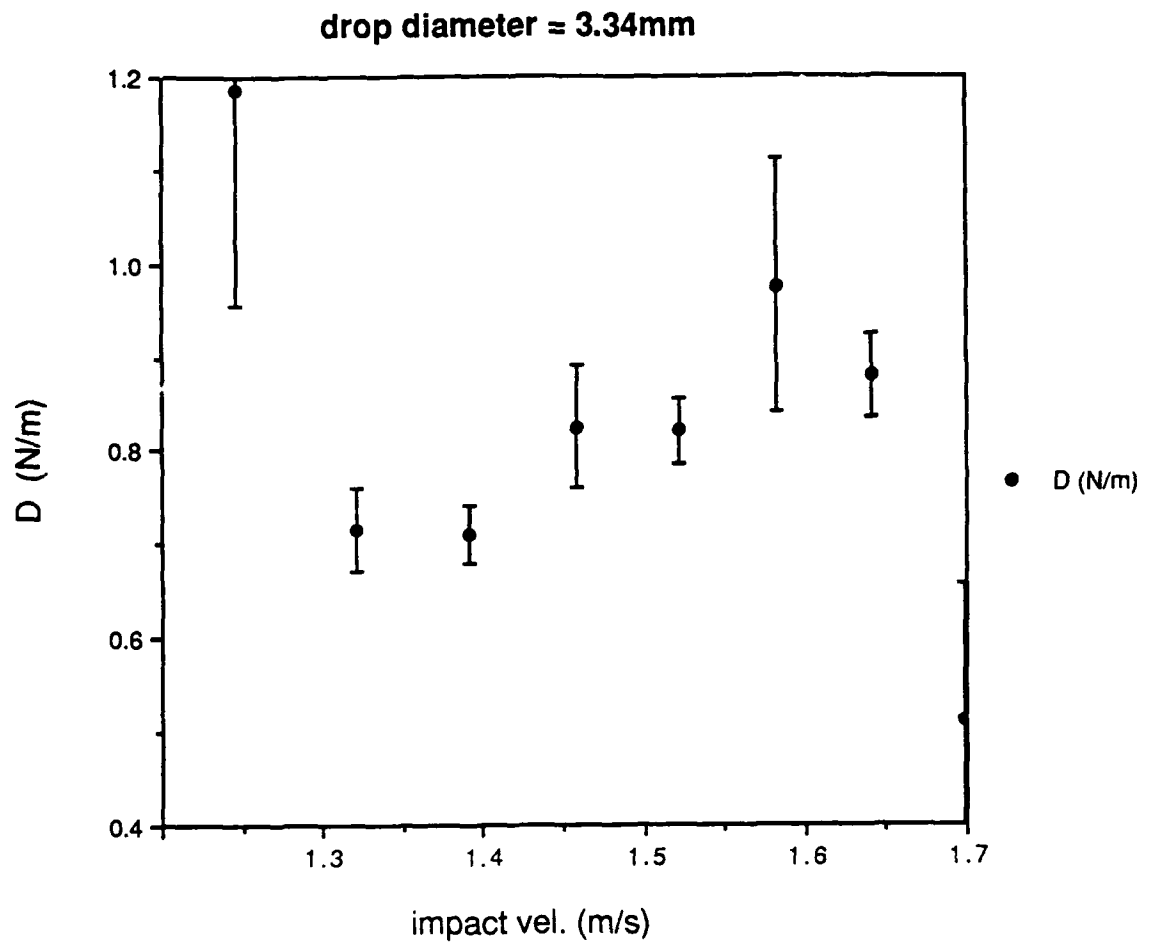
drop diameter = 3.34mm

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| | impact vel. | f (kHz) | sd of f | D (N/m) | sd of D | Bubble rad/mm | sd of rad |
|---|-------------|---------|---------|---------|---------|---------------|-----------|
| 1 | 1.246 | 21.170 | 5.790 | 1.185 | 0.230 | 0.155 | 0.042 |
| 2 | 1.321 | 10.536 | 1.551 | 0.715 | 0.045 | 0.311 | 0.046 |
| 3 | 1.391 | 7.186 | 0.357 | 0.710 | 0.030 | 0.456 | 0.023 |
| 4 | 1.458 | 7.938 | 0.630 | 0.825 | 0.065 | 0.413 | 0.033 |
| 5 | 1.522 | 7.985 | 0.311 | 0.820 | 0.035 | 0.411 | 0.016 |
| 6 | 1.583 | 12.064 | 3.968 | 0.975 | 0.135 | 0.272 | 0.089 |
| 7 | 1.641 | 9.687 | 0.427 | 0.880 | 0.045 | 0.339 | 0.015 |
| 8 | 1.698 | 17.586 | 6.049 | 0.512 | 0.145 | 0.187 | 0.064 |



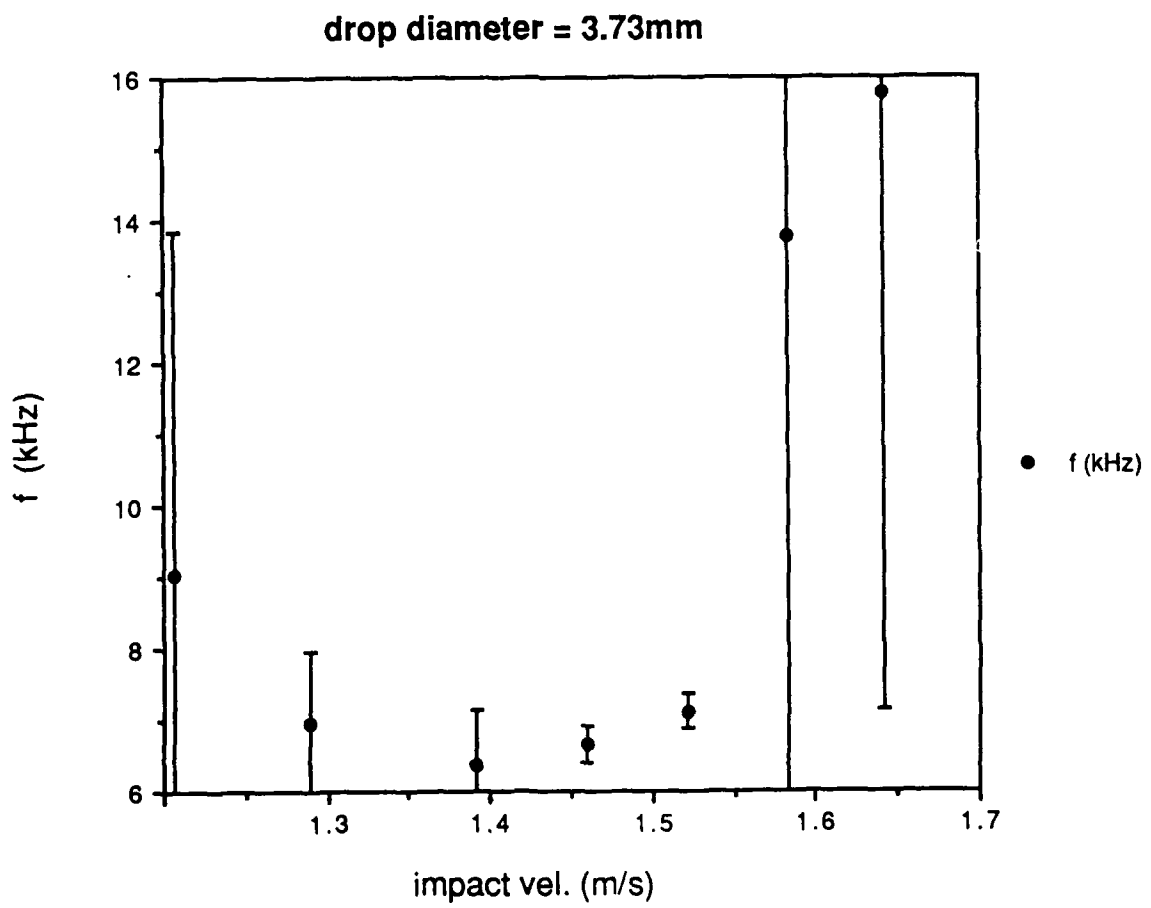
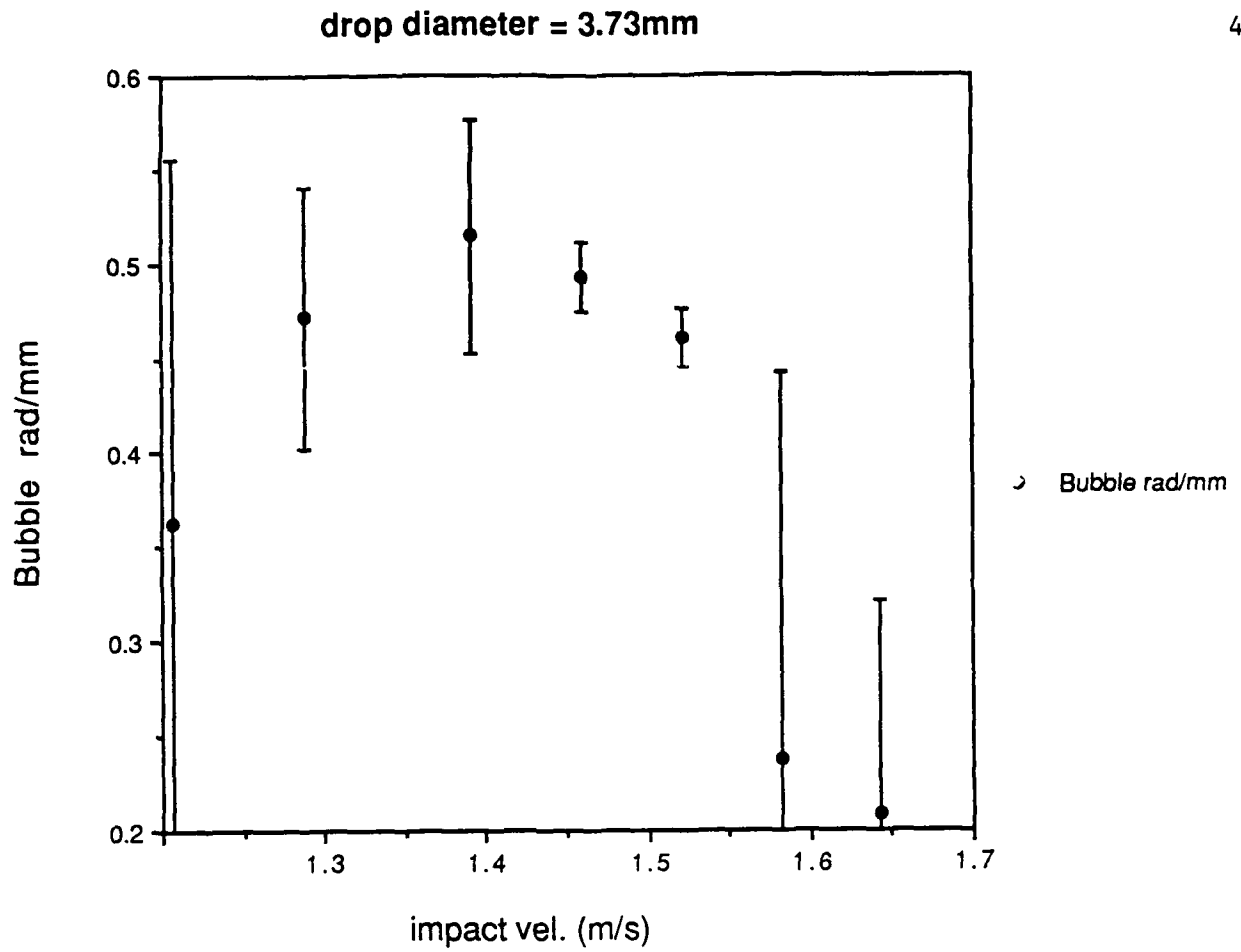


drop diameter = 3.73mm

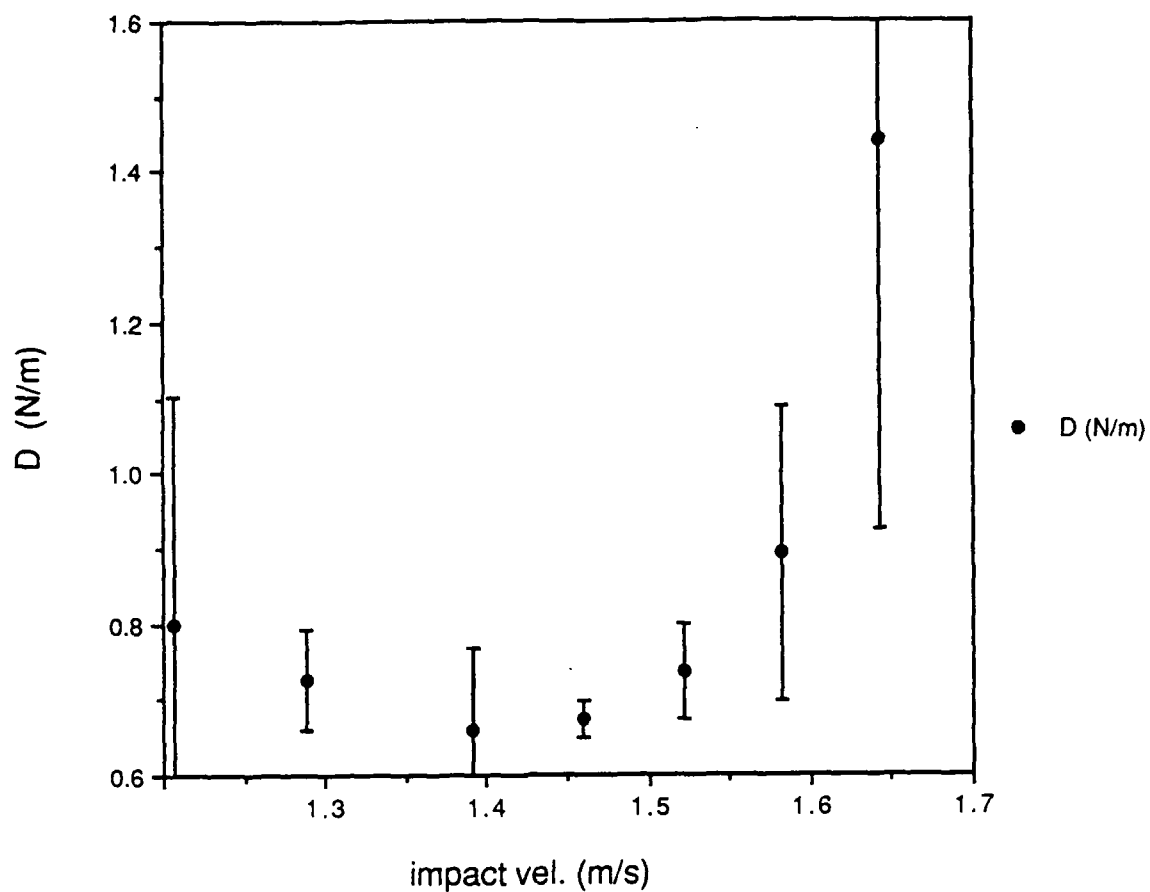
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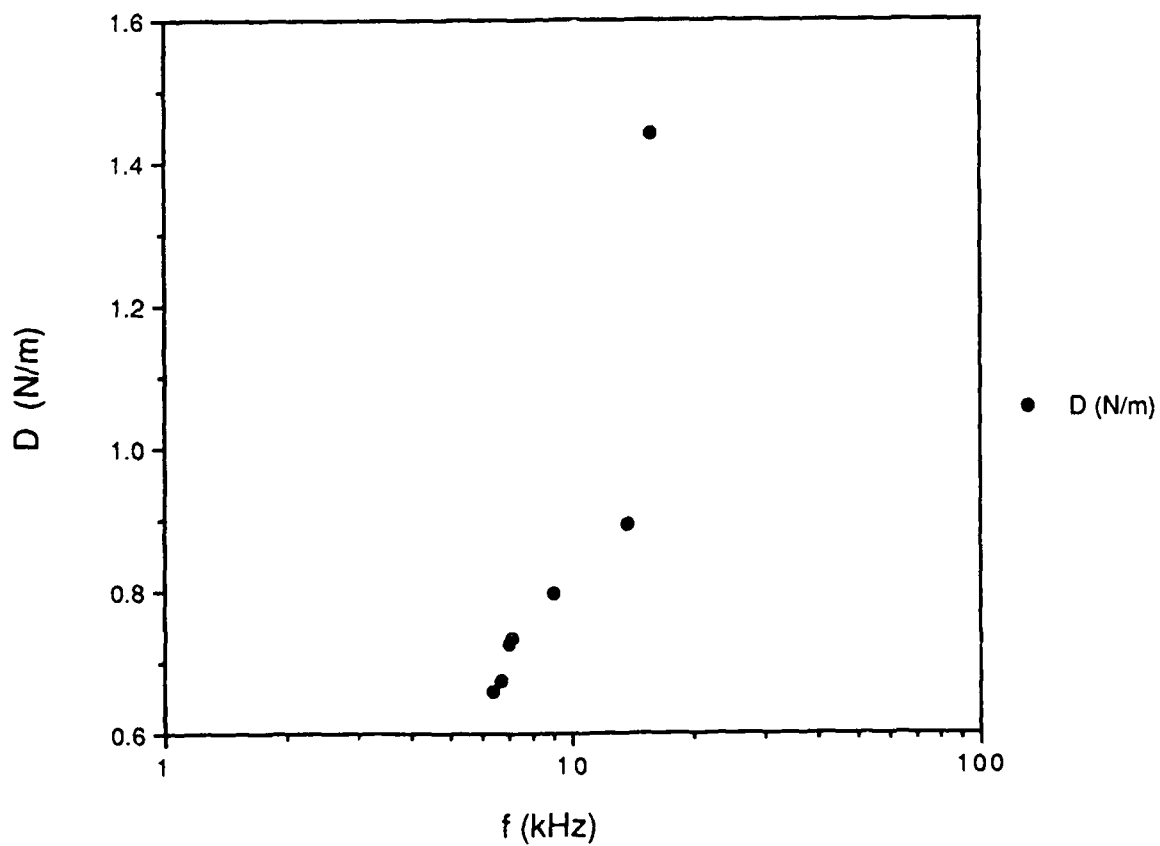
| | impact vel. | f (kHz) | sd of f | D (N/m) | sd of D | Bubble rad/mm | sd of rad |
|---|-------------|---------|---------|---------|---------|---------------|-----------|
| 1 | 1.207 | 9.050 | 4.809 | 0.797 | 0.305 | 0.362 | 0.193 |
| 2 | 1.289 | 6.957 | 1.017 | 0.725 | 0.065 | 0.471 | 0.069 |
| 3 | 1.391 | 6.377 | 0.767 | 0.657 | 0.110 | 0.514 | 0.062 |
| 4 | 1.459 | 6.661 | 0.247 | 0.672 | 0.025 | 0.492 | 0.018 |
| 5 | 1.522 | 7.124 | 0.244 | 0.735 | 0.062 | 0.460 | 0.016 |
| 6 | 1.583 | 13.785 | 11.822 | 0.892 | 0.195 | 0.238 | 0.204 |
| 7 | 1.642 | 15.768 | 8.605 | 1.440 | 0.517 | 0.208 | 0.114 |



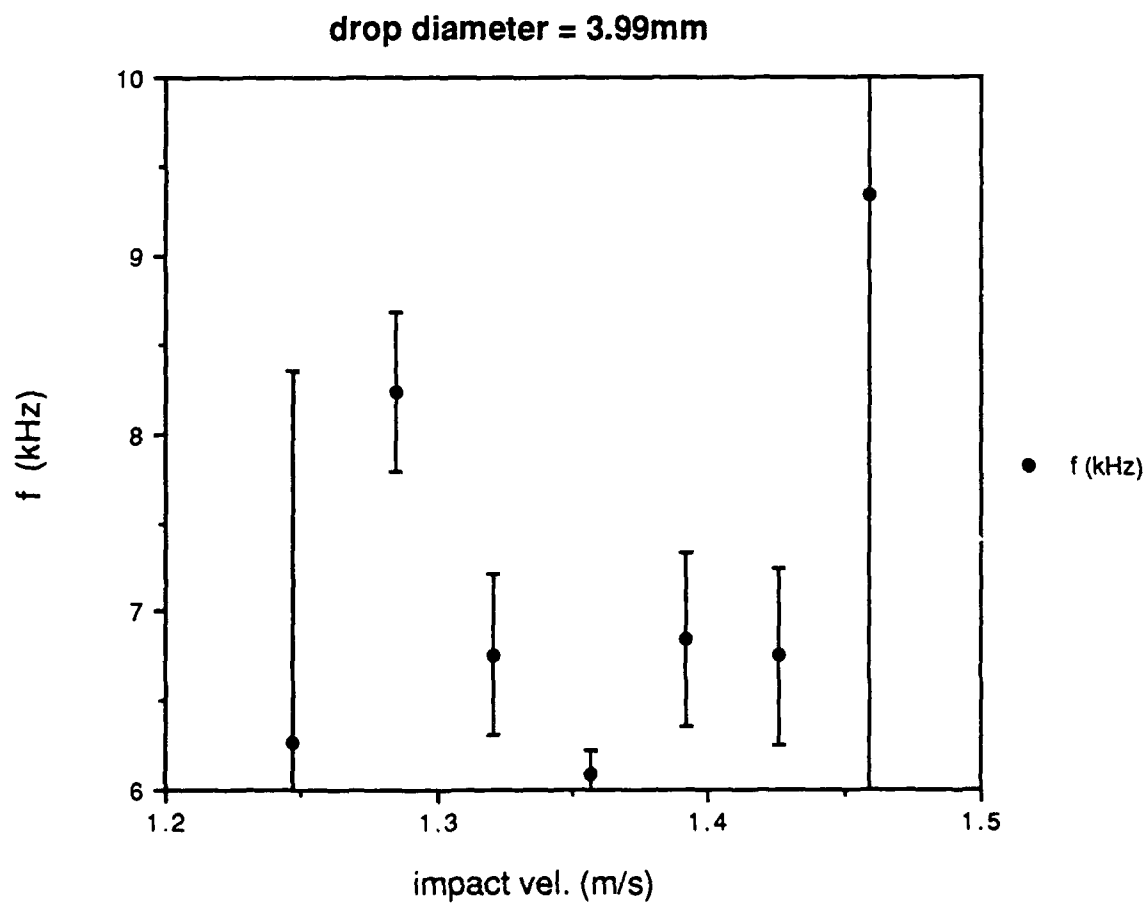
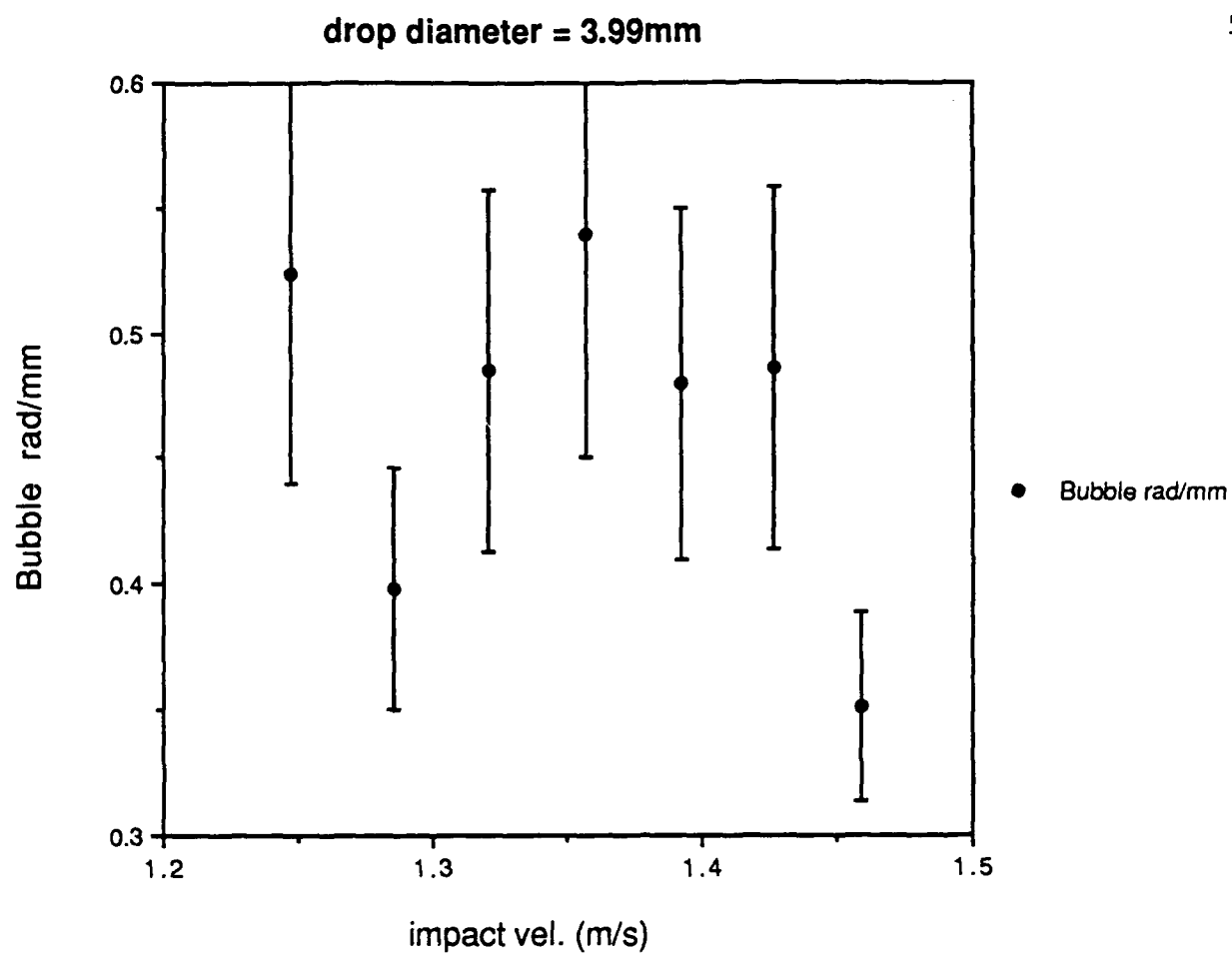
drop diameter = 3.73mm



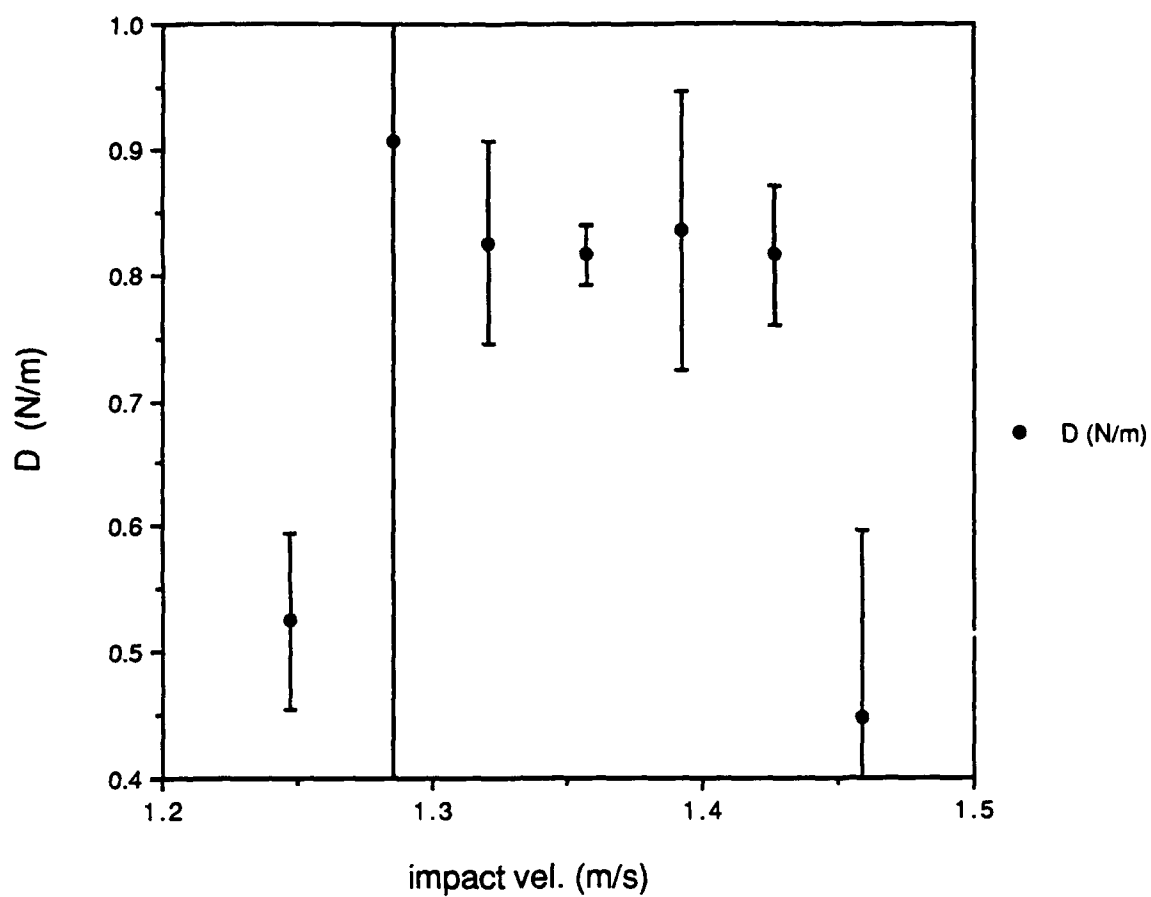
drop diameter = 3.73mm



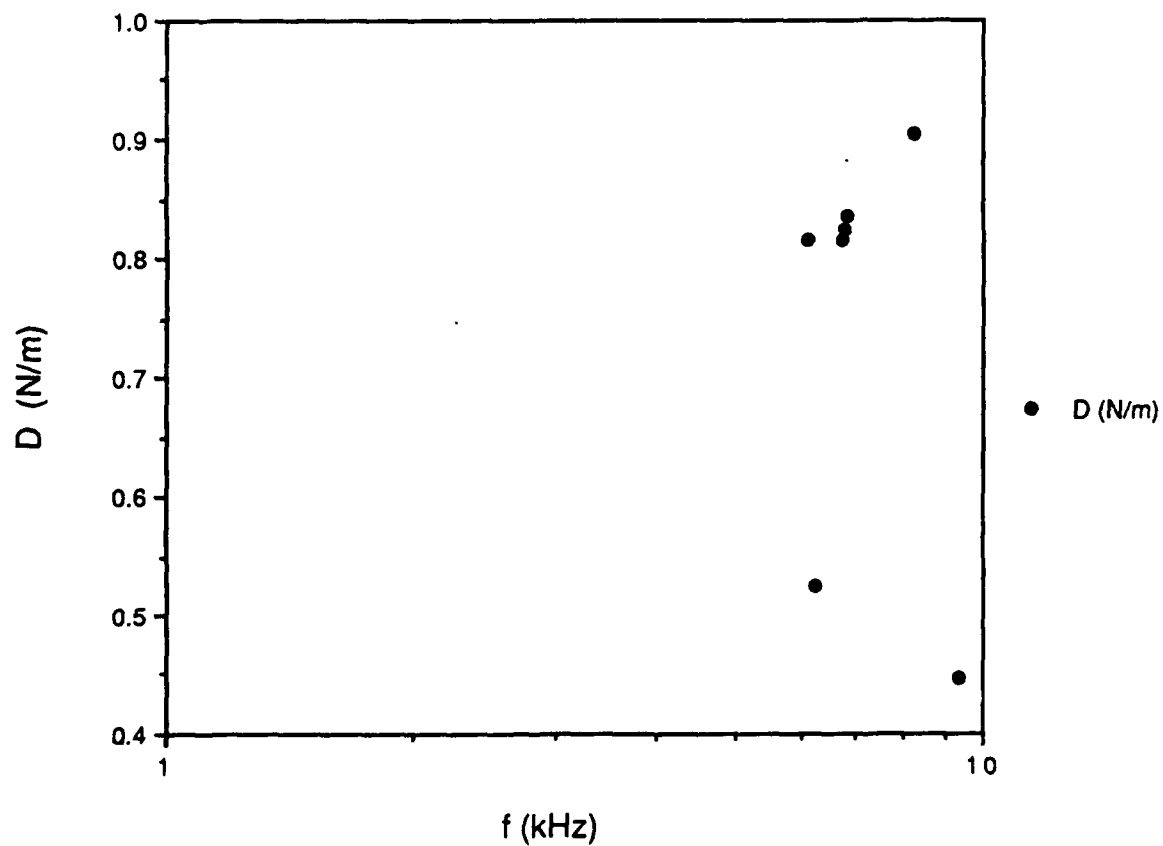
| | impact vel. | f (kHz) | sd of f | D (N/m) | sd of D | Bubble rad/mm | sd of rad |
|---|-------------|---------|---------|---------|---------|---------------|-----------|
| 1 | 1.247 | 6.265 | 2.088 | 0.525 | 0.070 | 0.524 | 0.084 |
| 2 | 1.321 | 6.761 | 0.452 | 0.825 | 0.080 | 0.485 | 0.072 |
| 3 | 1.392 | 6.842 | 0.488 | 0.835 | 0.110 | 0.479 | 0.070 |
| 4 | 1.285 | 8.240 | 0.448 | 0.906 | 0.510 | 0.398 | 0.048 |
| 5 | 1.357 | 6.085 | 0.137 | 0.815 | 0.025 | 0.539 | 0.089 |
| 6 | 1.426 | 6.749 | 0.494 | 0.815 | 0.055 | 0.486 | 0.072 |
| 7 | 1.459 | 9.331 | 3.556 | 0.448 | 0.150 | 0.352 | 0.038 |



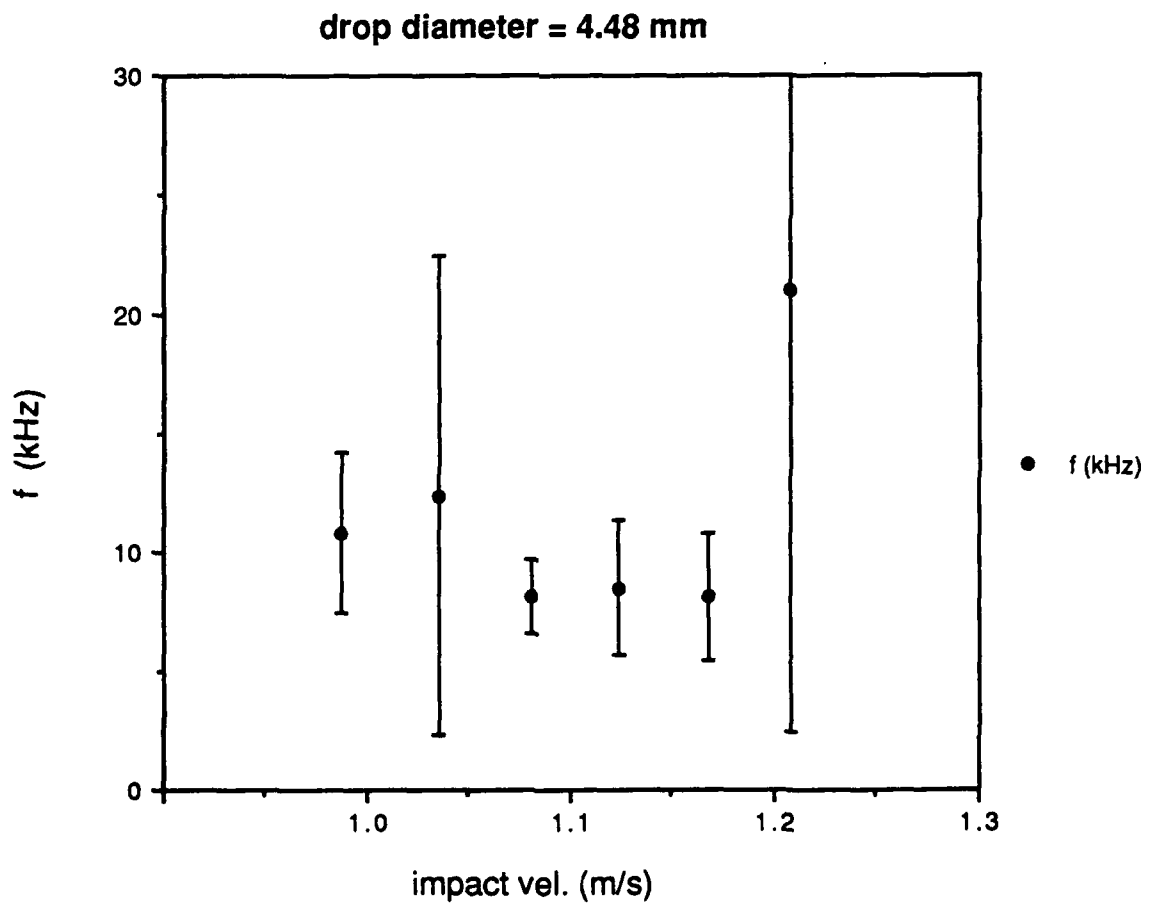
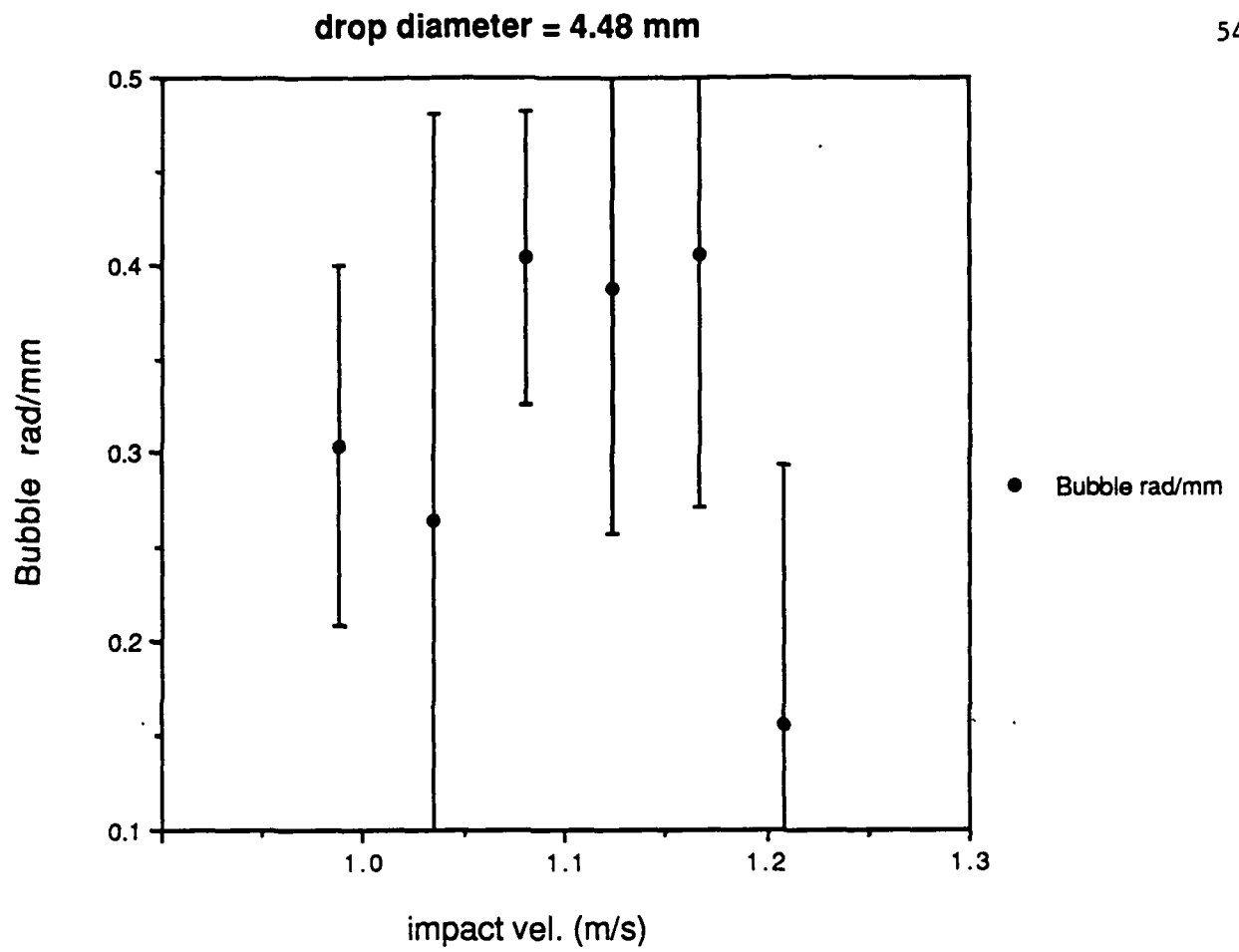
drop diameter = 3.99mm

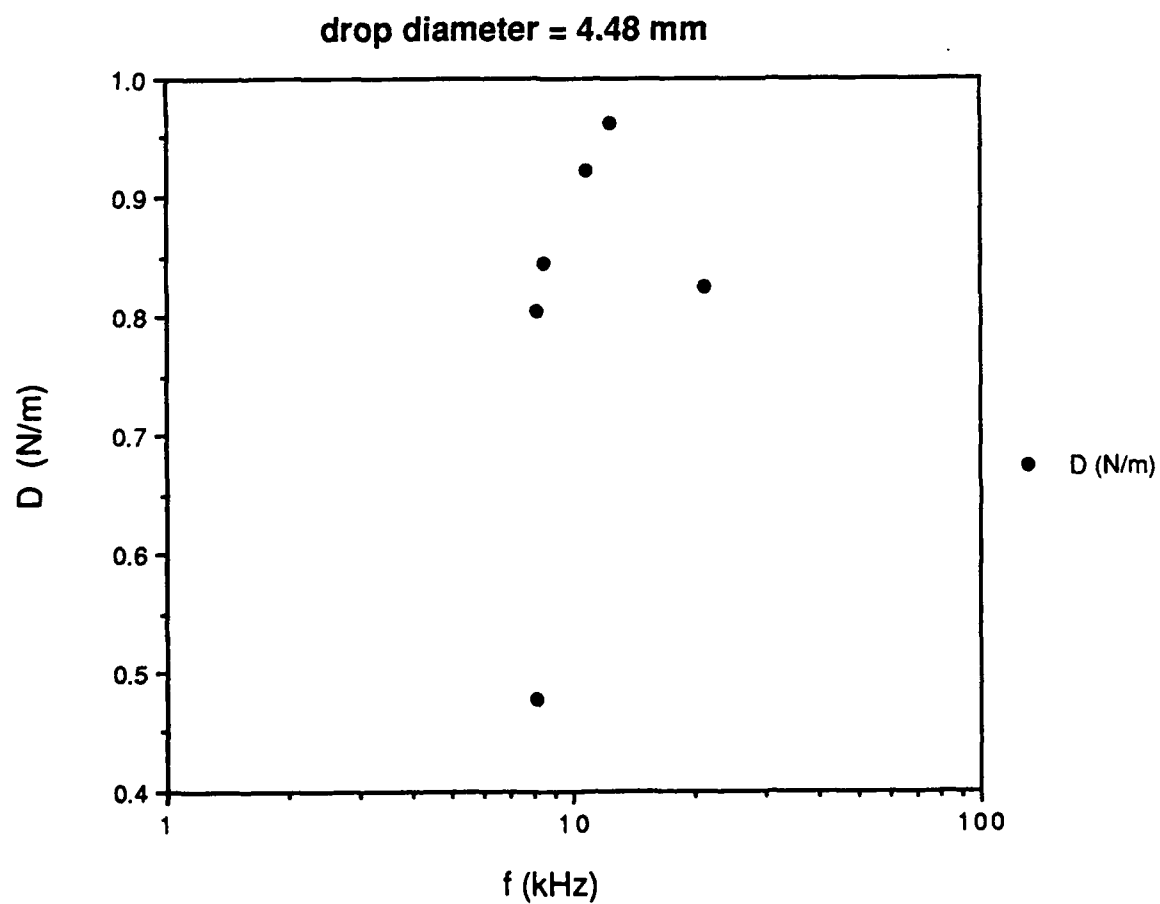
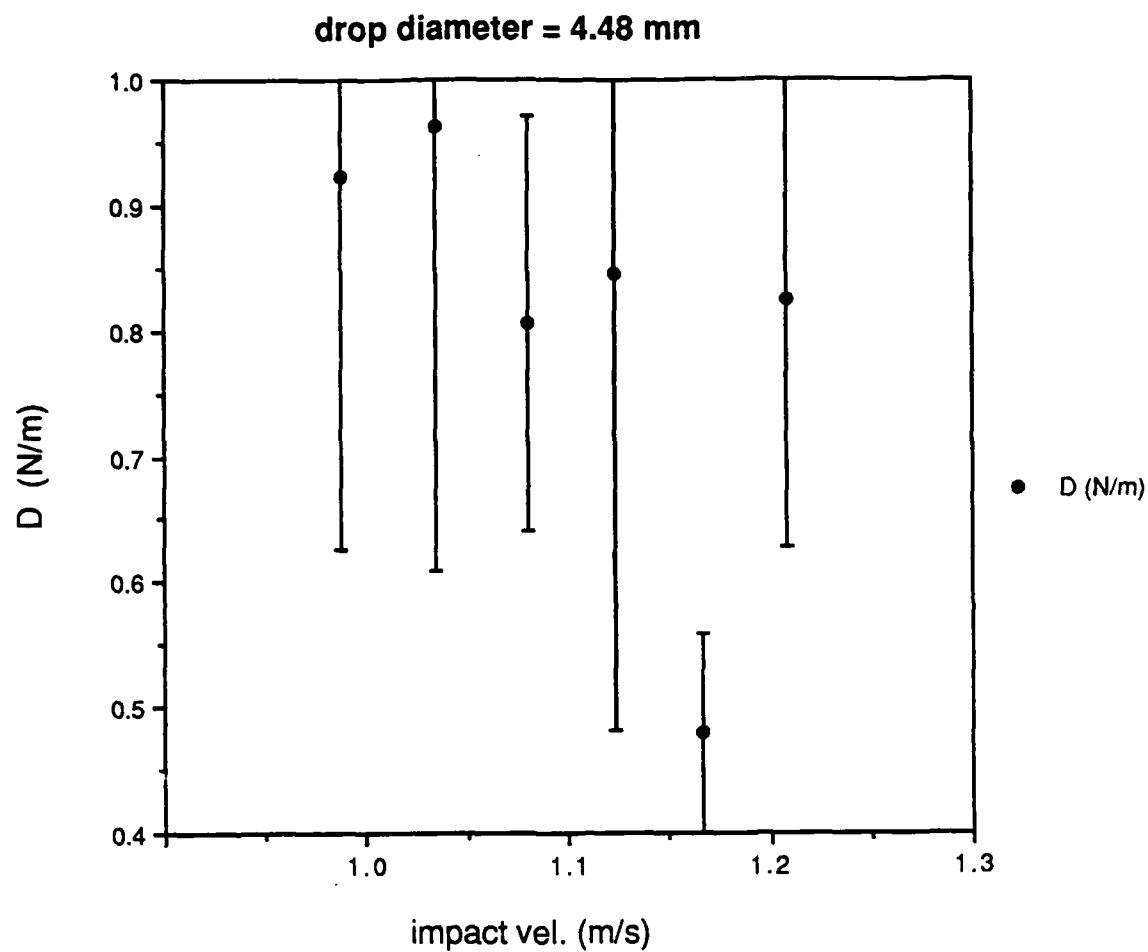


drop diameter = 3.99mm

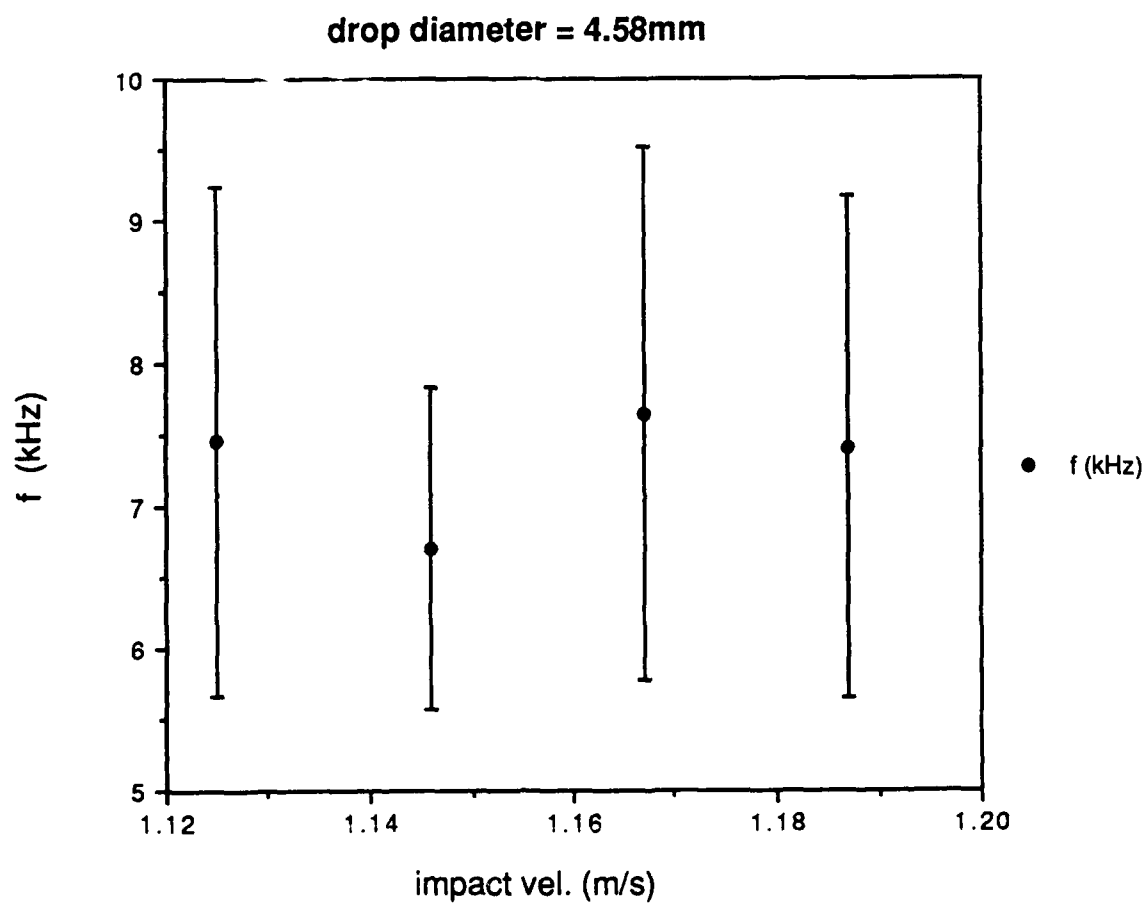
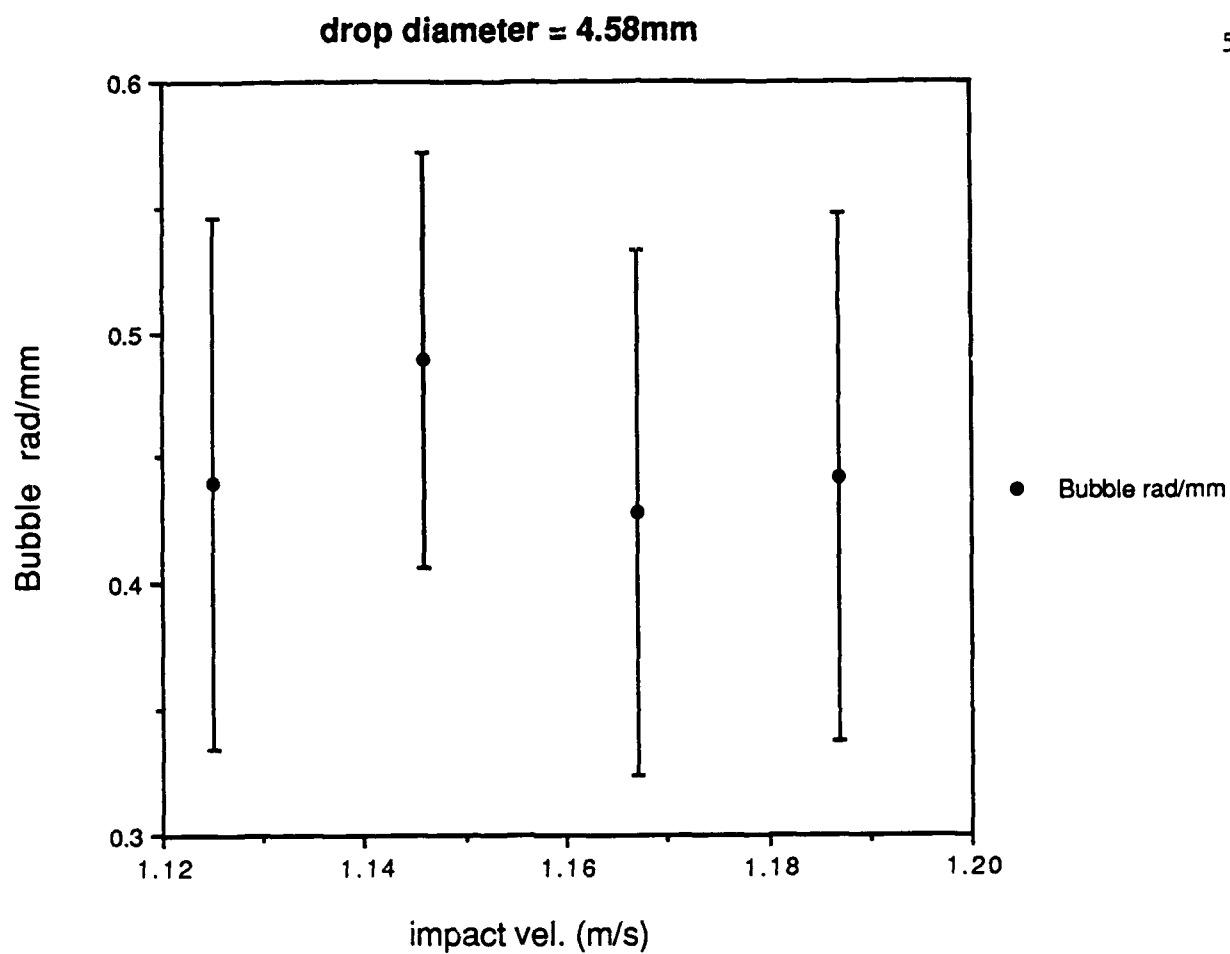


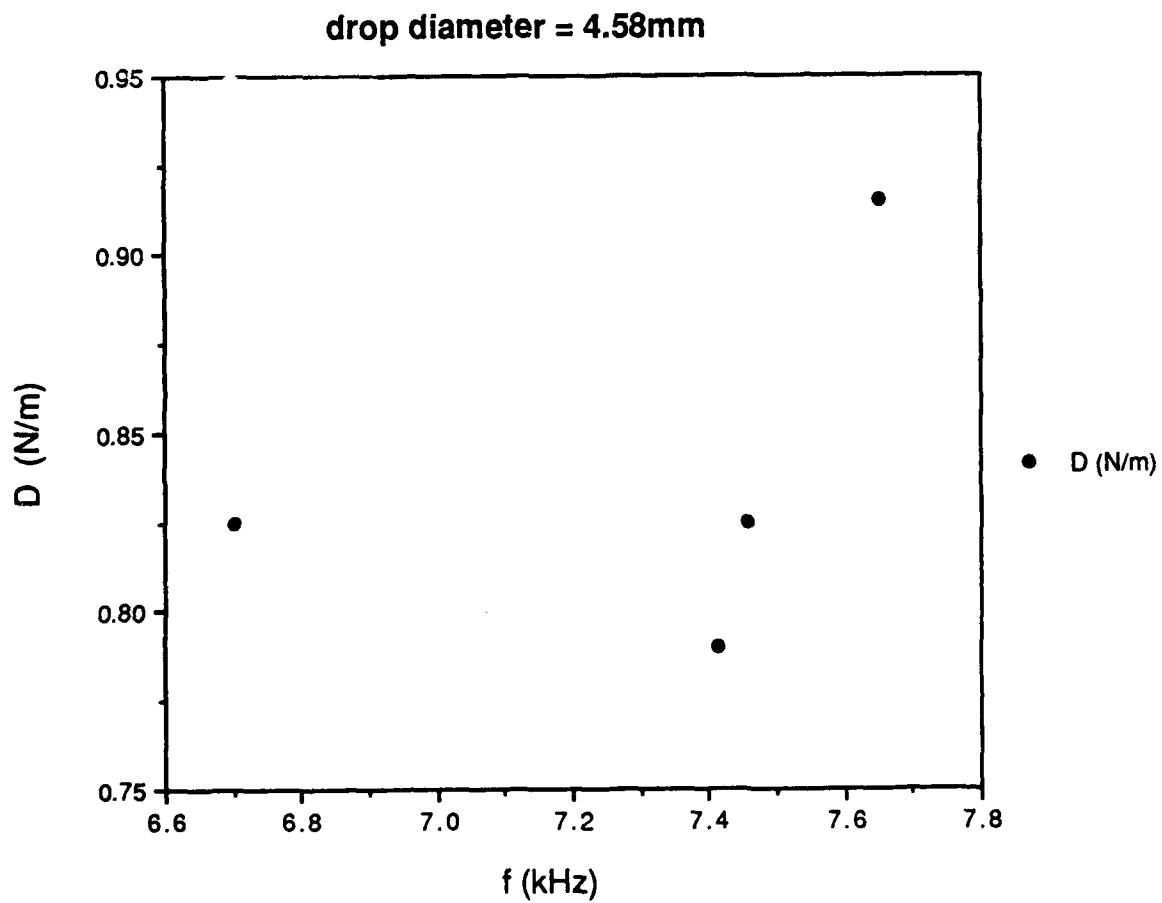
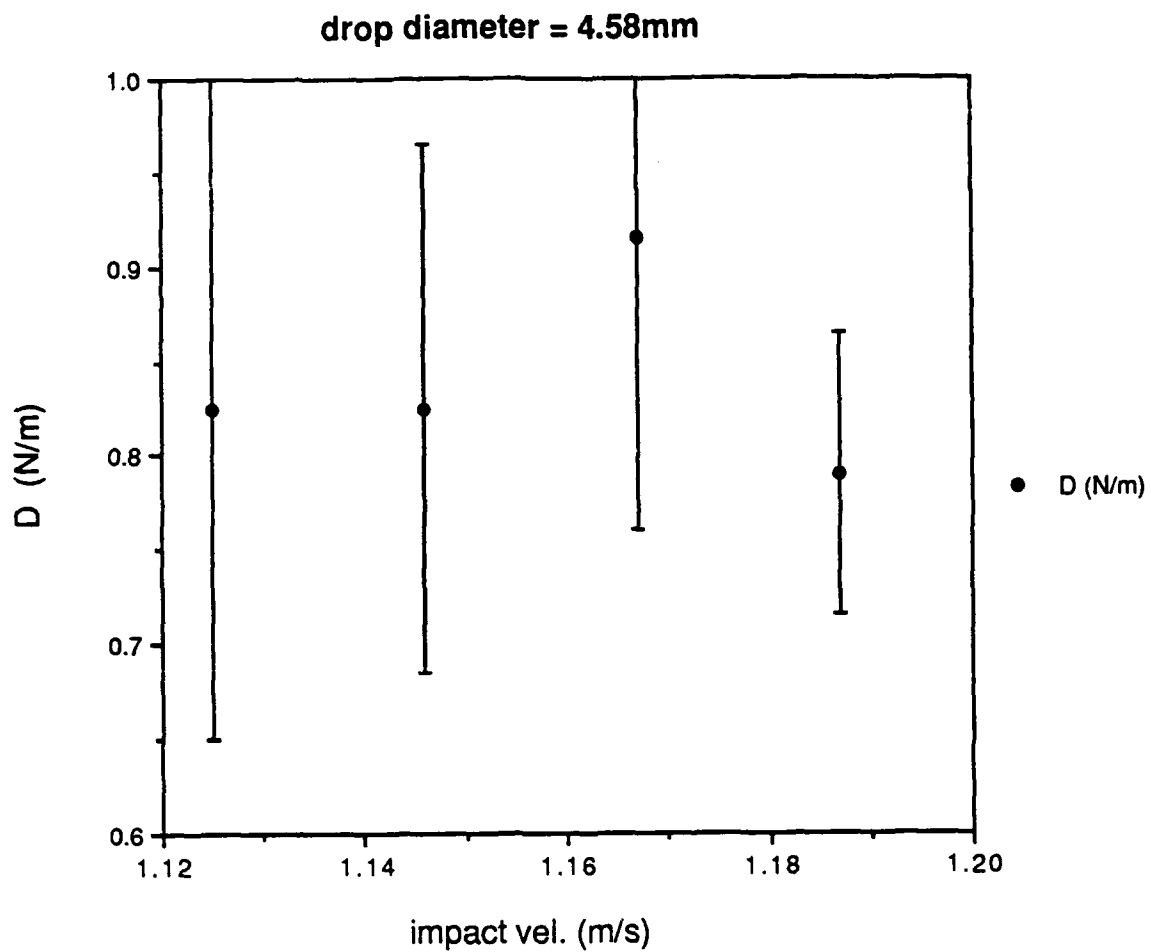
| | impact vel. | f (kHz) | sd of f | D (N/m) | sd of D | Bubble rad/mm | sd of rad |
|---|-------------|---------|---------|---------|---------|---------------|-----------|
| 1 | 1.035 | 12.377 | 10.077 | 0.963 | 0.352 | 0.265 | 0.216 |
| 2 | 1.124 | 8.488 | 2.826 | 0.845 | 0.362 | 0.386 | 0.129 |
| 3 | 0.987 | 10.790 | 3.400 | 0.922 | 0.295 | 0.304 | 0.096 |
| 4 | 1.167 | 8.082 | 2.680 | 0.479 | 0.080 | 0.406 | 0.135 |
| 5 | 1.081 | 8.132 | 1.576 | 0.805 | 0.165 | 0.403 | 0.078 |
| 6 | 1.208 | 21.017 | 18.564 | 0.825 | 0.198 | 0.156 | 0.138 |





| | impact vel. | f (kHz) | sd of f | D (N/m) | sd of D | Bubble rad/mm | sd of rad |
|---|-------------|---------|---------|---------|---------|---------------|-----------|
| 1 | 1.125 | 7.456 | 1.788 | 0.825 | 0.175 | 0.440 | 0.105 |
| 2 | 1.167 | 7.650 | 1.864 | 0.915 | 0.155 | 0.429 | 0.104 |
| 3 | 1.146 | 6.700 | 1.128 | 0.825 | 0.140 | 0.490 | 0.082 |
| 4 | 1.187 | 7.415 | 1.759 | 0.790 | 0.075 | 0.442 | 0.105 |





ANALYSIS OF DATA SET 1

The data seems to divide itself into three subsets. The first group encompasses drops 1.22 to 3.73 mm in diameter, the second for drops larger than 3.73 mm, and the third for drops smaller than 1.22 mm.

For the first group the plot of impact velocity versus bubble radii or frequency resembles a concave "U" shape. As impact velocity increases from zero through the point where entrainment begins, the bubble radius increases in size to a maximum value and then becomes smaller again as the highest entrainment velocity is reached. Regular entrainment discontinues after this point. The same sort of effect occurs with frequency, but since bubble radius is inversely proportional to frequency, the concavity is reversed. The graphs of the initial dipole strength versus impact velocity are similar to those for frequency versus impact velocity but with a "V" shaped rather than a "U" shaped pattern.* The variability of each data point is dependent on its impact velocity, being high if the impact velocity is near the upper or lower velocity limit and low if the impact velocity is in between the two limits. The final set of graphs in this group--initial dipole strength versus frequency--cannot be analyzed alone because there are not enough data points. However, some features can be determined if they are compared with Fig. 7, which plots 200 drops of the same size hitting the water at a constant speed. These graphs all show a monotonic rise in dipole strength with increased frequency. However, after a certain point the relationship is destroyed and prediction of initial dipole strength based on the knowledge of frequency is impossible.

With the exception of this last graph, the graphic features of the next two groups are different from first. The group consisting of drops larger than 3.73 mm has more of an isotropic behavior. From this point to the point where drops become too big to cause regular entrainment the curvature in the graphs is destroyed and the variance is constant among the points (Thus, one can conclude that entrainment is unstable in this region). The group made of drops smaller than 1.22 mm in diameter only partially displays characteristics of the first group. Since the drops' terminal velocities are lower than their highest entraining velocities, the graphs only show part a "U" or "V". If the drops could fall faster than their terminal velocities, the patterns would probably be complete.

Using the highest and lowest entrainment velocities observed in this study, a second graph of the range of impact velocities and drop diameters is displayed in Fig. 8. This range matches the one done in the earlier study, shown in Fig. 2a. The curves are the best fit curves of the observed lowest and highest entrainment velocities. From the

* The marring of this pattern in the graphs for drop diameters = 1.22 mm and 2.17 mm is probably due to contaminants in the water.

knowledge of the impact velocities and drop radii, Fig. 8 can be modified to show the range of regular entrainment based on kinetic energy and drop diameter, which is graphed in Fig. 9. Again, the curves are best fit curves of the highest and lowest entraining kinetic energies.

From the data, a determination of whether or not regular entrainment causes rain noise can be made. Fig. 10 shows an enlargement of Fig. 8 in the area where the upper and lower boundaries of the entrainment intersect the terminal velocity curve. Raindrops entraining bubbles at terminal velocity are symbolized by diamonds; the frequencies of the bubbles are listed beside them. Since most of the bubbles entrained by drops falling at terminal velocity oscillate around 12 to 14 kHz, regular entrainment must be the cause of the 14 kHz peak found in the spectrum of natural rainfall and the source of rain noise underwater.

At one point during the study, the peak was believed to be caused by the 14 kHz bubbles being the most in number and the loudest. However, for bubbles entrained by drops falling at terminal velocity, the dipole strengths of 14 kHz bubbles are usually lower than those oscillating at 20 to 40 kHz. Therefore, the peak must be due only to the amount of bubbles attributed to it.

Figures 11 and 12 display the data in the form of contour graphs. The first one, showing similar regions of initial dipole strength for the entrainment region, indicates that dipole strength weakens as drop diameter is decreased. The other graph, displaying similar areas of frequency or bubble radius, shows that frequency steadily increases as drop diameter decreases.

EXPLANATION OF DATA SET 2

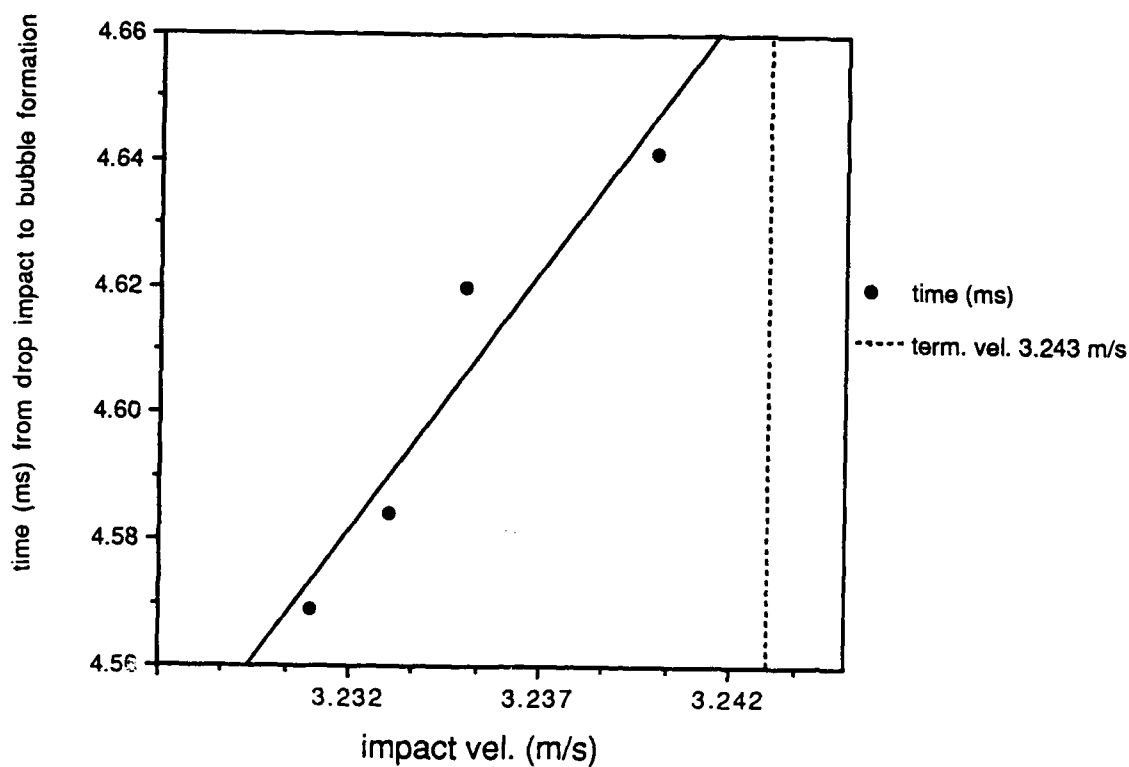
The second set of data measures the impact velocity and time required for the bubble to form after drop impact. Impact velocities are measured in meters per second and time is in milliseconds. As before, each row represents the average of thirty trials. After each data sheet are two graphs which plot both the relationship between the time and the impact velocity. However, the top graph is a logarithmic curve fit to the data while the bottom is a linear fit. Again, the drop diameter is listed at the top of each table, and the dates and times are unimportant.

DATA SET 2

| | impact vel. | time (ms) |
|---|-------------|-----------|
| 1 | 3.240 | 4.641 |
| 2 | 3.235 | 4.620 |
| 3 | 3.233 | 4.584 |
| 4 | 3.231 | 4.569 |

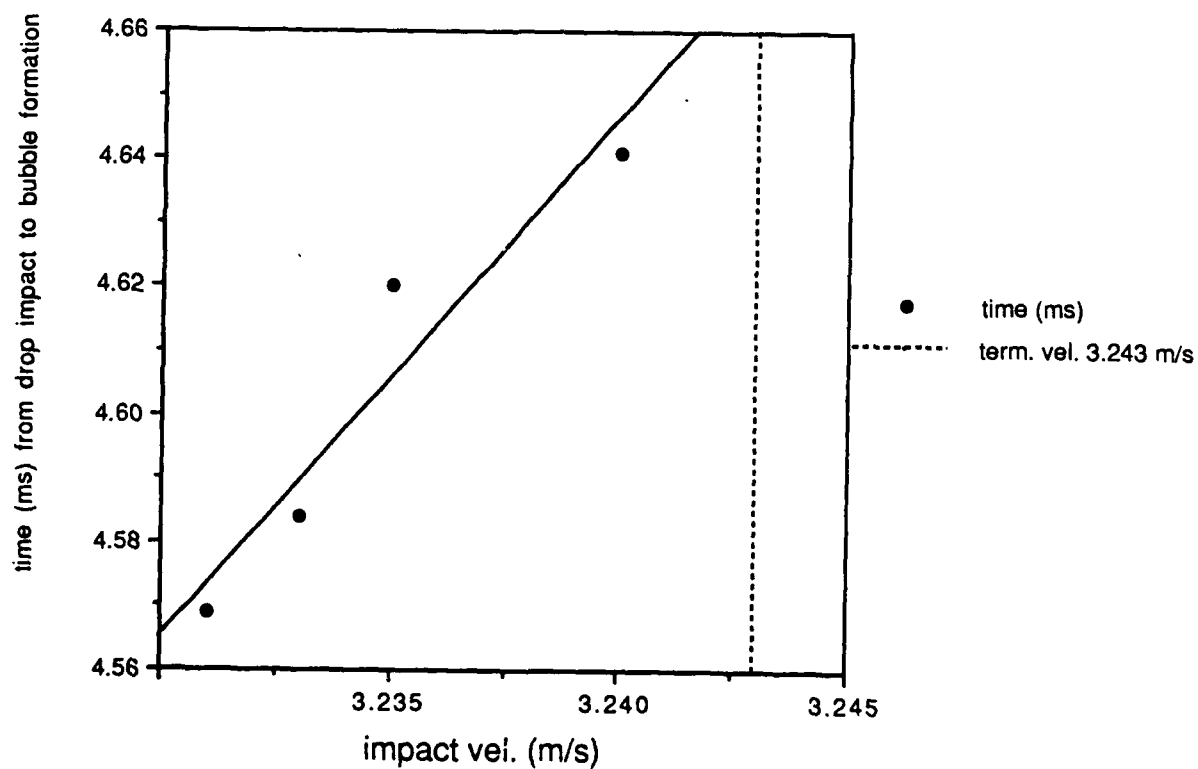
drop diameter = 0.79mm

$$y = -21.744 + 8.1452x \quad R^2 = 0.914$$



drop diameter = 0.79mm

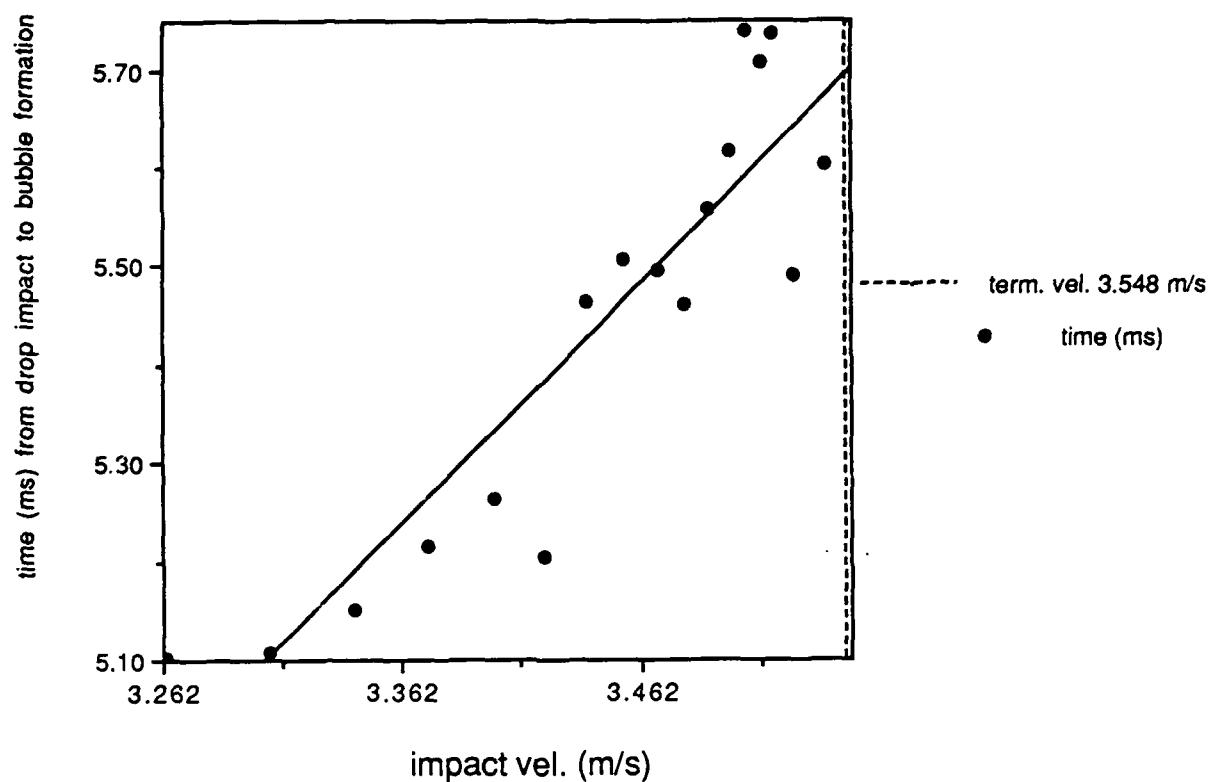
$$y = 5.5704e-3 * x^{5.7218} \quad R^2 = 0.913$$



| | impact vel. | time (ms) |
|----|-------------|-----------|
| 1 | 3.526 | 5.490 |
| 2 | 3.517 | 5.737 |
| 3 | 3.512 | 5.708 |
| 4 | 3.506 | 5.740 |
| 5 | 3.499 | 5.616 |
| 6 | 3.490 | 5.558 |
| 7 | 3.480 | 5.462 |
| 8 | 3.469 | 5.496 |
| 9 | 3.455 | 5.506 |
| 10 | 3.439 | 5.464 |
| 11 | 3.421 | 5.204 |
| 12 | 3.401 | 5.263 |
| 13 | 3.373 | 5.214 |
| 14 | 3.342 | 5.152 |
| 15 | 3.306 | 5.108 |
| 16 | 3.263 | 5.102 |
| 17 | 3.539 | 5.604 |

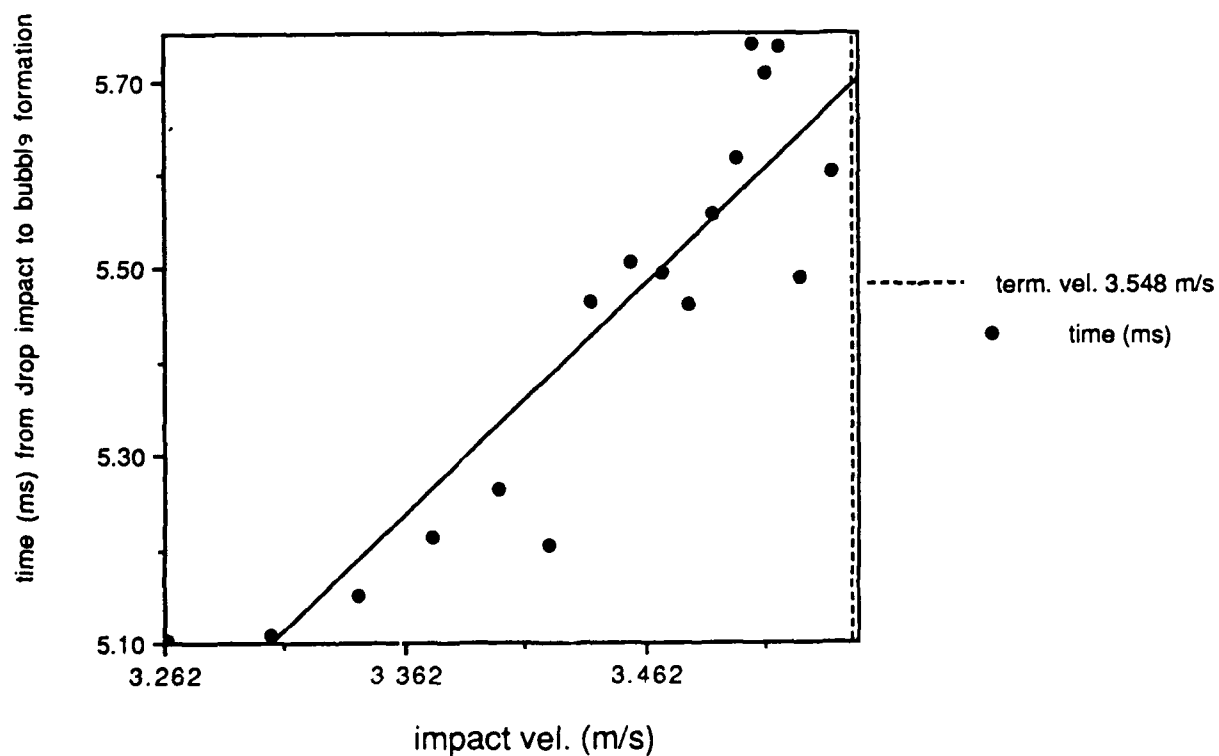
drop diameter = 0.87mm

$$y = 0.79549 * x^{1.5541} \quad R^2 = 0.831$$



drop diameter = 0.87mm

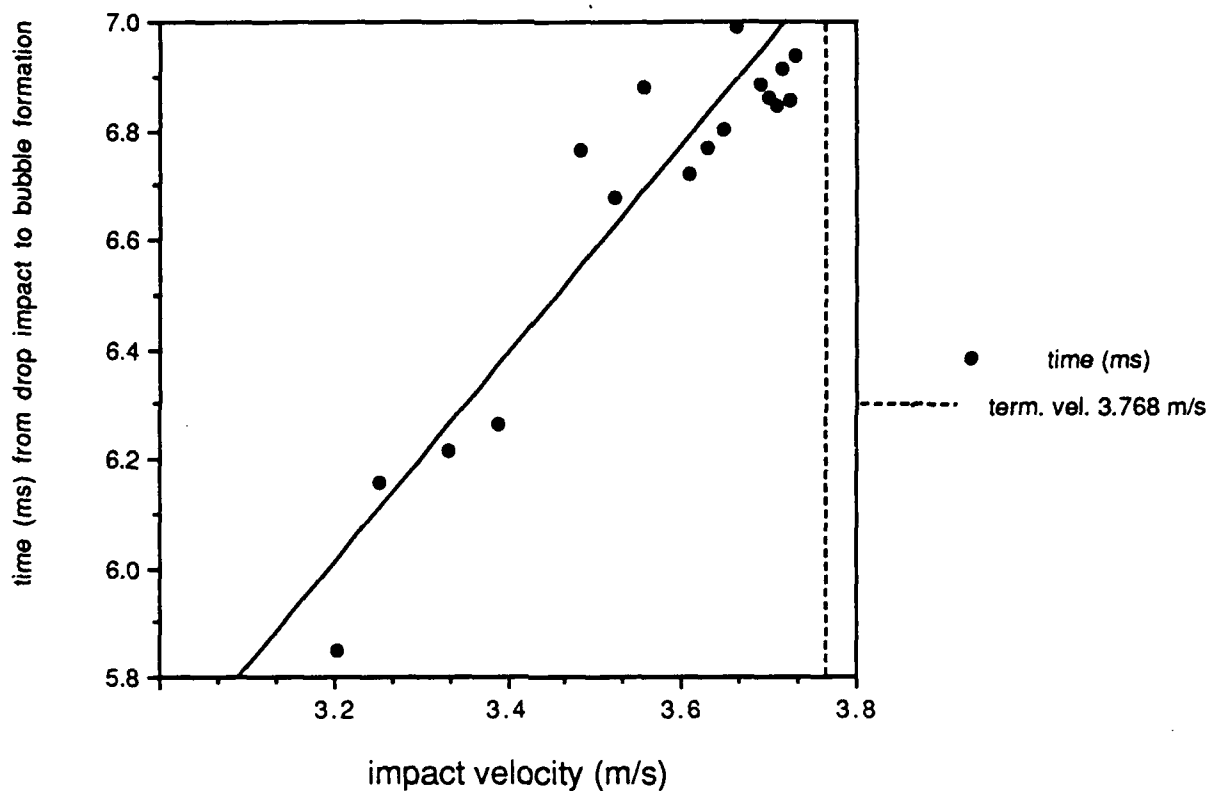
$$y = -3.0285 + 2.4584x \quad R^2 = 0.826$$



| | impact vel. | time (ms) |
|----|-------------|-----------|
| 1 | 3.204 | 5.847 |
| 2 | 3.253 | 6.155 |
| 3 | 3.331 | 6.216 |
| 4 | 3.390 | 6.265 |
| 5 | 3.485 | 6.763 |
| 6 | 3.523 | 6.679 |
| 7 | 3.558 | 6.881 |
| 8 | 3.583 | 7.081 |
| 9 | 3.608 | 6.720 |
| 10 | 3.629 | 6.769 |
| 11 | 3.647 | 6.804 |
| 12 | 3.663 | 6.991 |
| 13 | 3.677 | 7.044 |
| 14 | 3.689 | 6.886 |
| 15 | 3.699 | 6.860 |
| 16 | 3.708 | 6.847 |
| 17 | 3.716 | 6.913 |
| 18 | 3.723 | 6.855 |
| 19 | 3.723 | 6.937 |

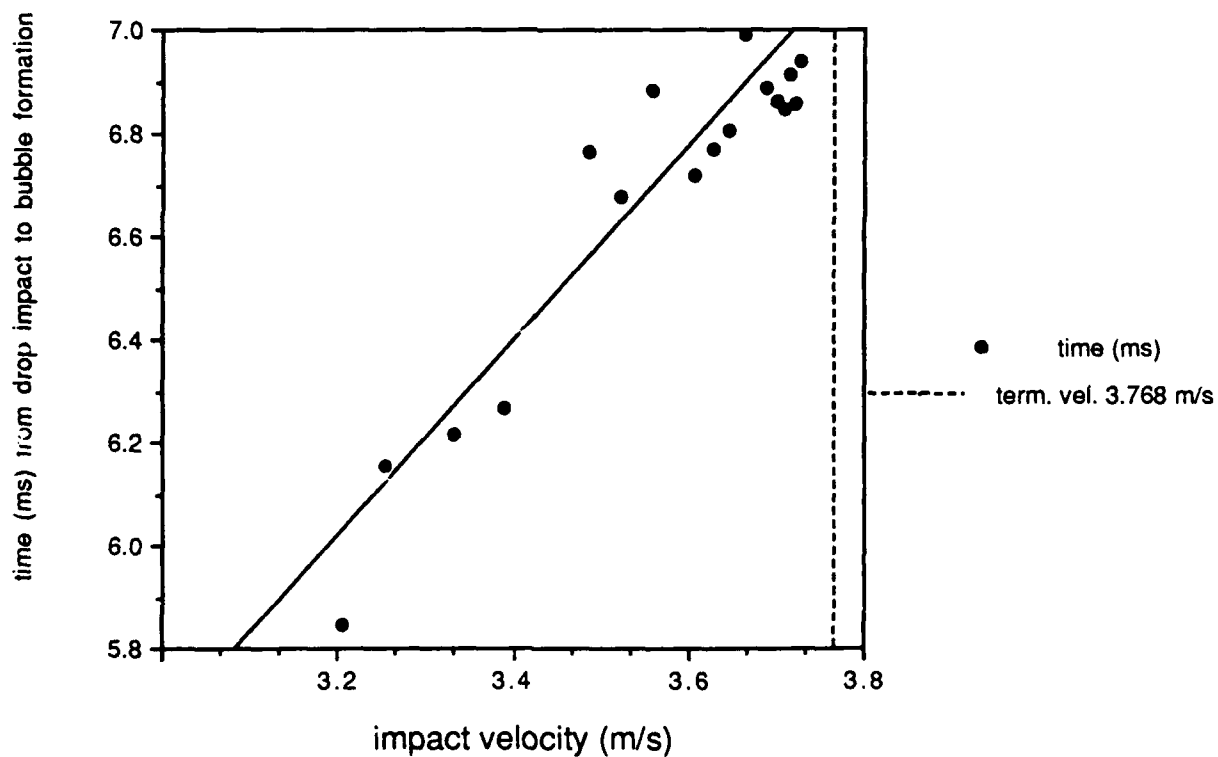
drop diameter = 0.93mm

$$y = 1.8427 * x^{1.0157} \quad R^2 = 0.844$$



drop diameter = 0.93mm

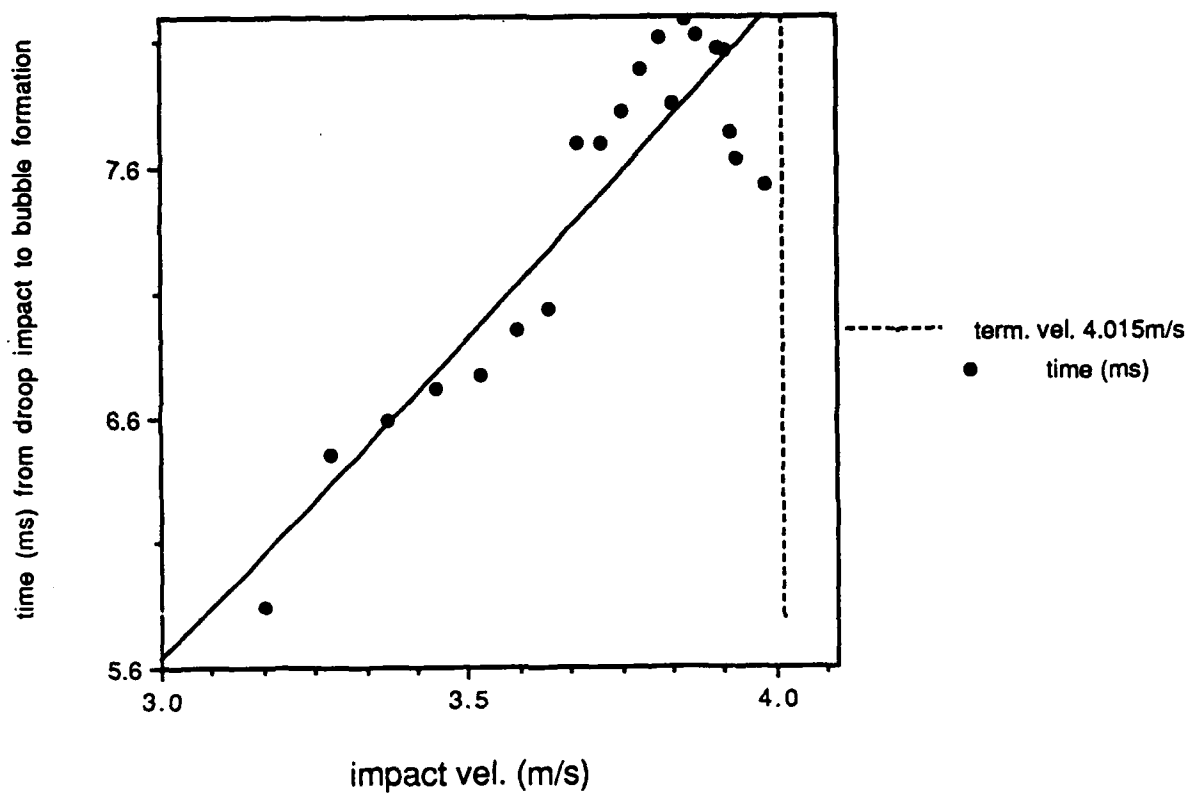
$$y = 9.0771e-3 + 1.8778x \quad R^2 = 0.832$$



| | impact vel. | time (ms) |
|----|-------------|-----------|
| 1 | 3.167 | 5.847 |
| 2 | 3.275 | 6.453 |
| 3 | 3.368 | 6.592 |
| 4 | 3.449 | 6.714 |
| 5 | 3.518 | 6.768 |
| 6 | 3.579 | 6.952 |
| 7 | 3.631 | 7.030 |
| 8 | 3.677 | 7.692 |
| 9 | 3.717 | 7.696 |
| 10 | 3.753 | 7.826 |
| 11 | 3.784 | 7.986 |
| 12 | 3.811 | 8.113 |
| 13 | 3.835 | 7.848 |
| 14 | 3.856 | 8.188 |
| 15 | 3.874 | 8.126 |
| 16 | 3.905 | 8.075 |
| 17 | 3.918 | 8.062 |
| 18 | 3.929 | 7.736 |
| 19 | 3.938 | 7.627 |
| 20 | 3.983 | 7.522 |

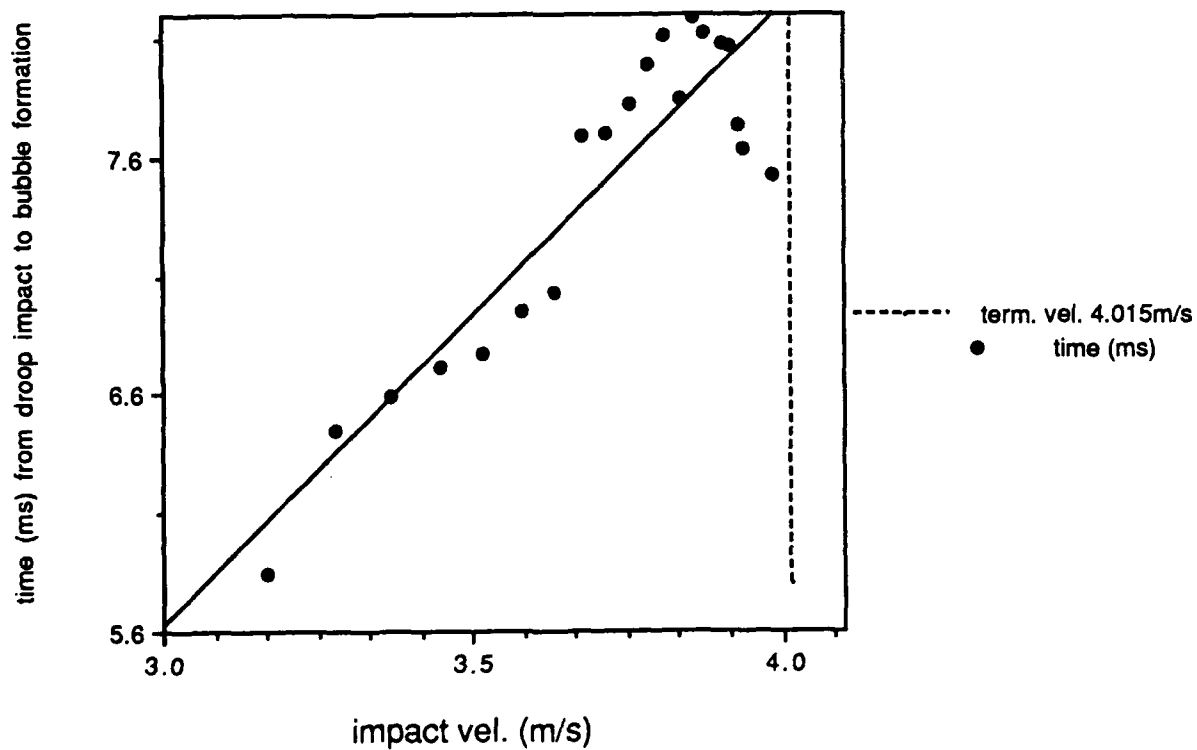
drop diameter = 1.00mm

$$y = 1.3061 \cdot x^{1.3294} \quad R^2 = 0.846$$



drop diameter = 1.00mm

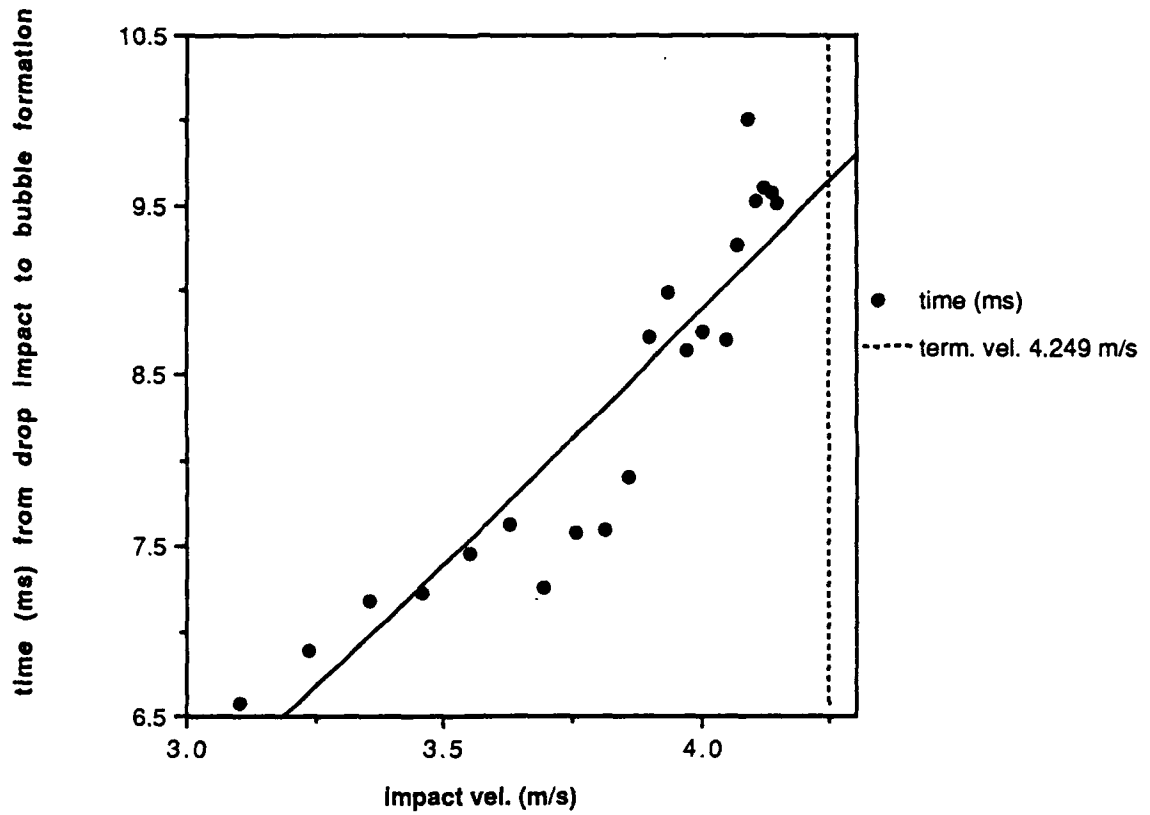
$$y = -2.1907 + 2.6048x \quad R^2 = 0.825$$



| | final vel. | time (ms) |
|----|------------|-----------|
| 1 | 3.101 | 6.573 |
| 2 | 3.238 | 6.881 |
| 3 | 3.356 | 7.176 |
| 4 | 3.459 | 7.232 |
| 5 | 3.549 | 7.460 |
| 6 | 3.627 | 7.633 |
| 7 | 3.696 | 7.257 |
| 8 | 3.757 | 7.587 |
| 9 | 3.810 | 7.594 |
| 10 | 3.858 | 7.903 |
| 11 | 3.900 | 8.725 |
| 12 | 3.937 | 8.994 |
| 13 | 3.971 | 8.639 |
| 14 | 4.000 | 8.756 |
| 15 | 4.050 | 8.703 |
| 16 | 4.071 | 9.261 |
| 17 | 4.090 | 10.013 |
| 18 | 4.106 | 9.531 |
| 19 | 4.121 | 9.607 |
| 20 | 4.138 | 9.567 |
| 21 | 4.147 | 9.509 |

drop diameter = 1.07mm

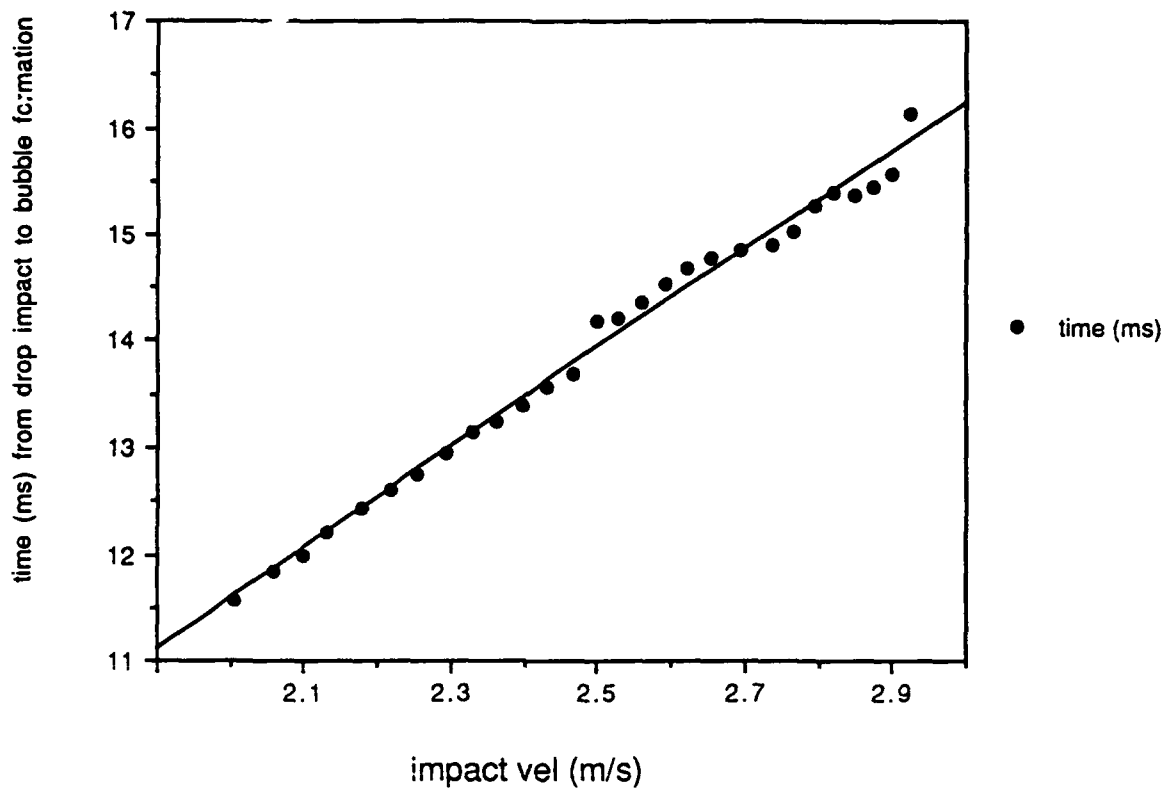
$$y = 1.3151 * x^{1.3767} \quad R^2 = 0.857$$



| | impact vel | time (ms) |
|----|------------|-----------|
| 1 | 2.004 | 11.560 |
| 2 | 2.058 | 11.840 |
| 3 | 2.099 | 12.000 |
| 4 | 2.130 | 12.220 |
| 5 | 2.179 | 12.420 |
| 6 | 2.217 | 12.600 |
| 7 | 2.255 | 12.760 |
| 8 | 2.292 | 12.940 |
| 9 | 2.328 | 13.140 |
| 10 | 2.363 | 13.240 |
| 11 | 2.397 | 13.400 |
| 12 | 2.431 | 13.560 |
| 13 | 2.465 | 13.700 |
| 14 | 2.497 | 14.180 |
| 15 | 2.529 | 14.220 |
| 16 | 2.561 | 14.360 |
| 17 | 2.591 | 14.520 |
| 18 | 2.622 | 14.680 |
| 19 | 2.652 | 14.780 |
| 20 | 2.695 | 14.850 |
| 21 | 2.738 | 14.910 |
| 22 | 2.766 | 15.030 |
| 23 | 2.794 | 15.280 |
| 24 | 2.821 | 15.400 |
| 25 | 2.847 | 15.370 |
| 26 | 2.874 | 15.440 |
| 27 | 2.900 | 15.560 |
| 28 | 2.925 | 16.140 |

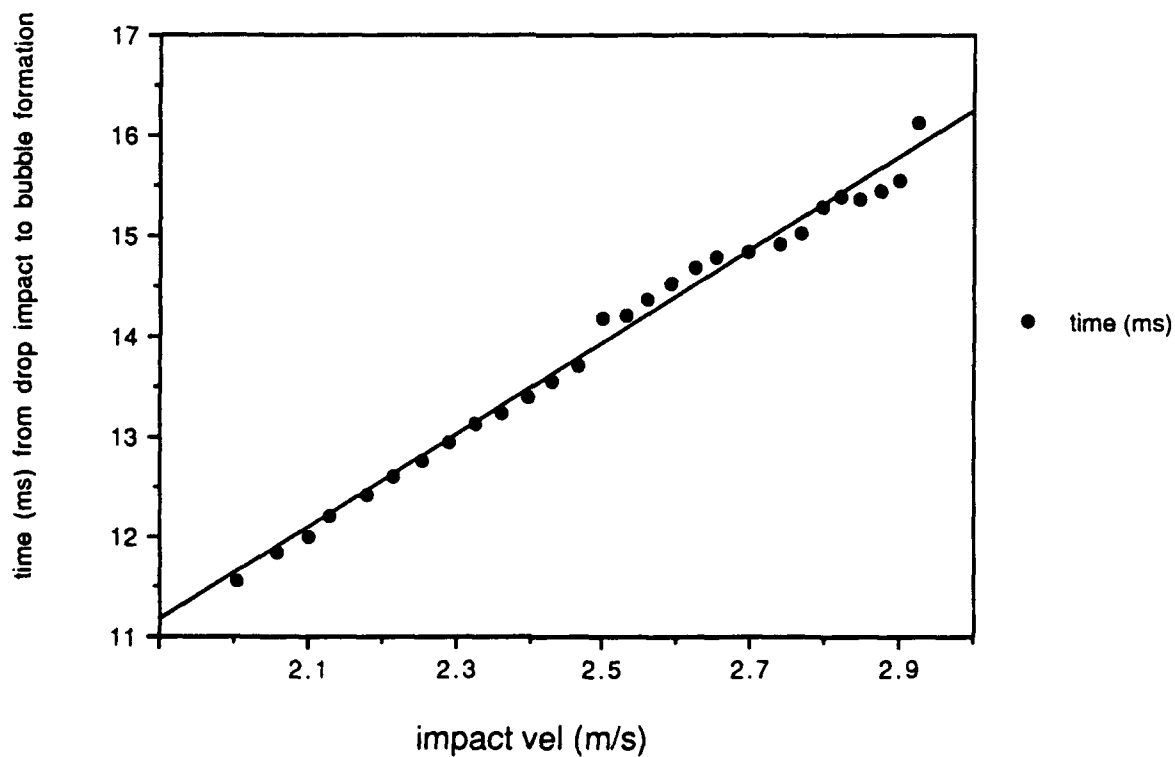
drop diameter = 1.71mm

$$y = 6.5009 * x^{0.83239} \quad R^2 = 0.992$$



drop diameter = 1.71mm

$$y = 2.3442 + 4.6332x \quad R^2 = 0.990$$

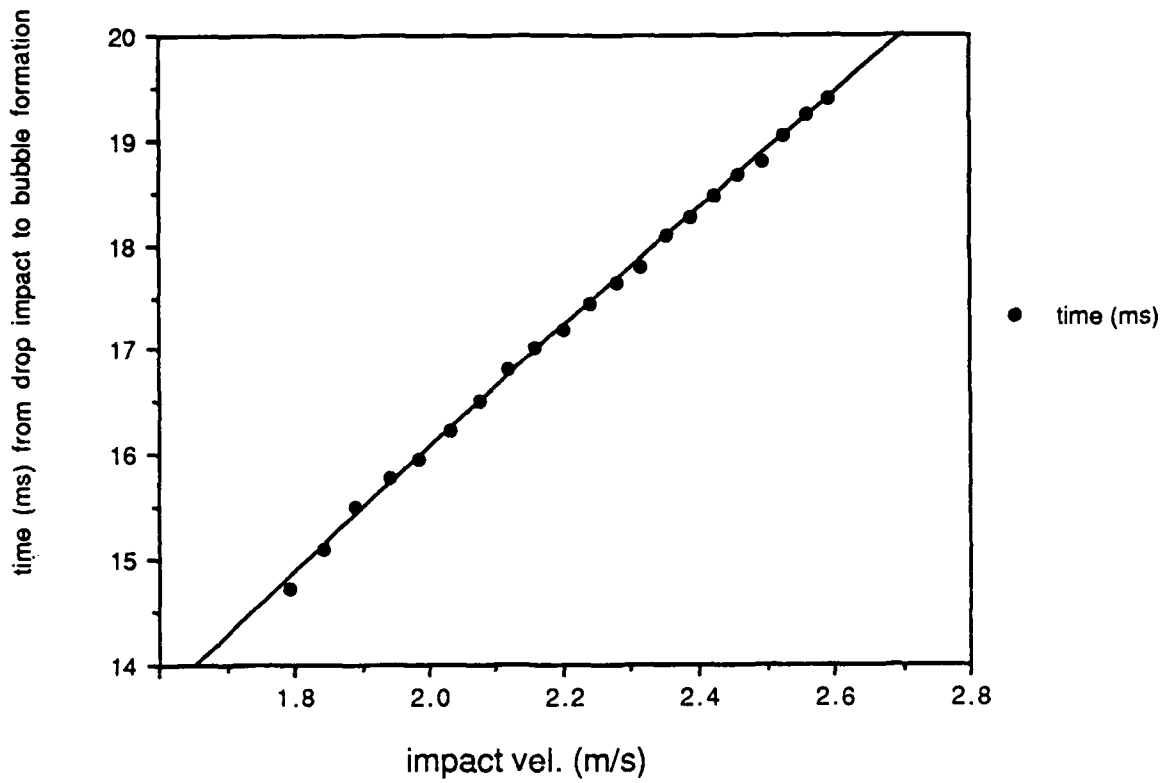


| | impact vel. | time (ms) |
|----|-------------|-----------|
| 1 | 1.794 | 14.720 |
| 2 | 1.844 | 15.100 |
| 3 | 1.890 | 15.500 |
| 4 | 1.940 | 15.780 |
| 5 | 1.986 | 15.970 |
| 6 | 2.031 | 16.230 |
| 7 | 2.074 | 16.520 |
| 8 | 2.117 | 16.800 |
| 9 | 2.158 | 17.000 |
| 10 | 2.199 | 17.200 |
| 11 | 2.238 | 17.440 |
| 12 | 2.277 | 17.640 |
| 13 | 2.315 | 17.800 |
| 14 | 2.352 | 18.080 |
| 15 | 2.389 | 18.280 |
| 16 | 2.424 | 18.460 |
| 17 | 2.459 | 18.680 |
| 18 | 2.494 | 18.800 |
| 19 | 2.527 | 19.040 |
| 20 | 2.561 | 19.240 |
| 21 | 2.594 | 19.400 |

drop diameter = 2.17mm

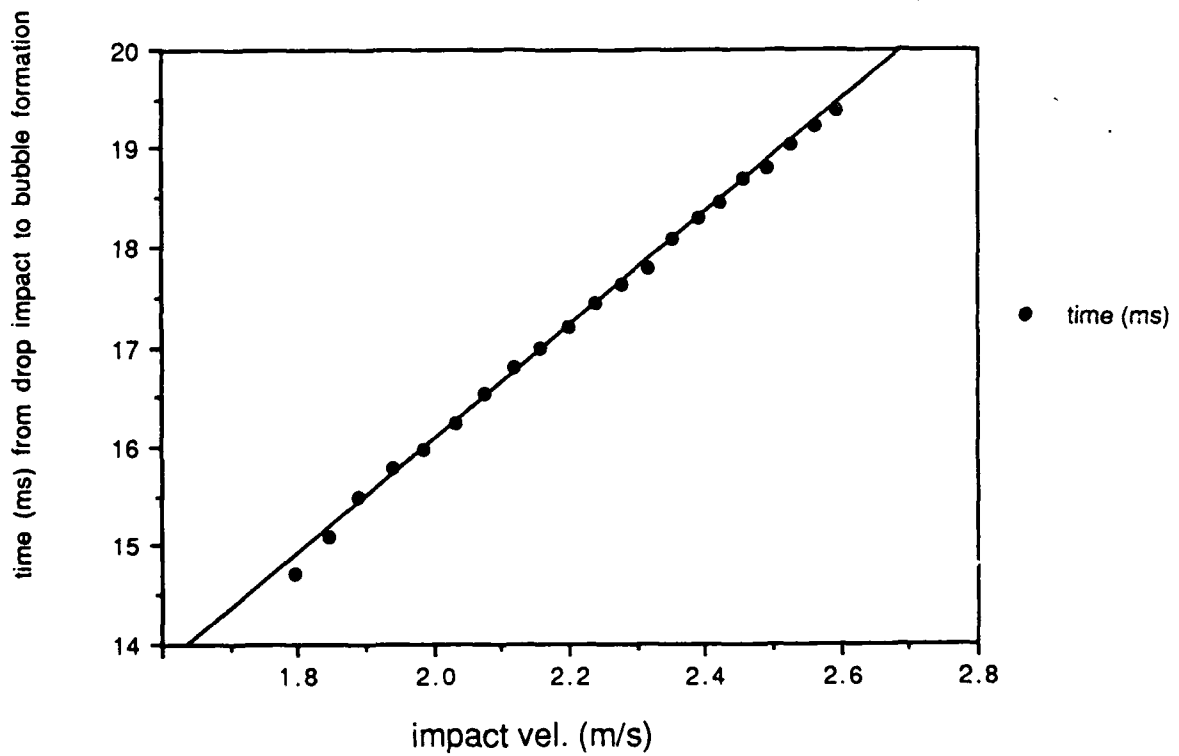
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$$y = 9.6971 * x^{0.72782} \quad R^2 = 0.999$$



drop diameter = 2.17mm

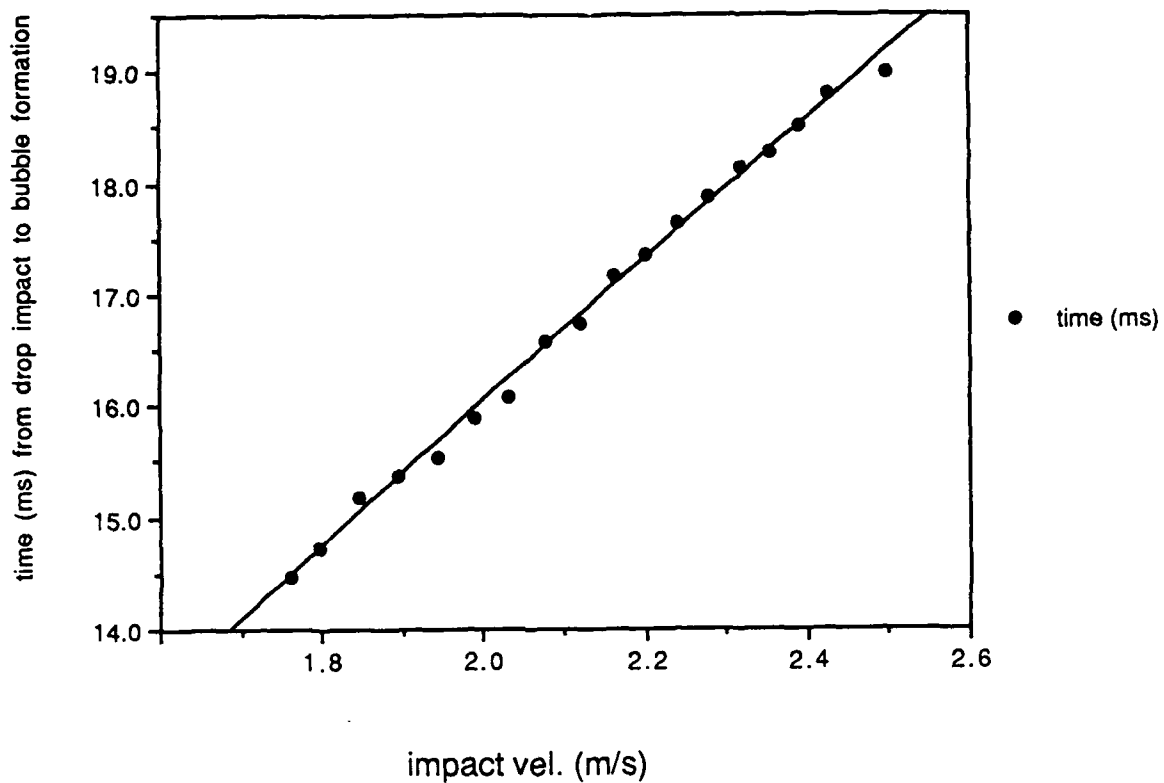
$$y = 4.6711 + 5.6916x \quad R^2 = 0.998$$



| | impact vel. | time (ms) |
|----|-------------|-----------|
| 1 | 1.760 | 14.480 |
| 2 | 1.796 | 14.720 |
| 3 | 1.846 | 15.180 |
| 4 | 1.895 | 15.360 |
| 5 | 1.942 | 15.530 |
| 6 | 1.988 | 15.890 |
| 7 | 2.033 | 16.080 |
| 8 | 2.077 | 16.570 |
| 9 | 2.119 | 16.750 |
| 10 | 2.161 | 17.170 |
| 11 | 2.202 | 17.350 |
| 12 | 2.241 | 17.640 |
| 13 | 2.280 | 17.880 |
| 14 | 2.318 | 18.130 |
| 15 | 2.356 | 18.280 |
| 16 | 2.392 | 18.500 |
| 17 | 2.428 | 18.800 |
| 18 | 2.498 | 18.980 |

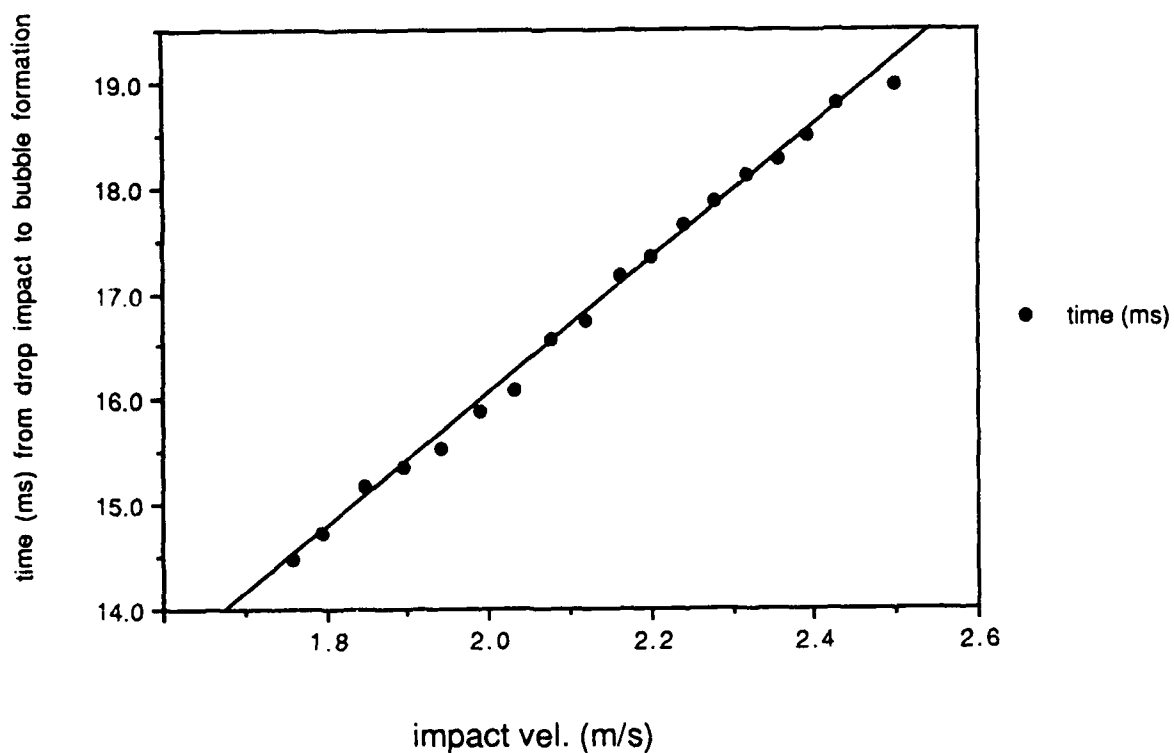
drop diameter = 2.27mm

$$y = 9.2074 * x^{0.80057} \quad R^2 = 0.996$$



Data from "drop diameter = 2.27mm"

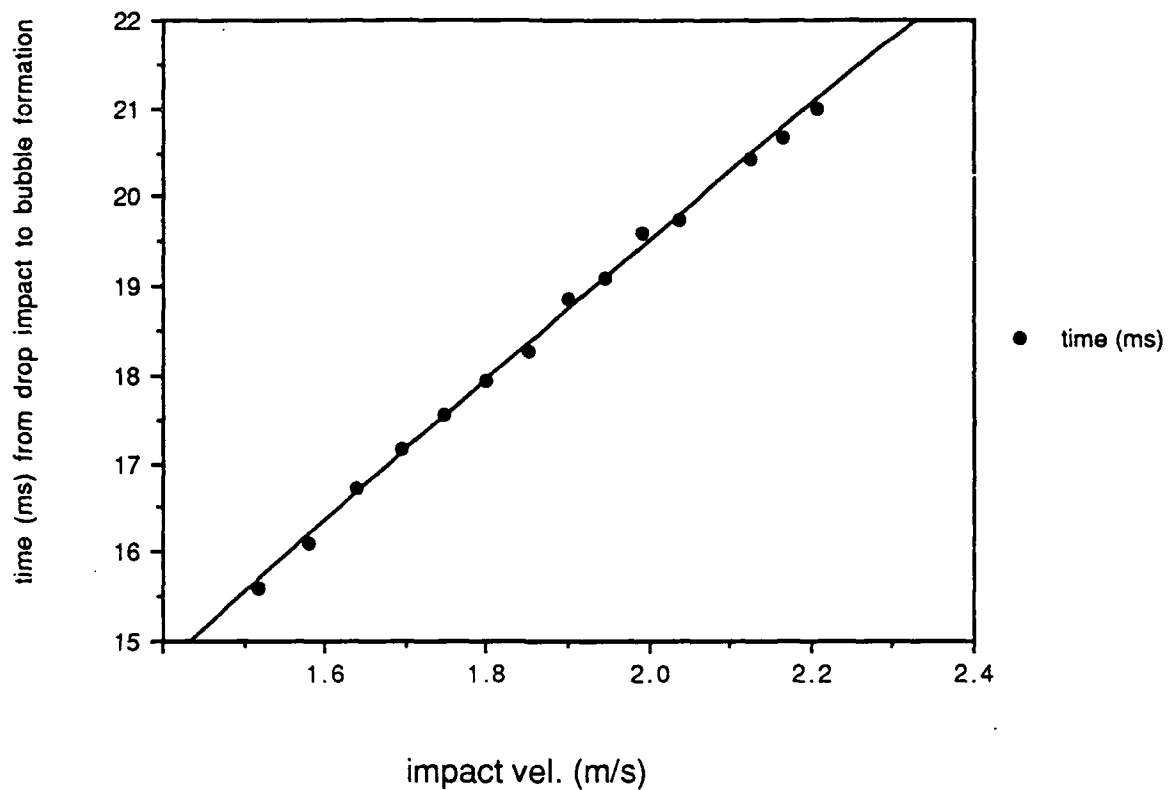
$$y = 3.3340 + 6.3466x \quad R^2 = 0.996$$



| | impact vel. | time (ms) |
|----|-------------|-----------|
| 1 | 1.519 | 15.580 |
| 2 | 1.579 | 16.110 |
| 3 | 1.637 | 16.710 |
| 4 | 1.693 | 17.160 |
| 5 | 1.747 | 17.560 |
| 6 | 1.800 | 17.930 |
| 7 | 1.850 | 18.270 |
| 8 | 1.899 | 18.864 |
| 9 | 1.947 | 19.088 |
| 10 | 1.993 | 19.584 |
| 11 | 2.038 | 19.748 |
| 12 | 2.125 | 20.424 |
| 13 | 2.164 | 20.680 |
| 14 | 2.208 | 20.984 |

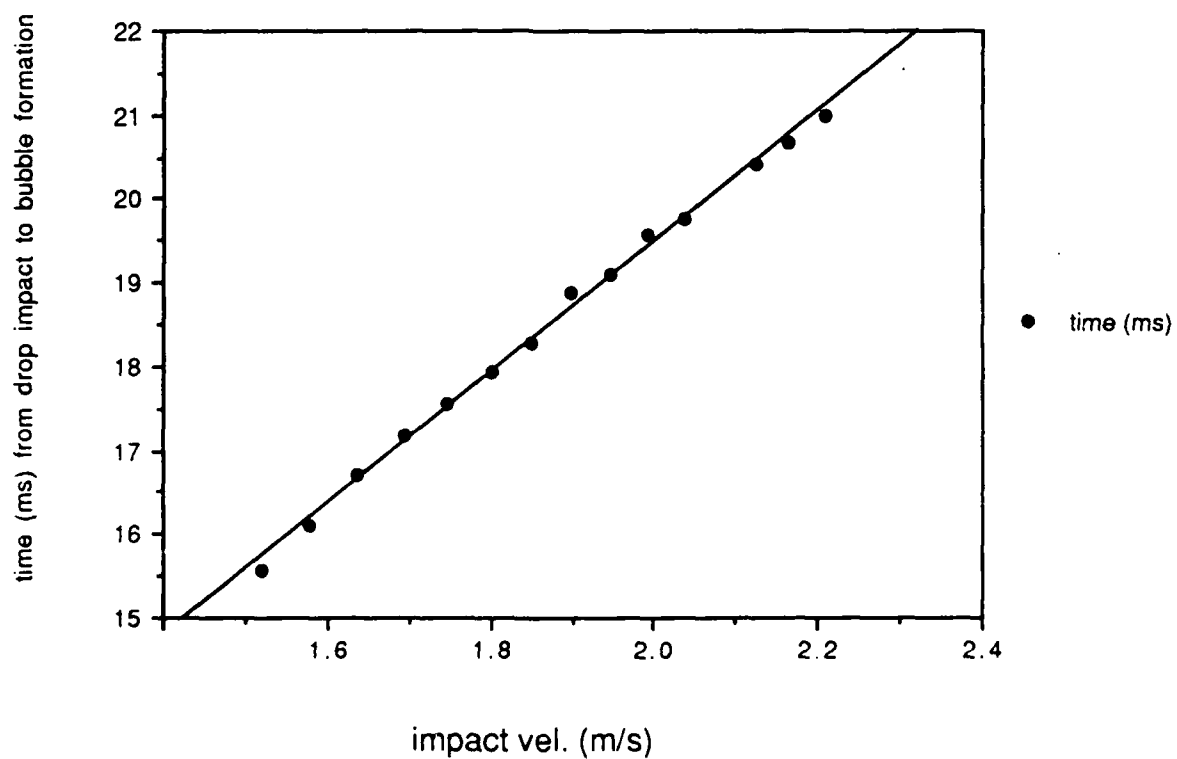
drop diameter = 2.57mm

$$y = 11.272 * x^{0.79038} \quad R^2 = 0.998$$



drop diameter = 2.57mm

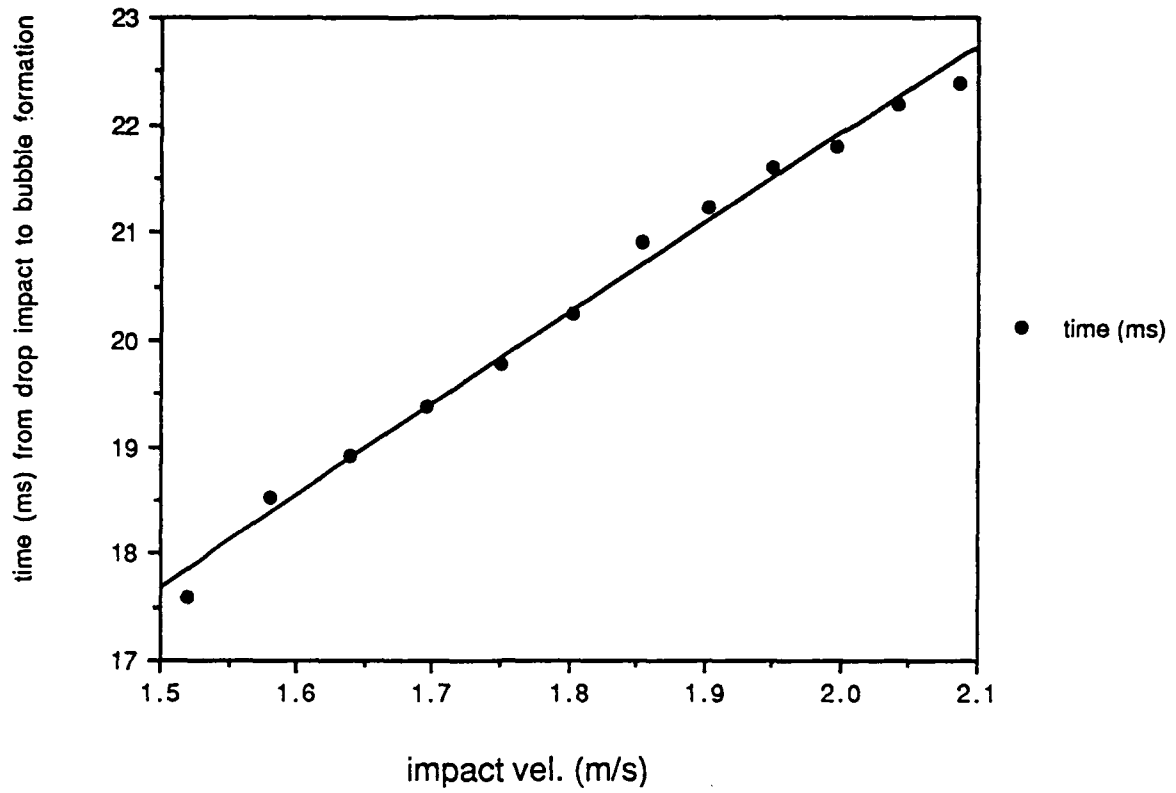
$$y = 3.9015 + 7.7893x \quad R^2 = 0.997$$



| | impact vel. | time (ms) |
|----|-------------|-----------|
| 1 | 1.520 | 17.589 |
| 2 | 1.581 | 18.532 |
| 3 | 1.639 | 18.930 |
| 4 | 1.695 | 19.392 |
| 5 | 1.750 | 19.772 |
| 6 | 1.802 | 20.240 |
| 7 | 1.853 | 20.904 |
| 8 | 1.902 | 21.238 |
| 9 | 1.950 | 21.608 |
| 10 | 1.997 | 21.786 |
| 11 | 2.042 | 22.188 |
| 12 | 2.086 | 22.388 |

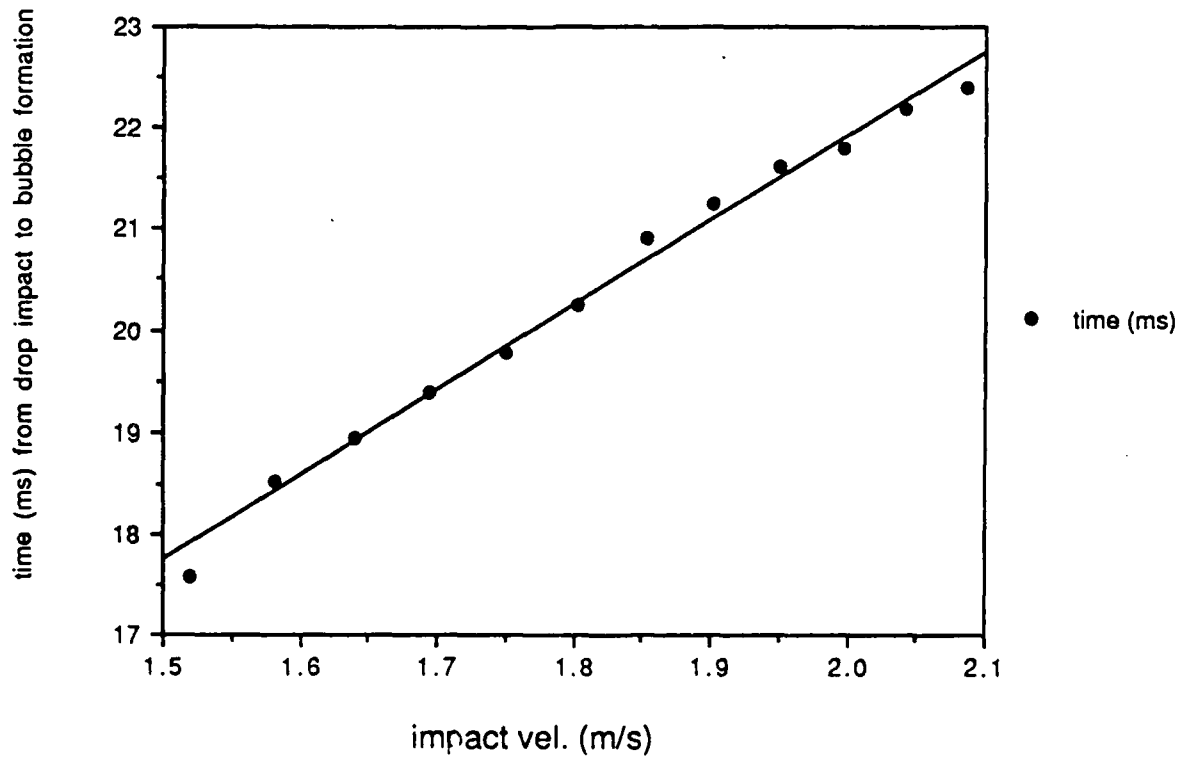
drop diameter = 2.86mm

$$y = 13.056 * x^{0.74647} \quad R^2 = 0.991$$



drop diameter = 2.86mm

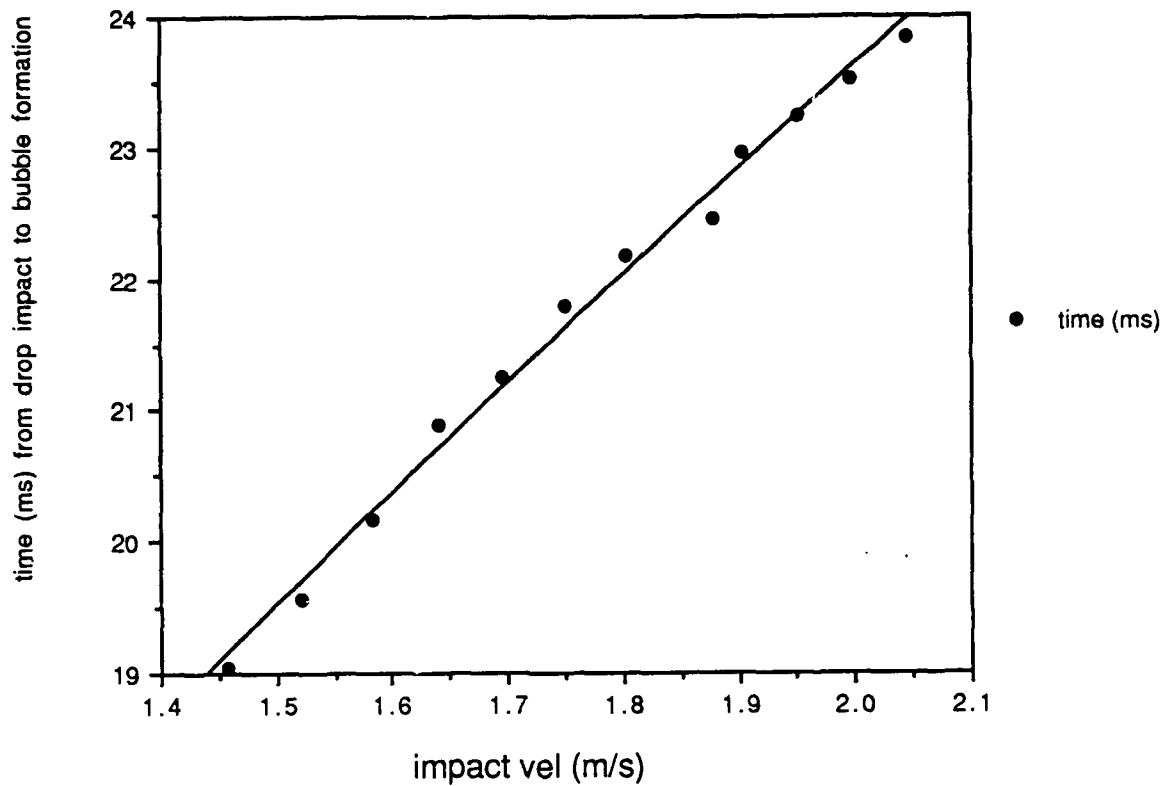
$$y = 5.2206 + 8.3385x \quad R^2 = 0.990$$



| | impact vel | time (ms) |
|----|------------|-----------|
| 1 | 1.457 | 19.040 |
| 2 | 1.521 | 19.568 |
| 3 | 1.582 | 20.160 |
| 4 | 1.640 | 20.880 |
| 5 | 1.696 | 21.256 |
| 6 | 1.751 | 21.784 |
| 7 | 1.803 | 22.180 |
| 8 | 1.879 | 22.456 |
| 9 | 1.904 | 22.960 |
| 10 | 1.952 | 23.232 |
| 11 | 1.998 | 23.524 |
| 12 | 2.044 | 23.832 |

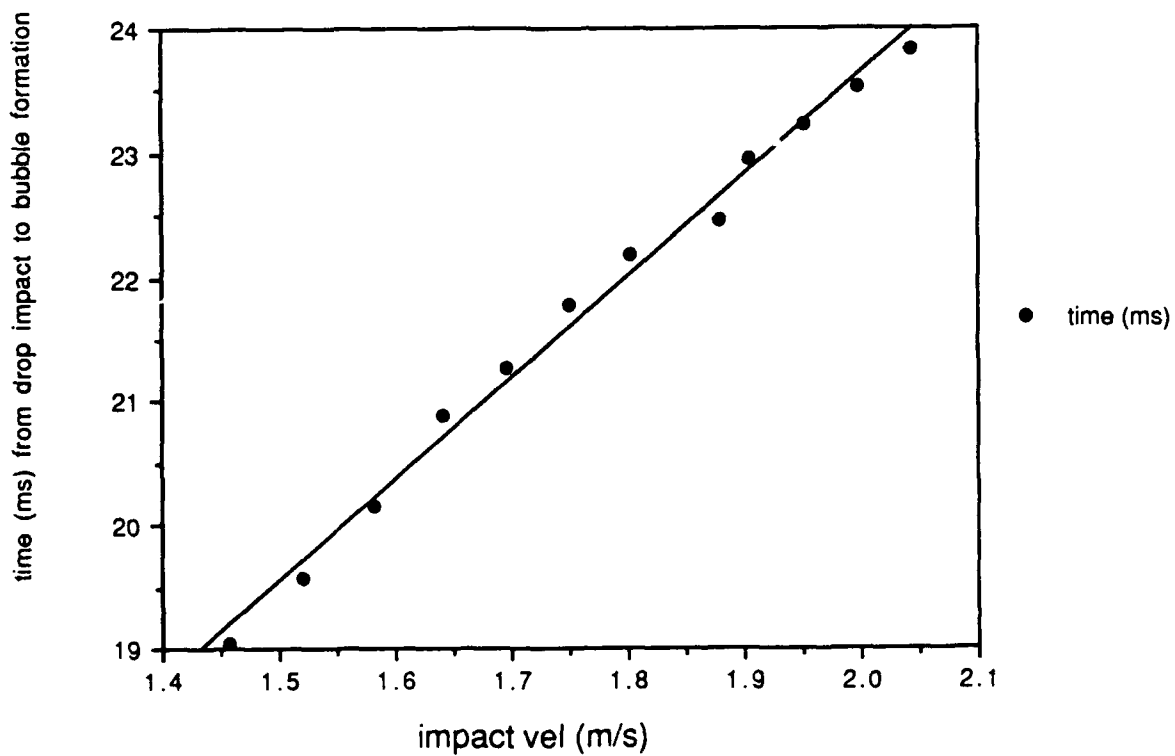
drop diameter = 3.03mm

$$y = 14.903 * x^{0.66408} \quad R^2 = 0.993$$



drop diameter = 3.03mm

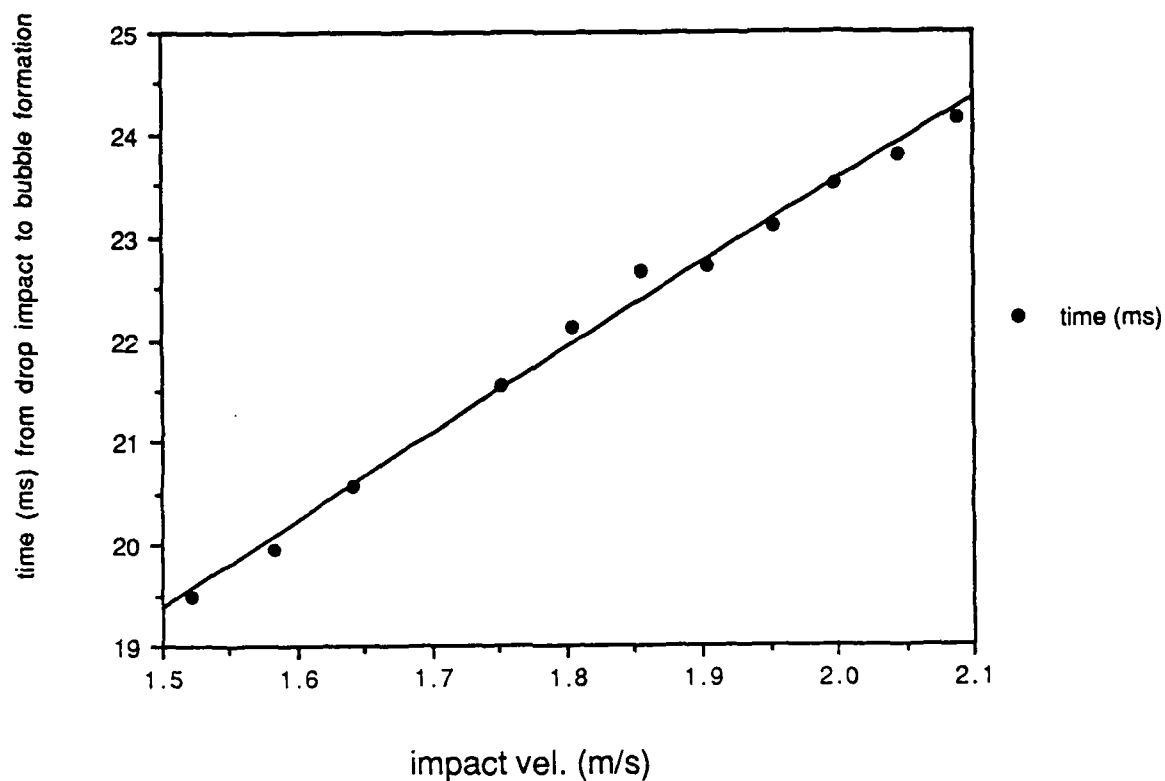
$$y = 7.3108 + 8.1567x \quad R^2 = 0.991$$



| | impact vel. | time (ms) |
|---|-------------|-----------|
| 1 | 1.321 | 20.032 |
| 2 | 1.391 | 20.844 |
| 3 | 1.458 | 21.384 |
| 4 | 1.522 | 22.036 |
| 5 | 1.583 | 22.916 |
| 6 | 1.641 | 23.476 |
| 7 | 1.698 | 23.968 |

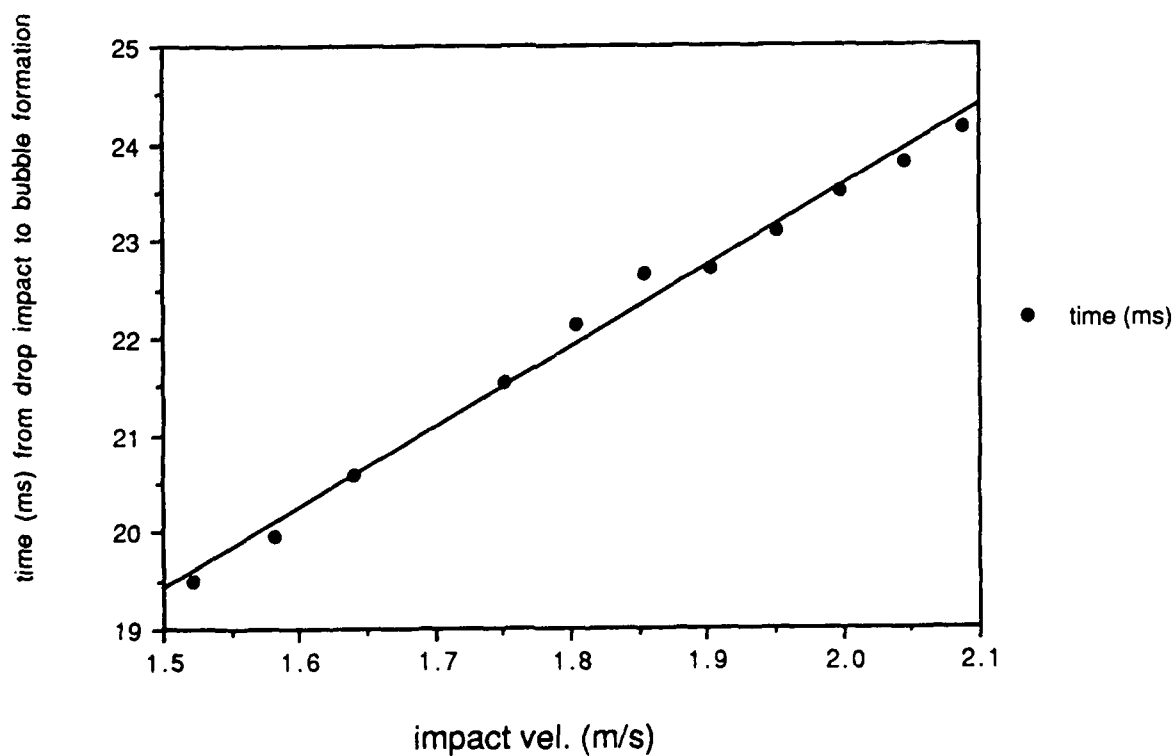
drop diameter = 3.13mm

$$y = 14.697 * x^{0.67948} \quad R^2 = 0.993$$



drop diameter = 3.13mm

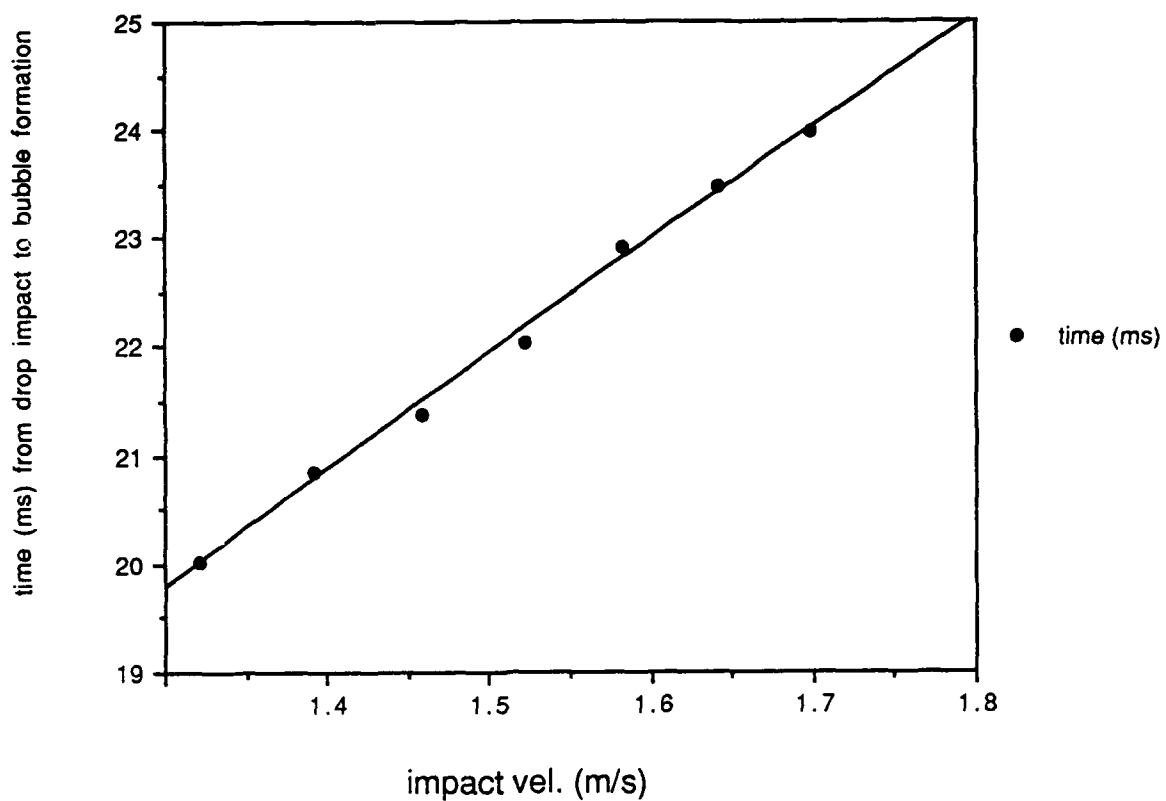
$$y = 7.0770 + 8.2283x \quad R^2 = 0.991$$



| | impact vel. | time (ms) |
|----|-------------|-----------|
| 1 | 1.246 | 19.340 |
| 2 | 1.321 | 20.480 |
| 3 | 1.391 | 21.126 |
| 4 | 1.458 | 21.936 |
| 5 | 1.522 | 22.446 |
| 6 | 1.583 | 23.276 |
| 7 | 1.642 | 23.508 |
| 8 | 1.698 | 24.072 |
| 9 | 1.753 | 24.580 |
| 10 | 1.805 | 24.992 |

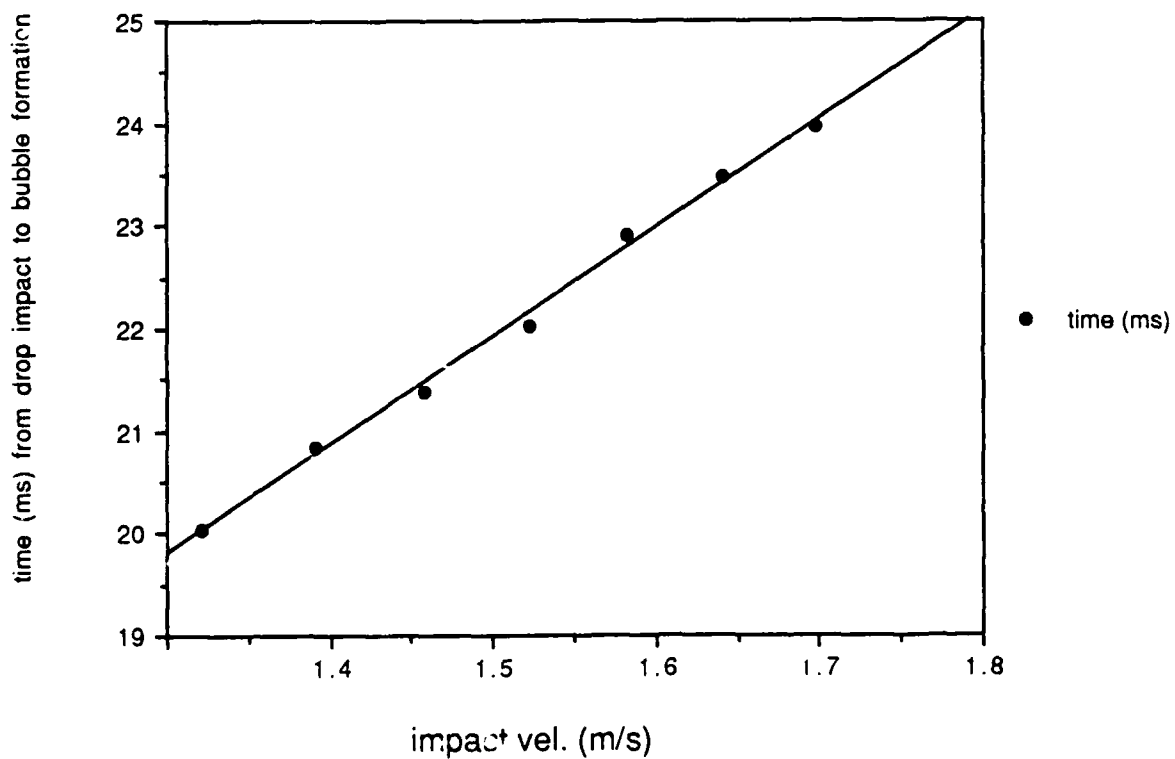
drop diameter = 3.34mm

$$y = 16.357 \cdot x^{0.72379} \quad R^2 = 0.996$$



drop diameter = 3.34mm

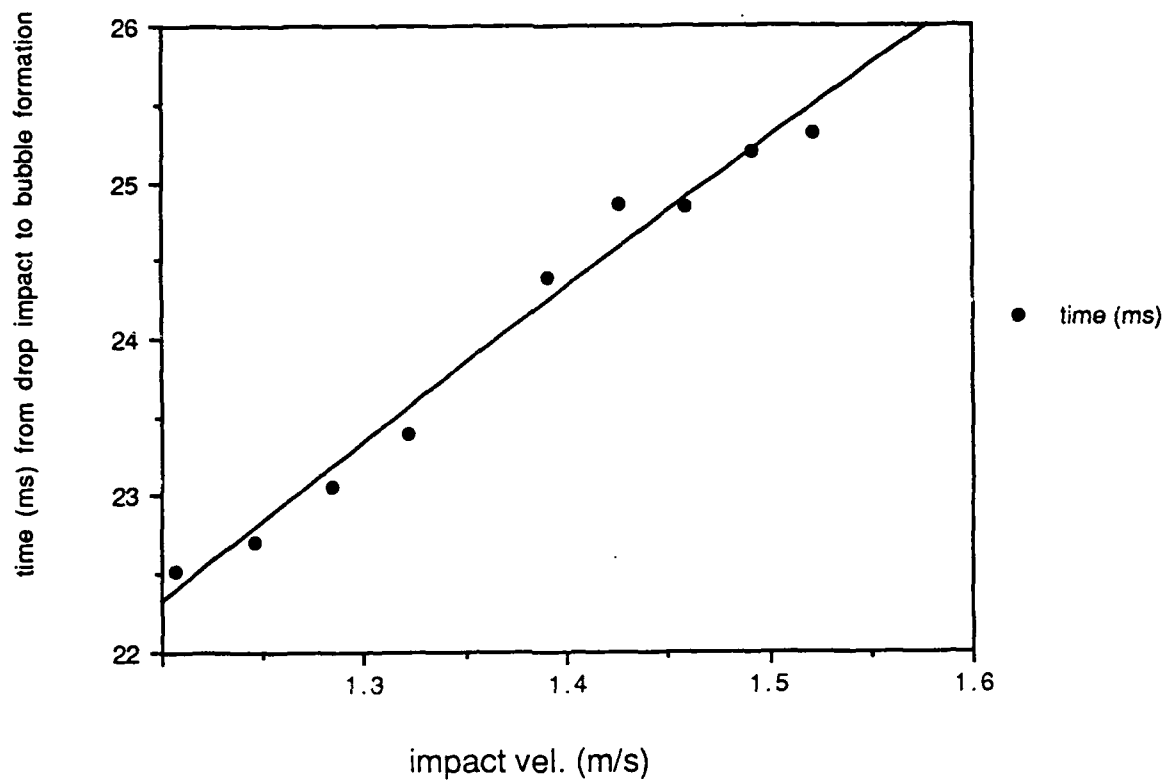
$$y = 6.0346 + 10.591x \quad R^2 = 0.996$$



| | impact vel. | time (ms) |
|---|-------------|-----------|
| 1 | 1.241 | 22.708 |
| 2 | 1.321 | 23.396 |
| 3 | 1.391 | 24.328 |
| 4 | 1.459 | 24.839 |
| 5 | 1.522 | 25.308 |
| 6 | 1.491 | 25.196 |
| 7 | 1.426 | 24.864 |
| 8 | 1.284 | 23.056 |
| 9 | 1.207 | 22.516 |

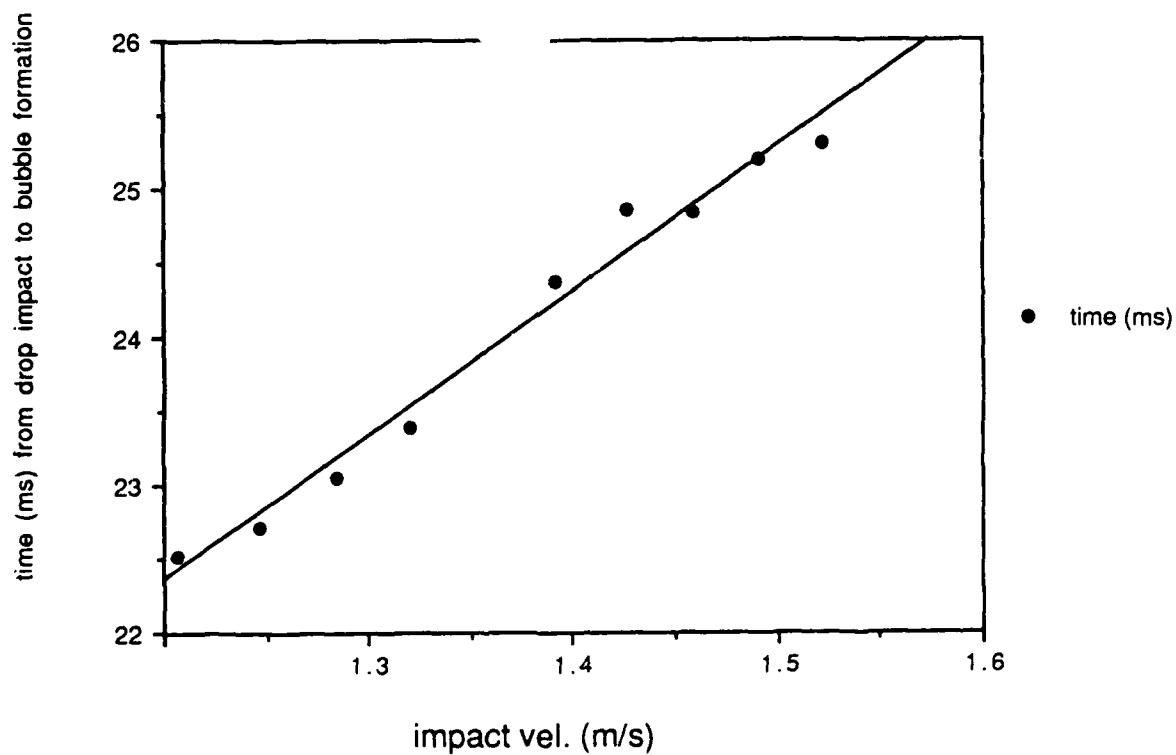
drop diameter = 3.73mm

$$y = 20.165 * x^{0.55673} \quad R^2 = 0.980$$



drop diameter = 3.73mm

$$y = 10.617 + 9.7767x \quad R^2 = 0.979$$

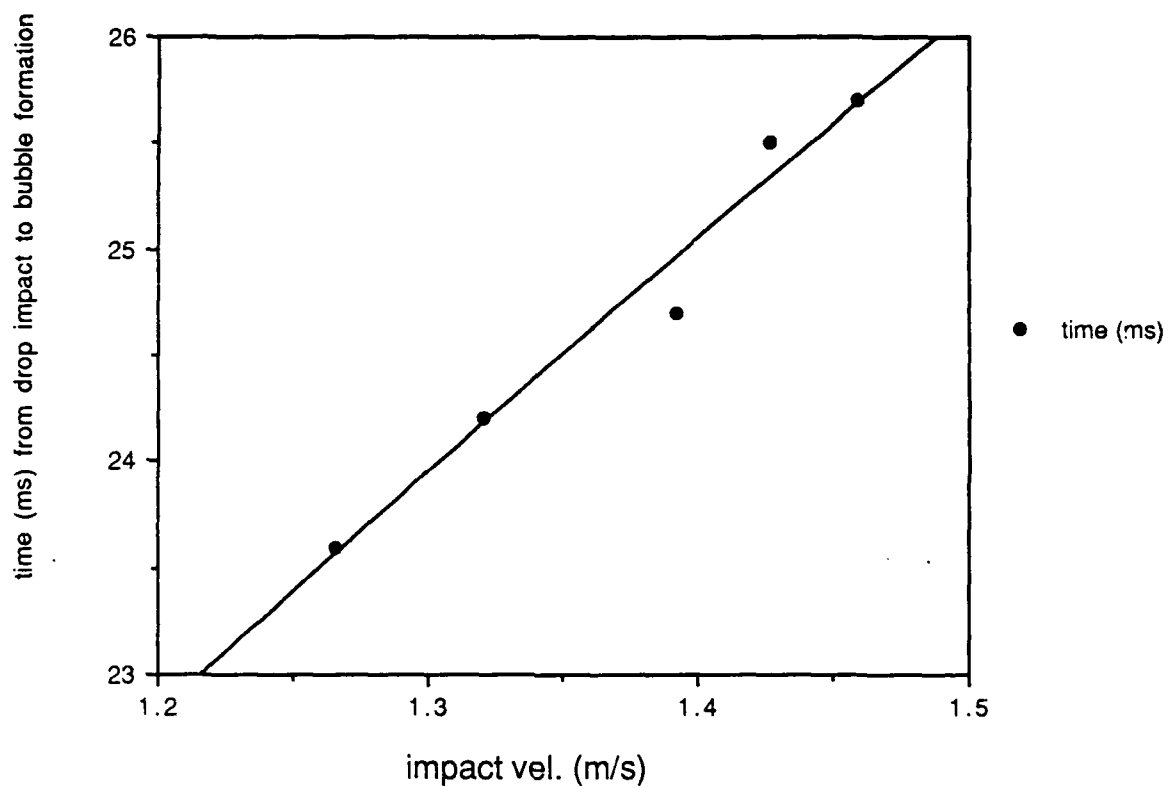


| | vel. (m/s) | time (ms) |
|---|------------|-----------|
| 1 | 1.266 | 23.600 |
| 2 | 1.321 | 24.200 |
| 3 | 1.392 | 24.700 |
| 4 | 1.426 | 25.500 |
| 5 | 1.459 | 25.700 |

drop diameter = 3.99mm

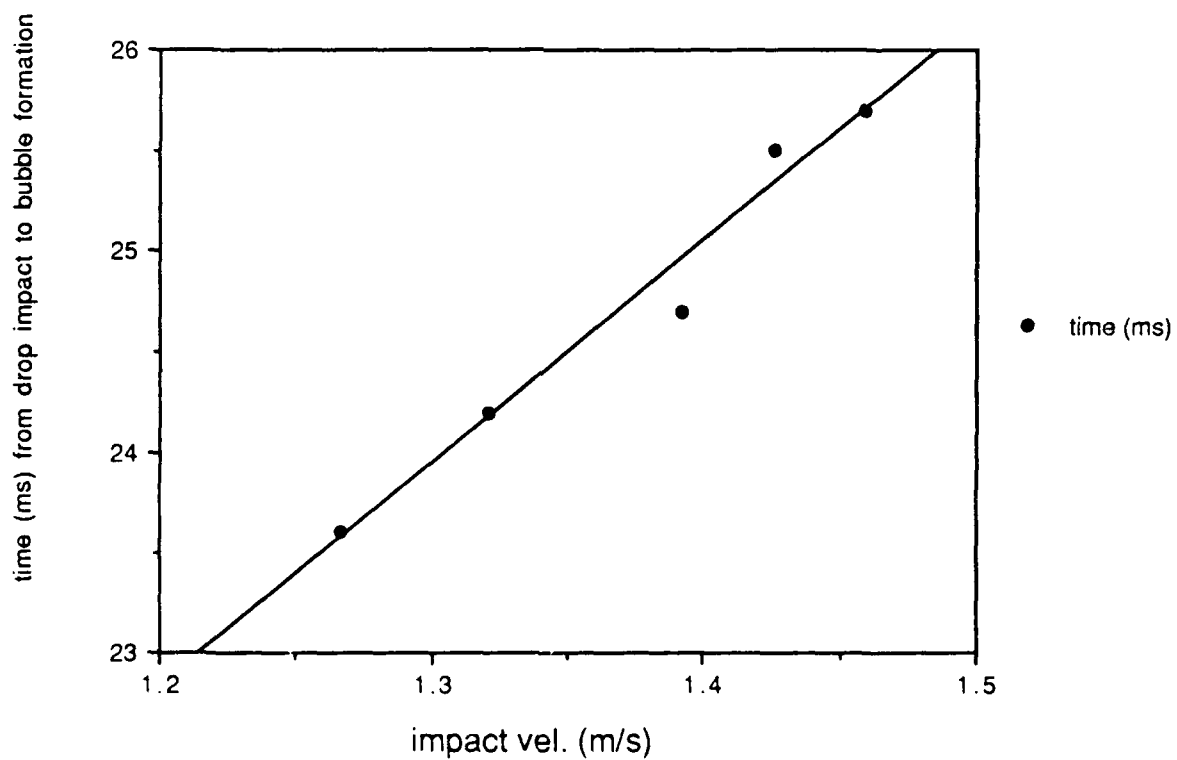
91

$$y = 20.421 * x^{0.60644} \quad R^2 = 0.969$$



drop diameter = 3.99mm

$$y = 9.6262 + 11.009x \quad R^2 = 0.969$$



ANALYSIS OF DATA SET 2

Figure 13 is a comprehensive graph of data set 2. It shows that the time between drop impact and bubble formation increases monotonically as drop size or impact velocity increases.

OTHER OBSERVATIONS

Figures 2a and 8 both show the range of impact velocities and drop sizes for regular entrainment. However, there are other activities occurring in and around the region.

Just above the upper velocity bound for drops larger than 3.73 mm in diameter, there is a region of irregular entrainment. As the impact velocity steadily increases from the lowest entraining velocity, entrainment eventually ceases and a lull of bubble formation is observed. However, if the velocity is increased a little more, entrainment resumes. At first glance, the entrainment area appears to have a forked end. But what happens in these two areas is different. Below the lull, the water cavity is in the shape of a cone, and one bubble pinched off the bottom every time. Above the lull, the cavity is spherically shaped with bubbles being formed in an unpredictable manner. Many times there are several bubbles formed by one drop.

Another event occurs just below the lower velocity boundary for drops about 4.5 mm in diameter. Here, surface bubbles measuring about 7 mm diameter and oscillating at 1.3 to 1.4 kHz, are formed when the drop hits the water. However, the event is not a regular occurrence and seems to be dependent on contaminants in the water.

Finally, when a bubble is entrained from a drop falling at a velocity near the upper or lower velocity boundary, the bubble will occasionally exhibit second harmonics, as shown, for example, in Fig. 14. The exact nature of these higher harmonics is not yet clear, but the most likely reason is that the bubble's radius is behaving like a Duffing oscillator. However, shape oscillations may be occurring some of the time since frequency peaks not corresponding to harmonics have been observed in some of the bubble's FFT's. Their occurrence, however, is not common.

CONCLUSIONS

In summary, the characteristics of bubbles inside the observed boundaries of regular entrainment have been explored. When the drop diameter is kept constant and the changes in the bubble's radius, frequency, or initial dipole strength are observed as the impact

velocity is continuously increased from the lowest to highest entraining velocities, an extrema is reached with the variance in the data points decreasing the closer they are to it. If the drop is large, ($d > 3.79$ mm), then any entrainment occurs marginally, and the graphs take on isotropic behavior. If the drop entrains a bubble at terminal velocity, only part of these trends will exist.

As the drop diameter is increased from the minimum to the maximum entrainment size, the frequency of the bubbles' oscillations decrease from 12 to 14 kHz to around 6 or 7 kHz. These results show that regular entrainment is the cause of the underwater noise produced by rain.

Also, bubbles have been shown to take longer to form after impact as the drop size or impact velocity is increased.

Finally, additional phenomena have been observed in and around the entrainment region: irregular entrainment, surface bubbles, and non-linear oscillations. Although, the details of regular entrainment has been extensively investigated, these other phenomena may prove to be sources of fruitful investigation for future researchers.

ACKNOWLEDGEMENTS

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FIGURE CAPTIONS

- Figure 1: The sound spectrum of natural rainfall made at various windspeeds between 1.3 to 1.5 meters per second (Scrimger et al. 1987).
- Figure 2a: A plot made in a previous study (Pumphrey, Crum, and Bjørnø 1989) of the impact velocities and drop diameters necessary for regular entrainment to occur. Anytime the drop diameter and impact velocity coordinates are located within the area bounded by the curves, regular entrainment will occur
- Figure 2b: The graph plots the number of different sized water drop measured earlier (Scrimger et al. 1987) in natural rainfall on three different occasions.
- Figure 3: A diagram of the experimental set-up used for this study.
- Figure 4: The arrows mark the reference points in the bubble noise used to measure frequency.
- Figure 5: The reference points in the bubble noise used to measure initial voltage. These points are marked by the tangential intersection of the vertical lines with the damped sine curve.
- Figure 6: The arrows mark the reference points used along the drop's noise to measure the time between drop impact and bubble formation. These points are at the base of the initial impact noise and a reference point in the bubble formation sound.
- Figure 7: A plot of two times the dipole strength versus frequency for 200 entrained bubbles. These bubbles were entrained from drops 2.57 mm in diameter striking the water at 2.29 m/s.
- Figure 8: A plot made during this study of the impact velocities and drop diameters necessary for regular entrainment to occur.
- Figure 9: A plot made during this study of the kinetic energies and drop diameters necessary for regular entrainment to occur.
- Figure 10: An enlargement of figure 5 showing the highest measured velocities for raindrops. The numbers to the sides show the average of thirty measured frequencies in kHz.
- Figure 11: Contours of frequency or bubble radius are shown within the entrainment region up to a drop diameter of 3.07 mm.
- Figure 12: Contours of initial dipole strength are shown within the entrainment region up to a drop diameter of 3.07 mm.
- Figure 13: Some of the graphs from data set 2 are shown plotted together. The drop diameters associated with each curve are listed beside them.

Figure 14: A marginally entrained bubble displaying primary and secondary harmonics. The top sweep is the acoustic pressure of the oscillation, while the bottom sweep is an enlarged view of its FFT. The numbers above the two peaks in the FFT correspond to the frequencies at those points.

figure 1

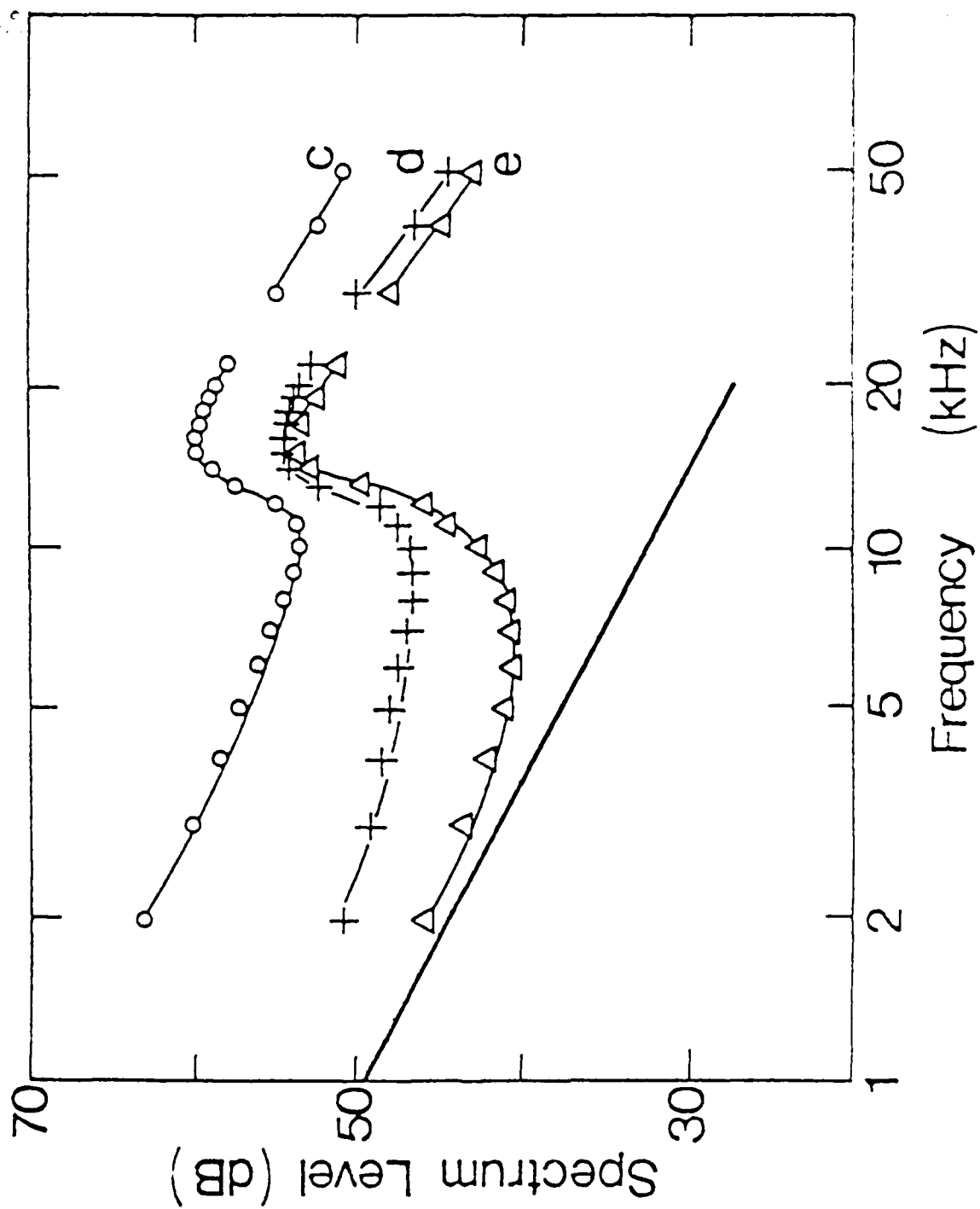


figure 2

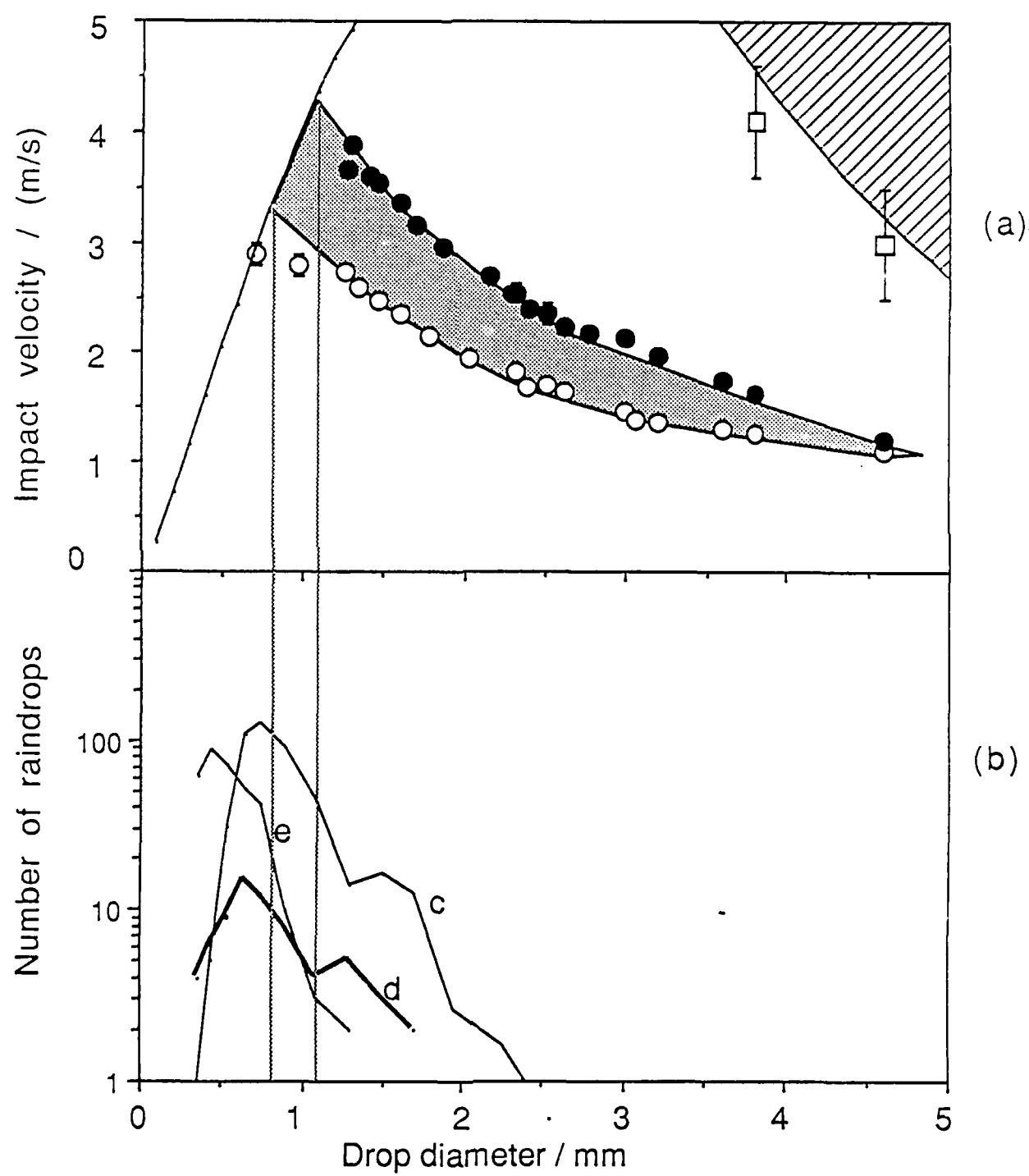


figure 3

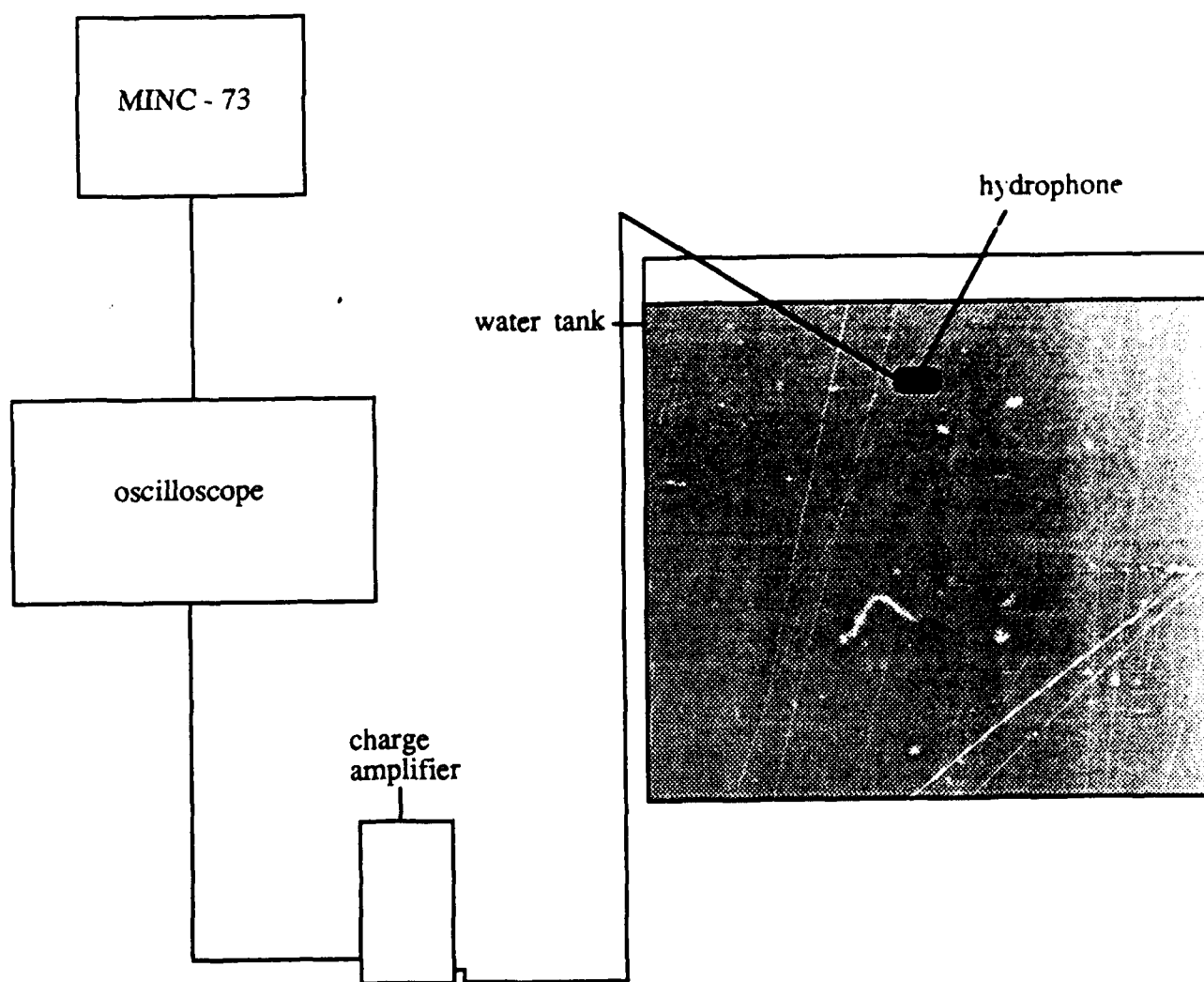
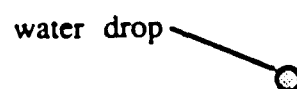
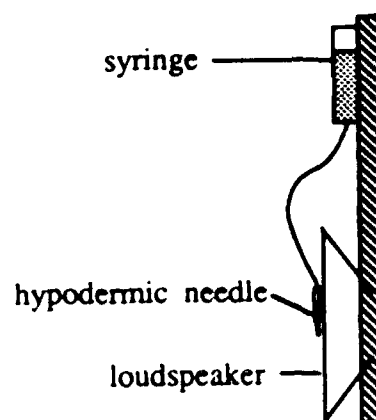
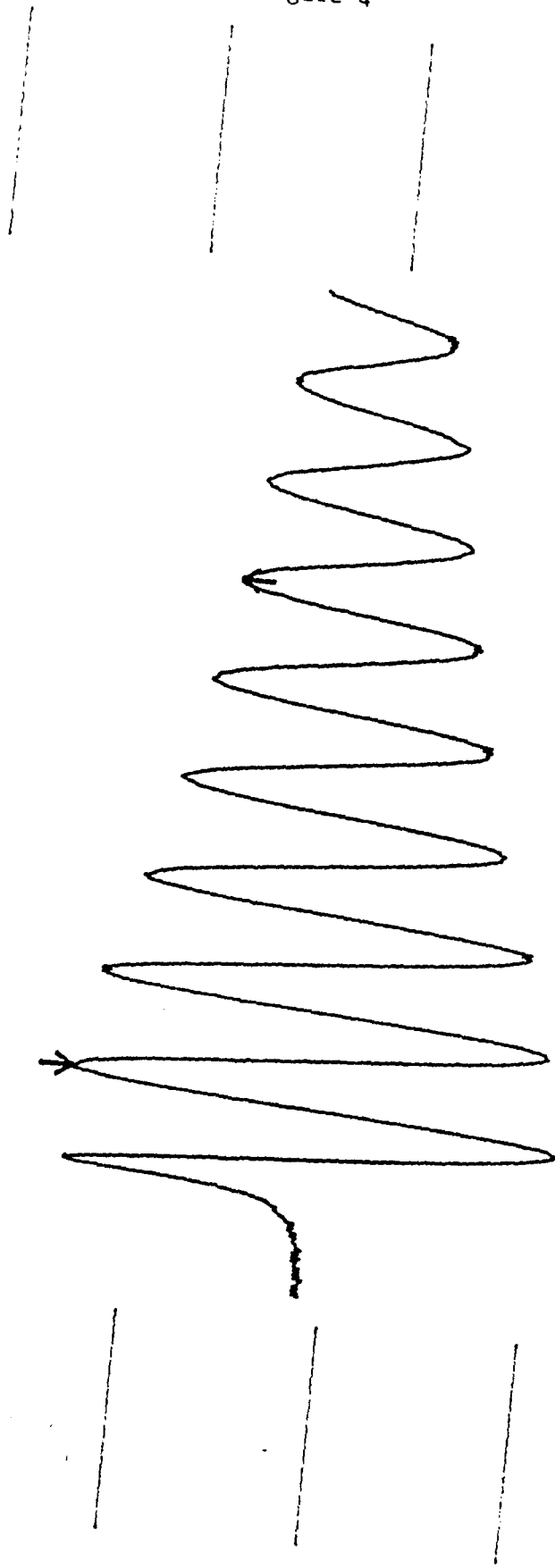


figure 4



Channel 1
-641 mV

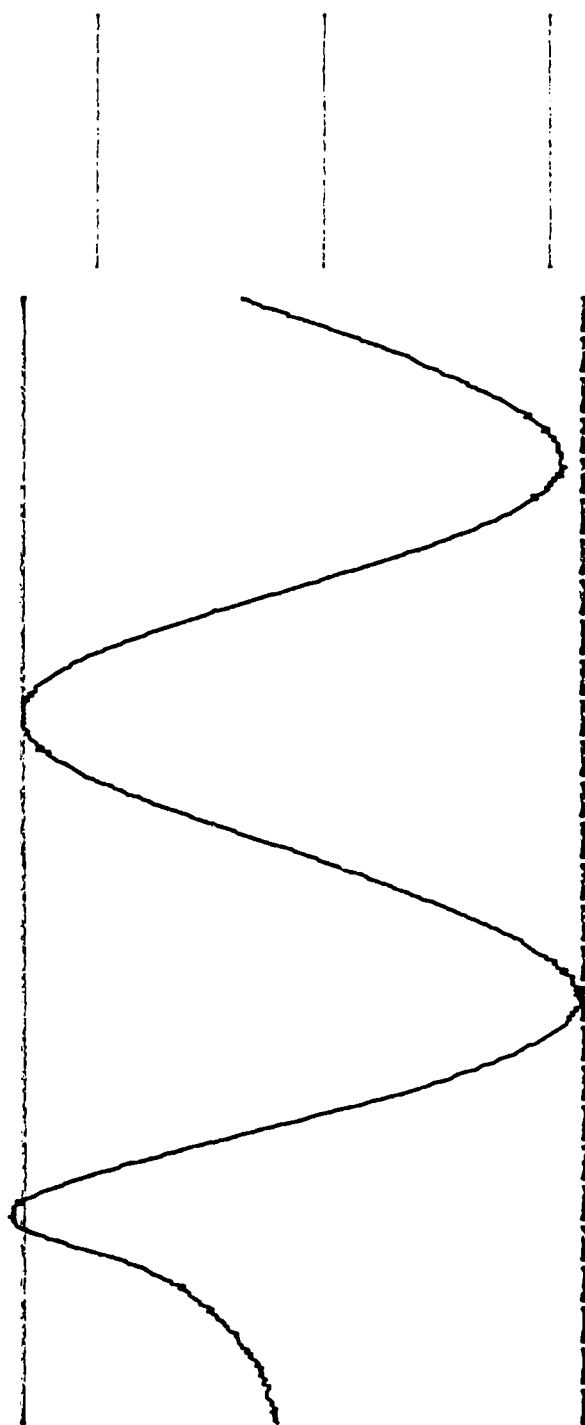
Δt 496 μ s

f 2.016 kHz

Ch 1 .5 V ~
T/div .1 ms
Ch 2 2 V ~
Trigt .58 div \pm CHAN 1 ~

figure 5

X-Chan 1
-2475 mV



Ch 1 .5 V ~
T/div .1 ms Ch 2 2 V ~
Trigt .58 div ± CHAN 1 ~



figure 6

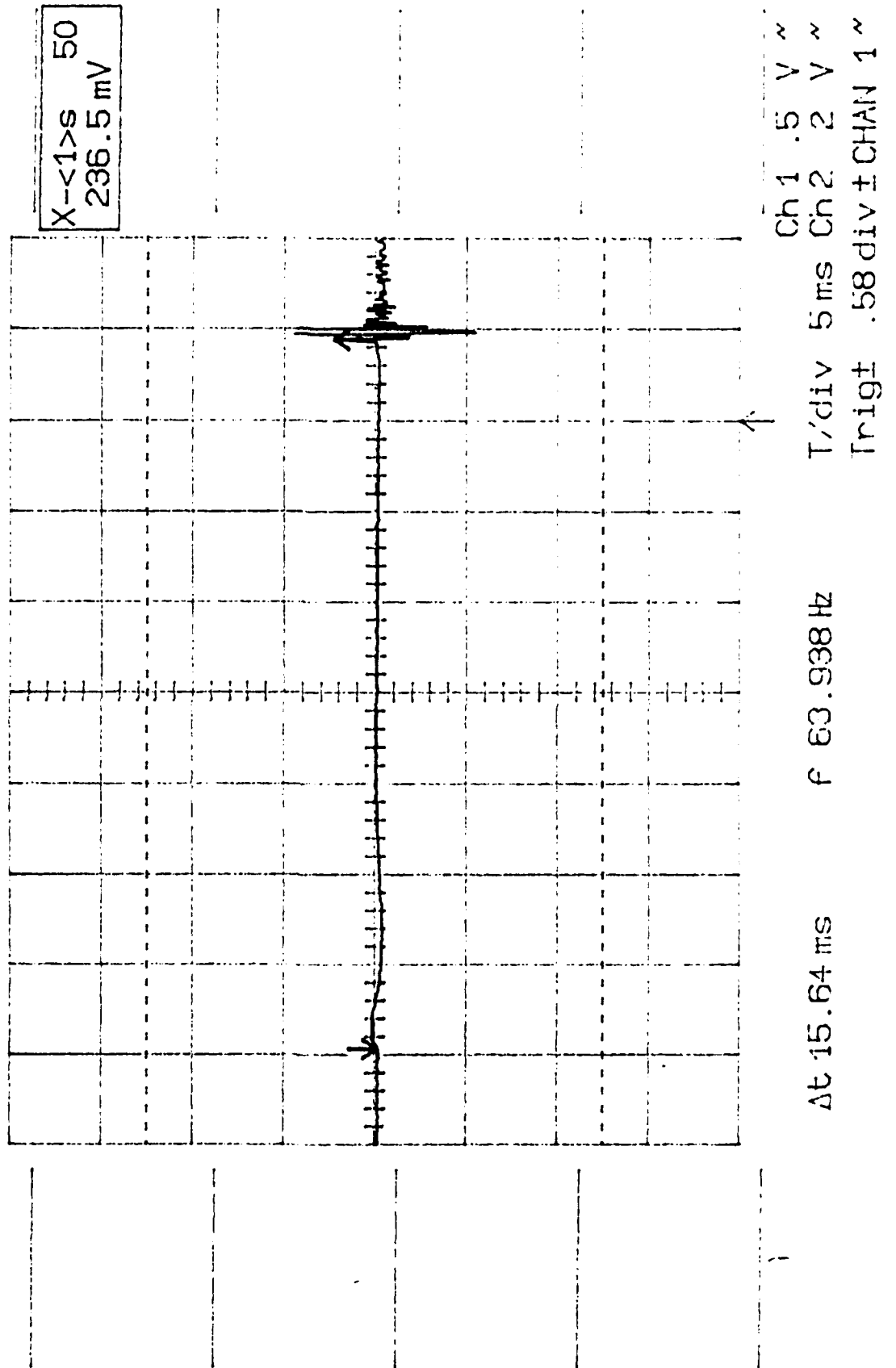


figure 7

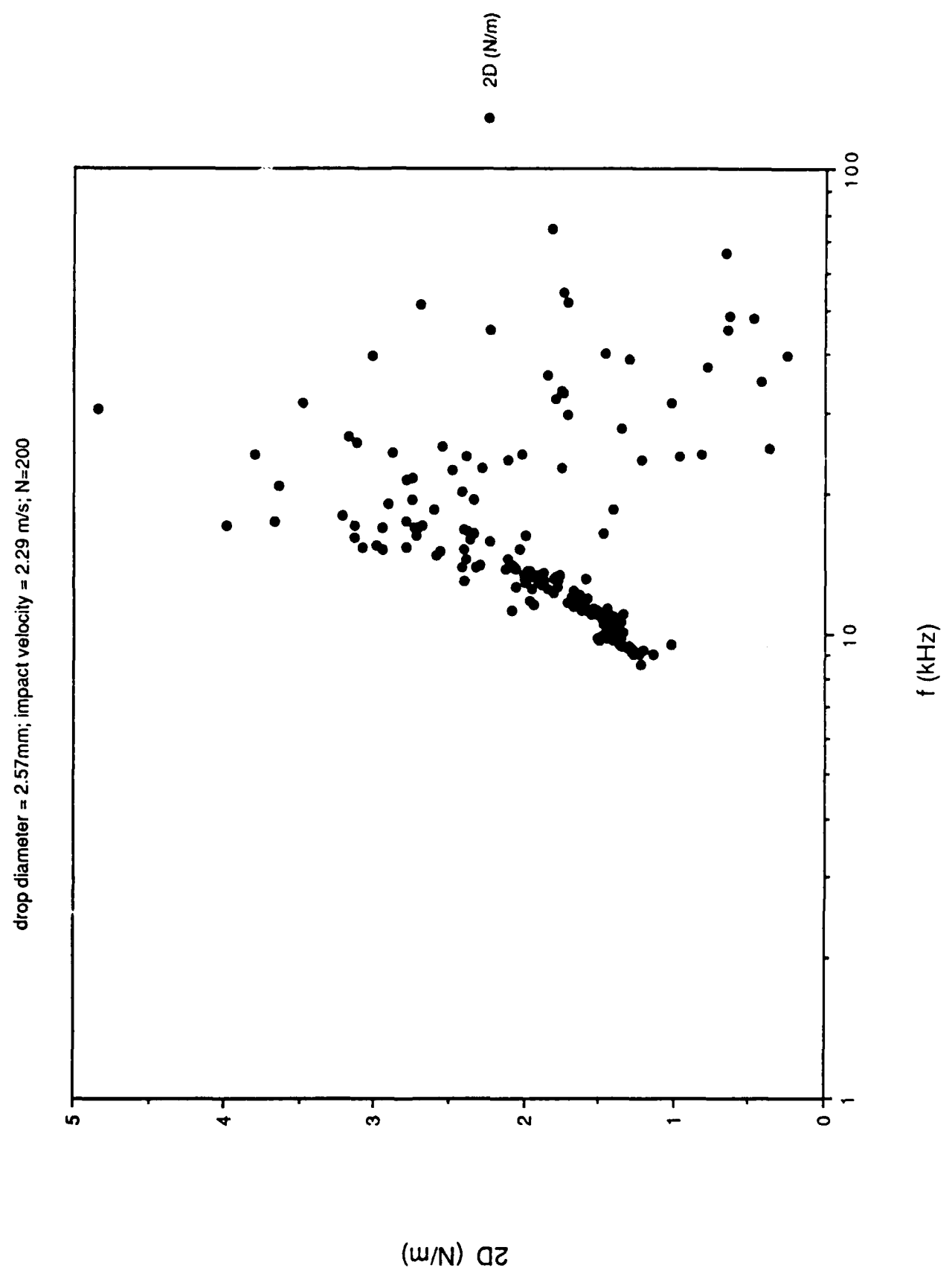


figure 8

impact velocity vs. drop diameter

$$y = 7.3637 - 3.8671x + 0.94015x^2 - 8.5407e-2x^3 \quad R^2 = 0.986$$

$$y = 5.1359 - 2.7258x + 0.66550x^2 - 5.7822e-2x^3 \quad R^2 = 0.990$$

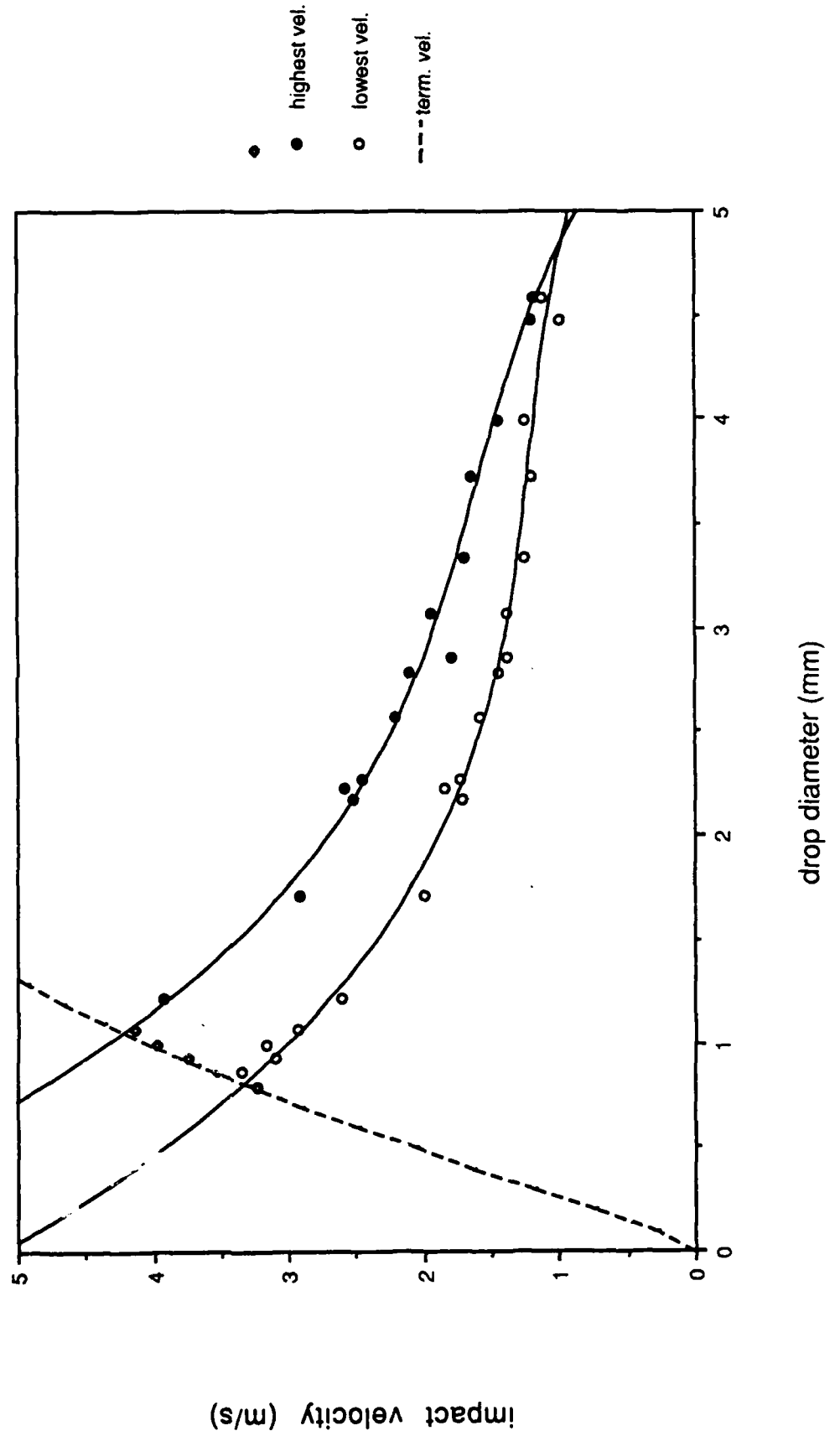


figure 9

kinetic energy vs. drop diameter

$$y = -2.0896 + 2.0419x + 4.7425x^2 - 0.74106x^3 \quad R^2 = 0.979$$

$$y = -1.3266 + 3.7614x + 7.3845e-2x^2 + 0.11928x^3 \quad R^2 = 0.964$$

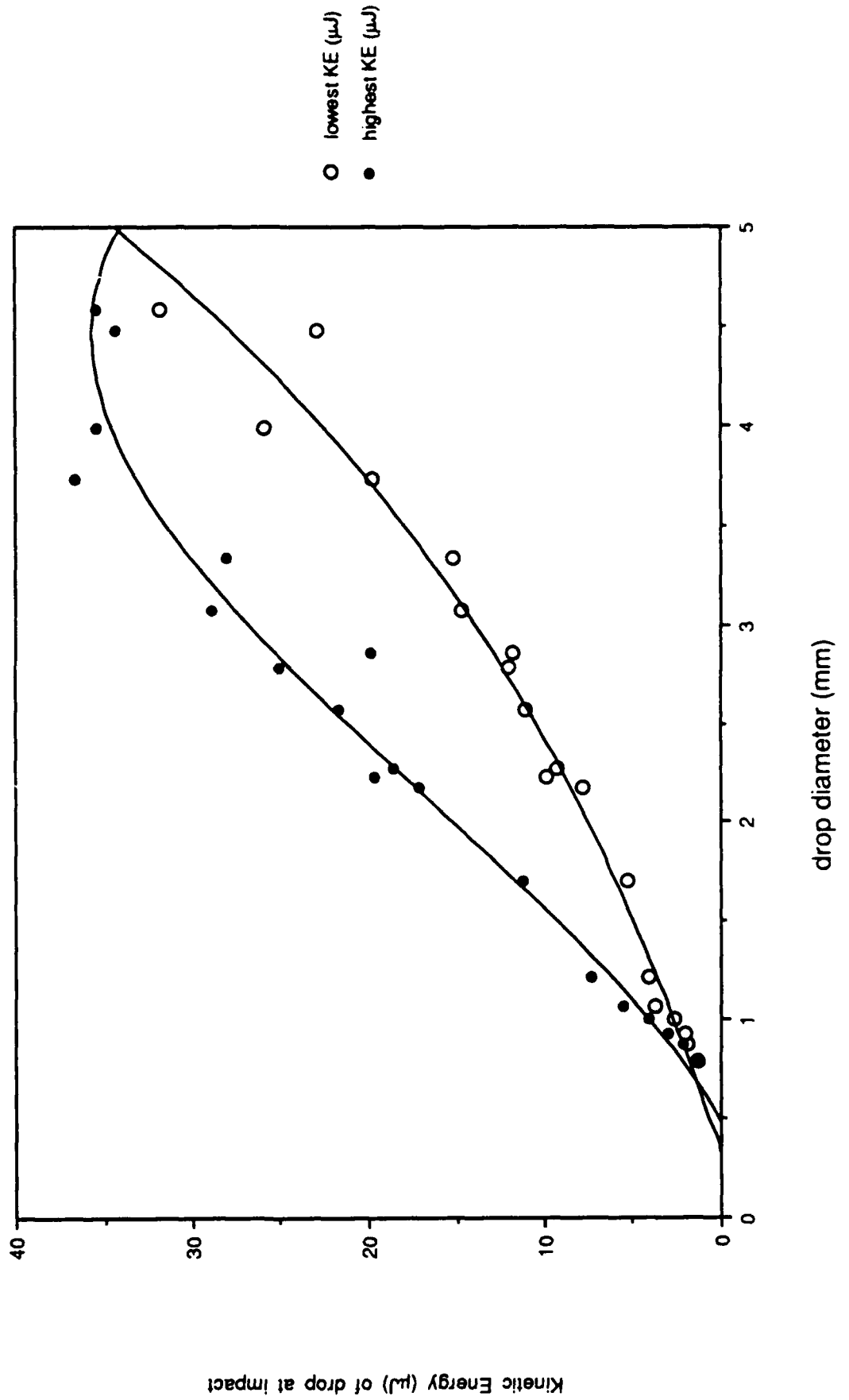


figure 10

impact velocity vs. drop diameter

$$y = 7.3637 - 3.8671x + 0.94015x^2 - 8.5407e-2x^3 \quad R^2 = 0.986$$

$$y = 5.1359 - 2.7258x + 0.66550x^2 - 5.7822e-2x^3 \quad R^2 = 0.990$$

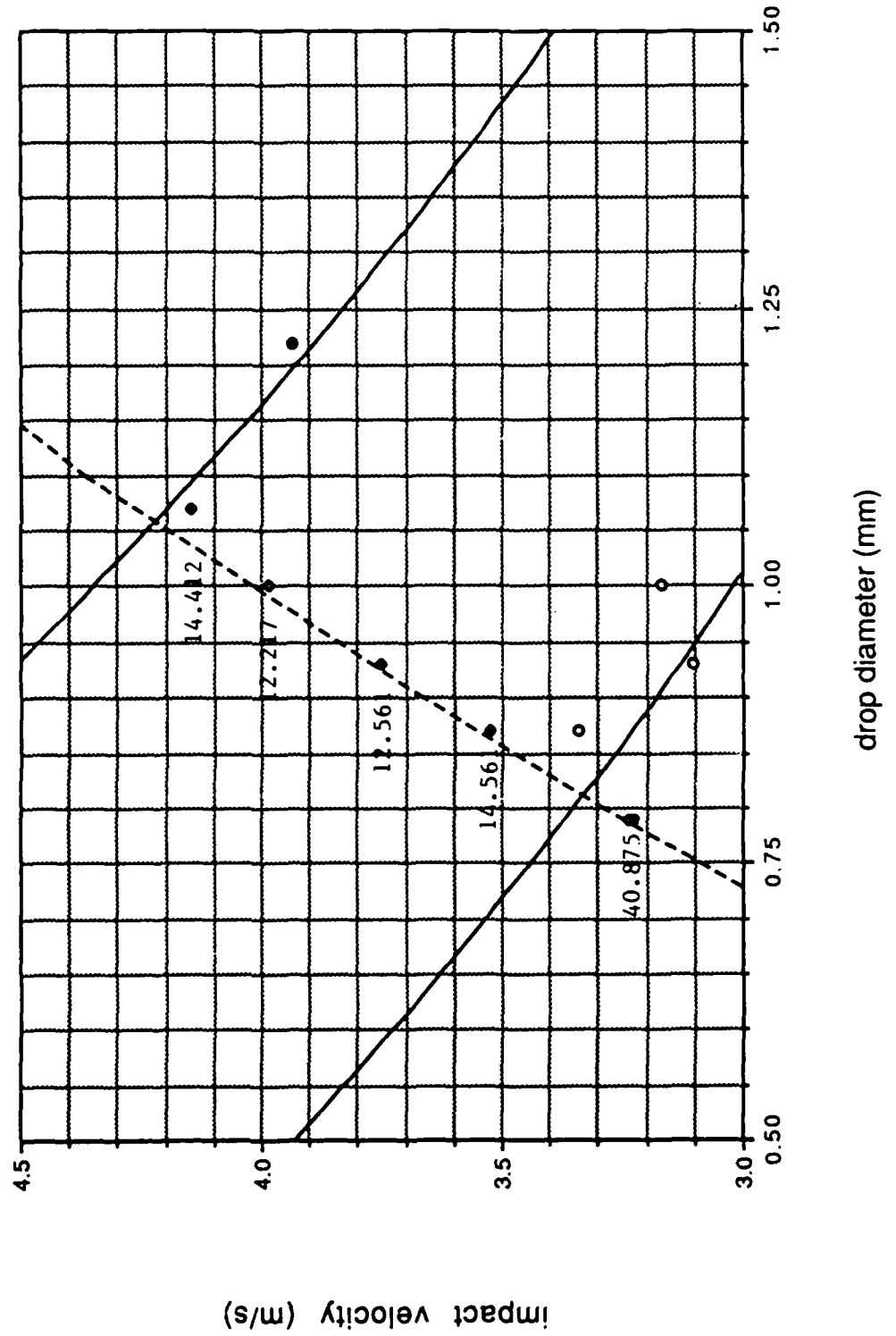


figure 11

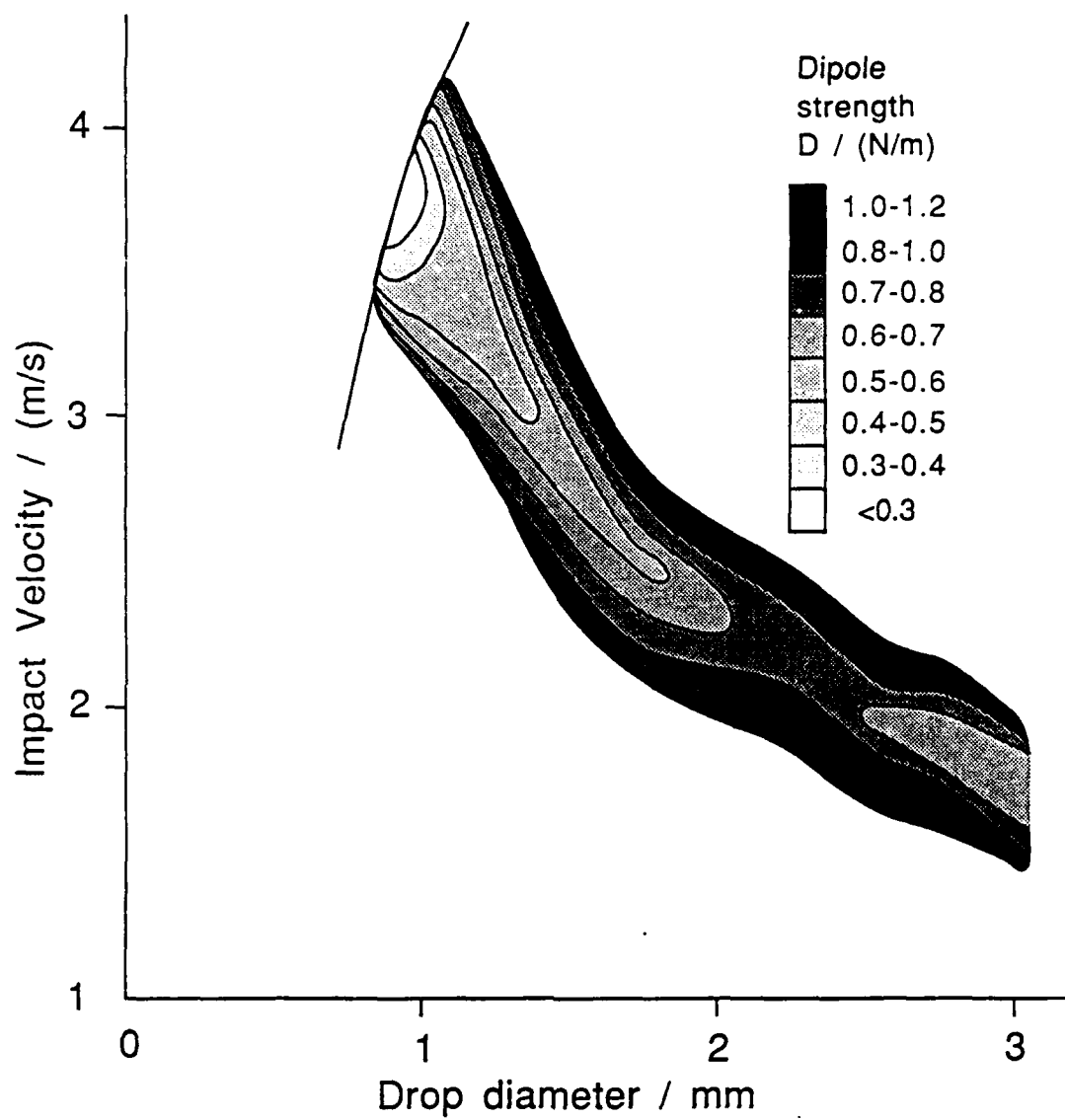


figure 12

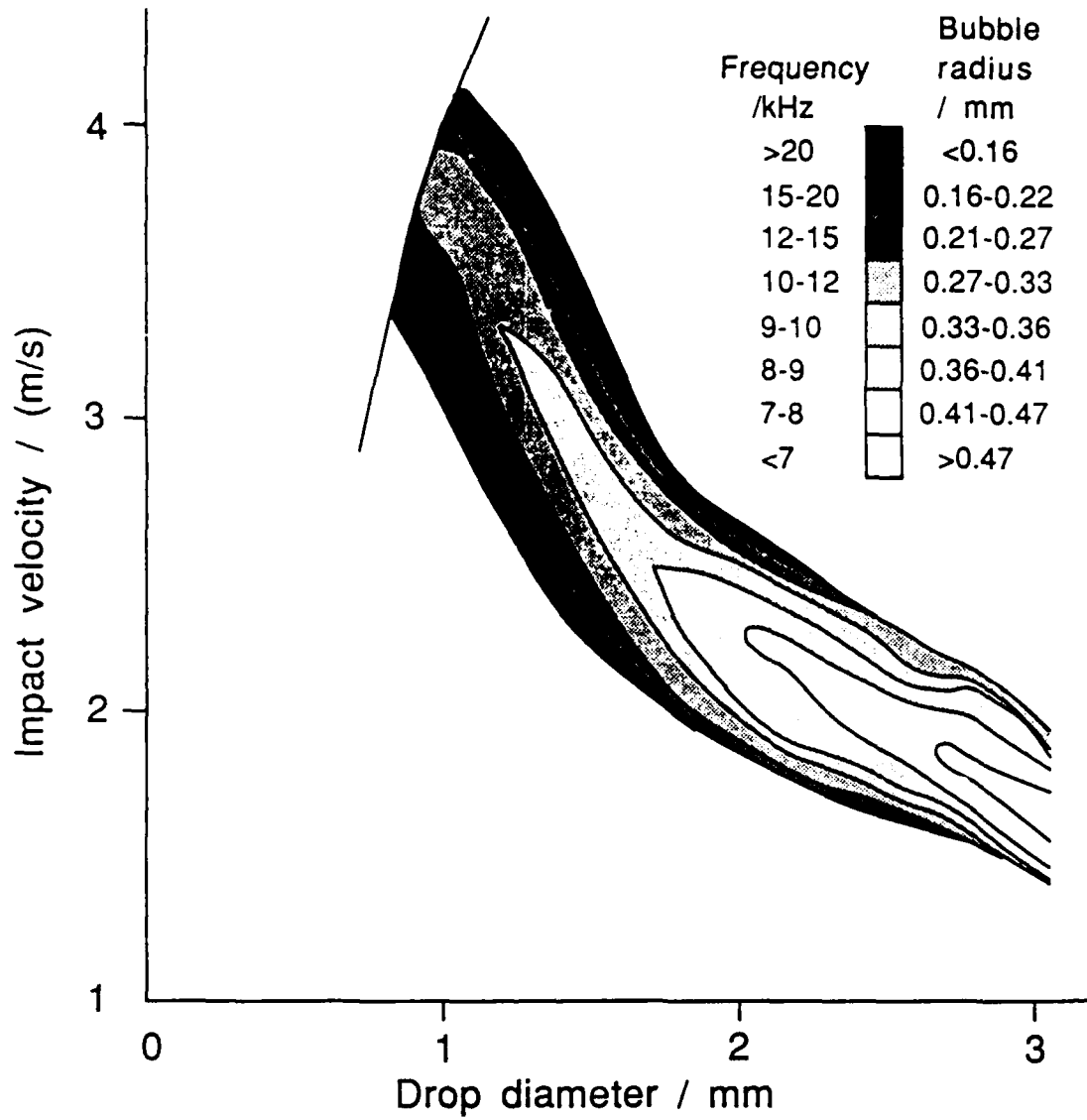


figure 13

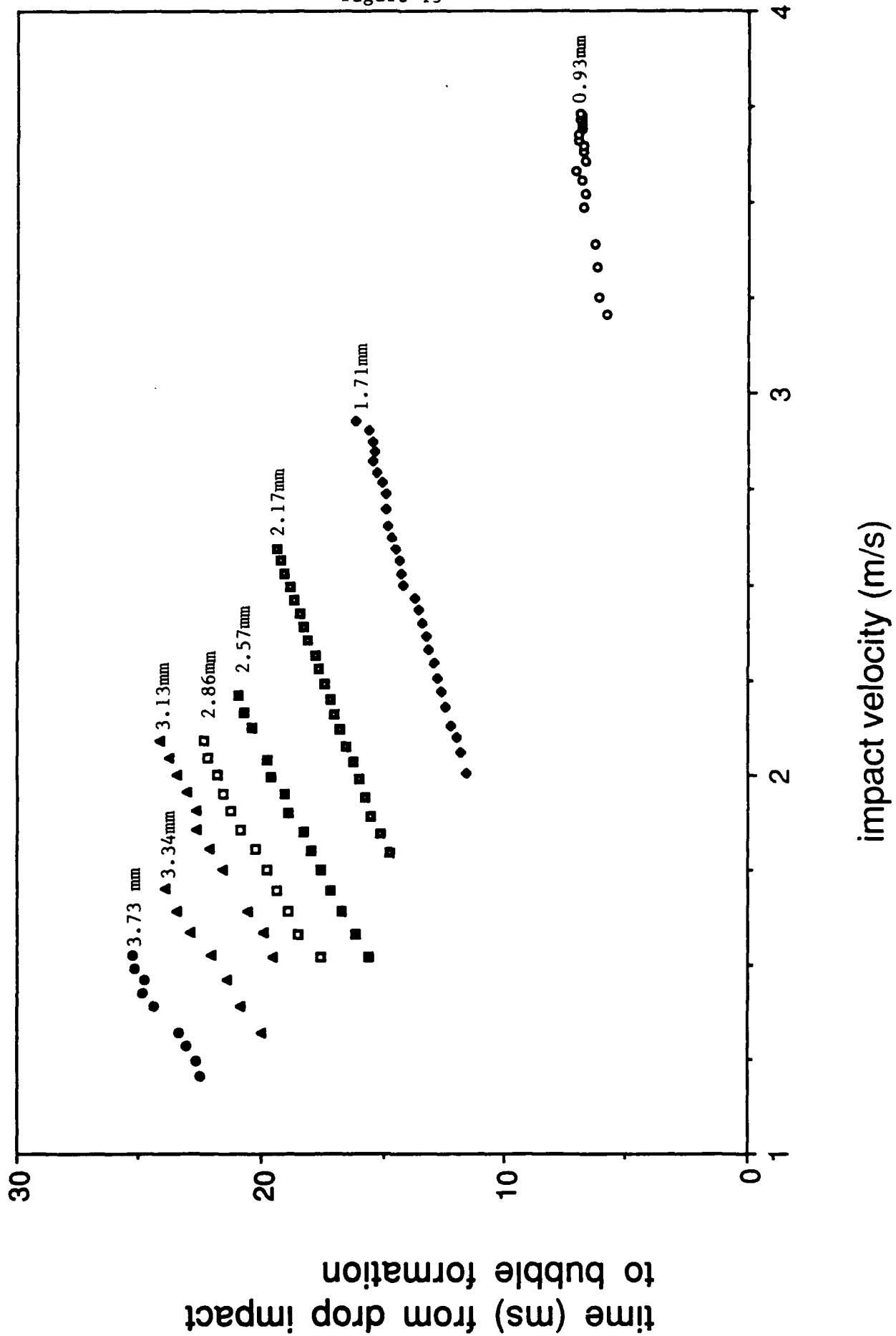
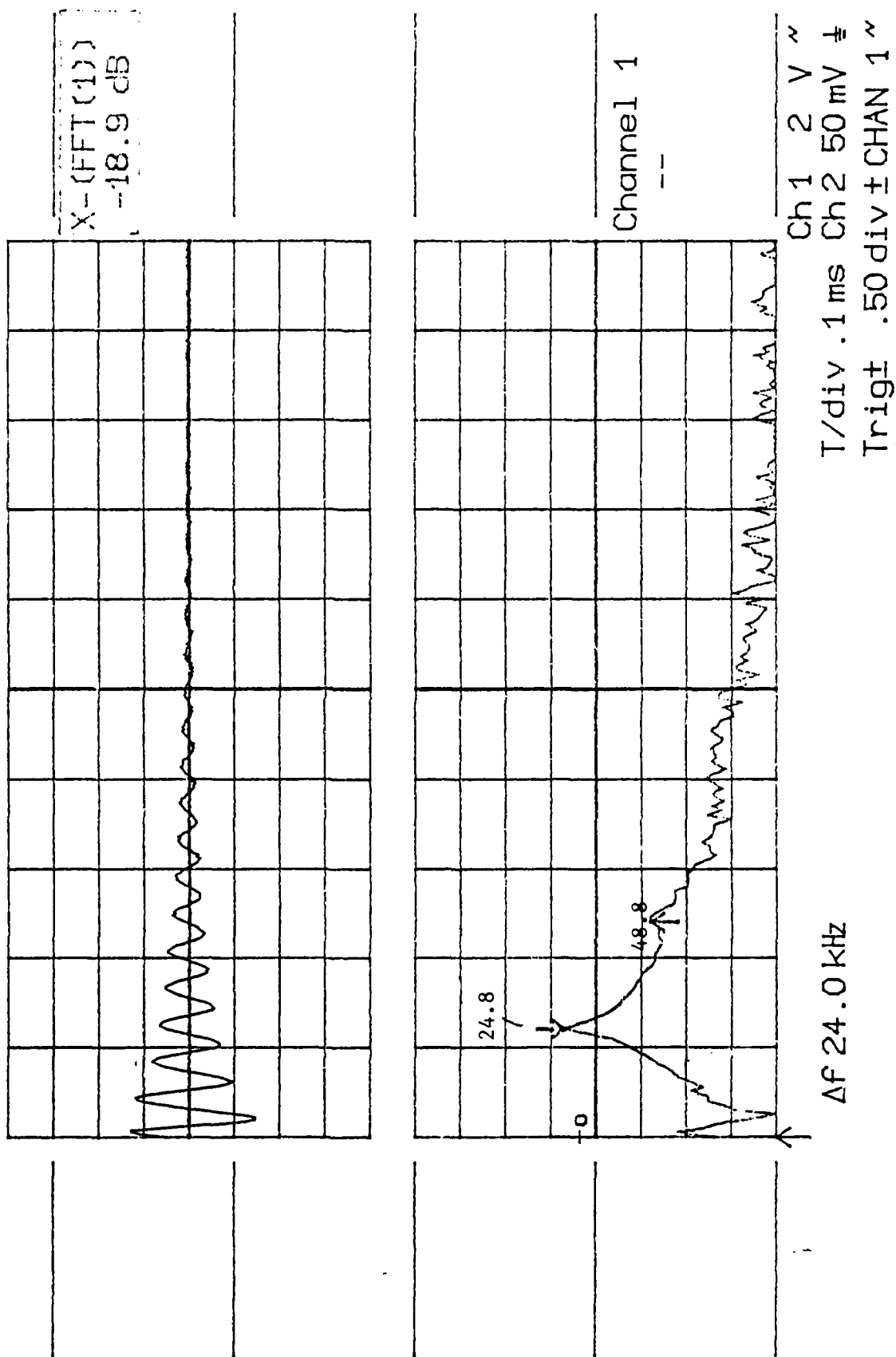


figure 14



- 1 Chief of Naval Research
Office of Naval Research
Department of the Navy
Arlington, VA 22219
Attn: Marshall Orr
- 2-5 Commanding Officer and Director
Defense Technical Information Center
Bldg. 5, Cameron Station
5010 Duke Street
Alexandria VA 22314
- 6-8 Dr. L. A. Crum
Associate Director of Basic Research
National Center for Physical Acoustics
University MS 38677
- 9 Professor M. S. Longuet-Higgins
Center for Studies of Nonlinear Dynamics
LaJolla Institute
10280 N. Torrey Pines Road, Suite 260
LaJolla CA 92037
- 10 Dr. A. Prosperetti
Department of Mechanical Engineering
The Johns Hopkins University
Baltimore MD 21218
- 11 Dr. B. R. Kerman
Atmospheric Environment Service
4905 Dufferin Street
Downsview, Ontario, M3H 5T4
Canada
- 12 Dr. J. A. Nystuen
Code 68Ny
Department of Oceanography
Naval Postgraduate School
Monterey CA 93943
- 13 Dr. W. A. Kuperman
Naval Research Laboratory
Washington DC 20375
- 14 L. Bjørnø
Industrial Acoustics Laboratory
Technical University of Denmark
Building 425, DK-2800
LYNGBY, Denmark
- 15-20 Paul A. Elmore
P.O.Box 15094
Millsaps College
Jackson, MS 39210